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USER'S MANUAL FOR COMPUTER PROGRAM ROTOR

Masahiro Yasue

August 1974

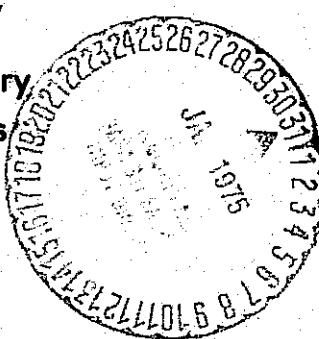


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Prepared under Contract No. NAS2-7262 by
Aeroelastic and Structures Research Laboratory
Department of Aeronautics and Astronautics
Massachusetts Institute of Technology
Cambridge, Massachusetts 02139

for

AMES RESEARCH CENTER
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION
MOFFETT FIELD, CALIFORNIA 94035



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FOREWORD

This report has been prepared by the Aeroelastic and Structures Research Laboratory (ASRL), Department of Aeronautics and Astronautics, Massachusetts Institute of Technology, Cambridge, Massachusetts, under NASA Contract No. NAS2-7262 from the Ames Research Center, National Aeronautics and Space Administration, Moffett Field, California 94035. Mr. John Rabbott and Dr. Wayne Johnson of the Ames Research Center served as technical monitors. The valuable assistance and advice received from these individuals is gratefully acknowledged.

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The computations were performed at the Information Processing Center of the Massachusetts Institute of Technology.

ABSTRACT

This report presents a detailed description of a computer program to calculate tilt-rotor aircraft dynamic characteristics. This program (named ROTOR) consists of two separate parts. In the first part, the natural frequencies and corresponding mode shapes of the rotor blade and wing are developed from structural data (mass distribution and stiffness distribution). The second part of the program deals with the frequency response (to gust and blade pitch control inputs) and eigenvalues of the tilt-rotor dynamic system, based on the natural frequencies and mode shapes derived beforehand. Sample problems are included to assist the user.

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SECTION 1

INTRODUCTION

1.1 Purpose and Scope

Program ROTOR is an in-core program written in FORTRAN IV language for analysis of the dynamic characteristics of the tilt-rotor aircraft.

The analytical model considered here consists of a cantilevered semispan wing with the engine-rotor system at the wing tip (see Fig. 1 of Ref. 1). The dynamic and aeroelastic characteristics of this aircraft are in many ways unique and complicated. The large flexible blades with a large amount of twist have significant coupling between flapping and lagging motion. The engines and gearboxes at the wing tip lead to low wing natural frequencies and possible resonances in the low frequency range.

The purpose of this program is the numerical analysis of the complicated dynamic and aeroelastic behavior of the tilt-rotor aircraft. The first step is the derivation of the equations of motion of the blade and the wing, including inertia forces, blade aerodynamic forces and wing aerodynamic forces. This formulation is described in detail in Ref. 1. Based on the equations of motion, the frequency response of the blade and wing motions to the gust input or blade pitch angle control input are derived. An eigenvalue analysis provides the system stability characteristics.

1.2 Program Outline and Limitations

Program ROTOR consists of two separate parts. One is called FREEVI (free vibration of the tilt-rotor aircraft), which produces the natural frequencies and mode shapes of the free vibration from the blade or from the wing structural characteristic data. The second part is named TILDYN (tilt-rotor dynamics)

which calculates the dynamic characteristics of the aircraft, including eigenvalues and frequency response to the gust and to the pitch-control inputs.

The reason for the separation of the program into two parts is that this system gives the user the opportunity to check the results for the natural frequencies and mode shapes without performing the entire calculation. In addition, the dynamic characteristics can be evaluated easily by changing the input natural frequencies or using different assumed modes without changing the structural characteristics, mass distribution, or stiffness distribution. The disadvantage is that the input data for TILDYN are the output data of FREEVI.

The free vibration problem of the wing and blade is solved as an eigenvalue problem in FREEVI by the finite element method. The wing has three degrees of freedom, vertical bending, chordwise bending and torsion. A large wing tip mass represents the rotor, engine, and gearbox.

Only flapping and lagging motions are considered for the blade. Torsion is neglected as a higher-order effect for the blade case. The rotor types treated here are the hingeless rotor and the gimbaled rotor. The maximum number of elements is limited to twenty.

With respect to the TILDYN program, it should be mentioned that the flight configuration is restricted to cruising flight only, with the rotor disk plane perpendicular to the free stream. Both powered and autorotation cases can be treated. Total degrees of freedom considered are nine or eighteen for powered flight. The nine degrees of freedom consist of blade flapping and lagging fundamental modes (each has a collective and two cyclic degrees of freedom) and wing vertical bending, chordwise bending, and torsion modes. The eighteen degrees of freedom include two additional blade modes and three additional wing modes. It should be noted

that description of the blade motion requires three independent degrees of freedom to reduce one equation with periodic coefficients in the rotating system to three equations with constant coefficients in the non-rotating system.

In the autorotation case, one more degree of freedom is added, the rigid body rotation of the rotor, and the total degrees of freedom become ten or nineteen. After the construction of the equations of motion for each case, the frequency response problem is solved. The excitation inputs consist of the following: vertical gust, lateral gust, longitudinal gust, collective-blade pitch control and two cyclic blade pitch controls. By appropriately specifying the excitation input components, the flight in a cross-wind gust can be considered.

The eigenvalue problem to be solved is the usual eigenvalue problem of a linear system of equations. The EISPACK subroutine developed by the Argonne Code Center is used to treat this problem (Refs. 2 and 3).

SECTION 2

DESCRIPTION OF THE PROGRAMS

2.1 Description of the FREEVI Program

This program consists of one main program and twelve subroutines for the computation of the lowest few eigenvalues and eigenvectors of the proprotor dynamic system modelled by the finite-element method, as described in Ref. 1. The outline flow chart is shown in Fig. 1.

Input data include element-structural characteristics (mass distribution, stiffness distribution and angle of twist), rotational speed, and some instruction data for the computation. The boundary conditions are automatically chosen when the calculation case is selected appropriately. Boundary conditions and degrees of freedom are tabulated in Table 1 for the rotor and wing. Next, the element stiffness and mass matrices are assembled globally. From the input information, the boundary conditions are imposed on the global system. The subspace iteration method is applied to find the eigenvalues and eigenvectors of the system (Refs. 4 and 5). Consider the eigenvalue problem of the n-degree-of-freedom equations:

$$[K][u] = \lambda [M][u] \quad (2.1)$$

where $[K]$ and $[M]$ are square stiffness and mass matrices with order n , $[u]$ is a matrix of the mode shape and λ is an eigenvalue. When m eigenvalues and eigenvectors are required, the main steps of the subspace iteration method are as follows:

- (a) Assume mode shape matrix $[u_0]$; $n \times m$ matrix containing m vectors
- (b) $[M_R] = [u_0]^T [M] [u_0]$; $[K_R] = [u_0]^T [K] [u_0]$ where $[M_R]$ and $[K_R]$ are reduced square matrices with order m .

- (c) Find eigenvectors $[A]$ ($m \times m$ matrix) such that $[K_R] [A] = [D] [M_R] [A]$, with $[D]$ denoting a diagonal matrix.
- (d) $[\bar{u}_o] = [u_o] [A]$
- (e) $[u_1] = [K]^{-1} [M] [\bar{u}_o]$
- (f) $[u_o] = [u_1]$ and go to step (b)

The eigenvalue analysis of the smaller system (order m) in step (c) is achieved by using the Jacobi method. The criterion of terminating the iteration is defined as

$$\left| \frac{\lambda_{i+1} - \lambda_i}{\lambda_i} \right| \leq e \quad (2.2)$$

Each eigenvalue must satisfy this criterion; the error threshold e can be defined by the user.

Output includes the input data, the eigenvalues, the eigenvectors, and, if required, punched-out cards of the eigenvectors. A built-in message as to whether convergence was achieved is also furnished.

A short description of each of the subroutines is given below:

MAIN	Defines dimensions
TEIGEN	Calculates the normal modes and frequencies
INPUT	Supplies input information
ELEMK	Controls the generation of element stiffness and mass matrices
MESH	Calculates mesh information for the finite element assemblage
ASBV	Applies boundary conditions
FAC	Triple matrix factorization
MTRTR	Matrix multiplication
MULTZ	Matrix multiplication
SOLZ	Forward and backward substitution
DNROOT	Eigen-analysis routine
EIGEN	Eigen-analysis routine needed in DNROOT
OUTPUT	Output routine

The listing is shown in Appendix A.

2.2 Description of the TILDYN Program

This program to solve the equations of motion of the tilt-rotor aircraft derived in Ref. 1, consists of one main program and twenty-four subroutine programs. The outline flow chart is shown in Fig. 2.

Input data are natural frequencies and corresponding mode shapes of the rotor and wing, aerodynamic coefficients, and flight conditions.

Based on such input data, the coefficients of the equations of motion are derived, using the numerical integration method. Finally, the equations of motion are formulated as a matrix:

$$[\mathbf{A}] \{ \ddot{\mathbf{x}} \} + [\mathbf{B}] \{ \dot{\mathbf{x}} \} + [\mathbf{C}] \{ \mathbf{x} \} = [\mathbf{D}] \{ \mathbf{e} \} \quad (2.3)$$

$[\mathbf{A}]$, $[\mathbf{B}]$, $[\mathbf{C}]$, and $[\mathbf{D}]$ are the coefficient matrices, including inertia terms and aerodynamic terms. The matrix $\{ \mathbf{x} \}$ is a set of variables and $\{ \mathbf{e} \}$ is an exciting force matrix including gust components and blade pitch-control components (see Ref. 1). These equations have nine or eighteen degrees of freedom in the powered flight case. In the autorotation flight case, ten or nineteen degrees of freedom are required, due to the addition of rigid-body rotation (see Table 2).

The dynamic characteristics of these equations are analyzed by two methods. One is the frequency-response analysis and the other is the eigenvalue analysis. In the frequency-response analysis, the accelerations and velocities of the equations are expressed in terms of a given frequency, and the differential equations are transformed into a set of linear algebraic equations. These linear equations are solved by the Gauss-Jordan reduction to obtain the response to the gust or blade pitch-control input.

The eigenvalue problem is formulated in the usual way. Equation 2.3 is rewritten

$$\begin{Bmatrix} \dot{x} \\ \ddot{x} \\ x \end{Bmatrix} = \begin{bmatrix} -A^{-1}B & -A^{-1}C \\ I & 0 \end{bmatrix} \begin{Bmatrix} \dot{x} \\ x \end{Bmatrix} \quad (2.4)$$

to obtain first-order differential equations. The real general matrix eigenvalue problem is solved by the EISPACK package, developed by Argonne National Laboratory to solve a standard matrix eigenvalue-eigenvector problem (Refs. 2 and 3).

A short description for each of the subroutines of the TILDYN program is given below:

MAIN	Defines the sequence of the program
BLOCK DATA	Initializes the coefficients of Gaussian quadrature
INITIL	Initialization of the matrices
COEFF	Defines the points and coefficients of the Gaussian quadrature
INPUT	Supplies input information
INTPL	Interpolation for the numerical integration by Gaussian quadrature
AERO	Defines the aerodynamic coefficients at the points of Gaussian quadrature
ORDINT	Defines the order of the numerical integration
INTEG	Numerical integration
F	Defines the integrand function
AINER	Defines the inertia coefficients of the equations in matrix form
AEROMT	Defines the aerodynamic coefficients of the equations in matrix form
EQMTX	Defines the coefficient matrices [A], [B], [C], and [D] in Eq. 2.3.
AUTO	In the autorotation case, another degree of freedom is added

GUSTCO	Defines gust and blade pitch control components
FRQRES	Calculates the frequency response
GAELI	The Gauss-Jordan reduction routine
EIGEN	Routine to form the eigenvalue problem and to call EIPACK subroutine
EIPACK	An eigensystem problem solver for the real general matrix consisting of EISPACK subroutine BALANC, ELMHES, ELTRAN, HQR2 and BALBAK
BALANC	Balances a real general matrix and isolates eigenvalues whenever possible
ELMHES	Obtains an upper Hessenberg matrix from a real general matrix
ELTRAN	Accumulates the elementary similarity transformations for the reduction to upper Hessenberg form
HQR2	Finds the eigenvalues and eigenvectors
BALBAK	Forms the eigenvectors by back-transforming those of the corresponding balanced matrix determined by BALANC
MINV	Inverses a matrix

The listing is shown in Appendix A.

SECTION 3
USER'S GUIDE FOR FREEVI PROGRAM

3.1 Input Data Requirements

The input and output of the computer code is a part of the built-in program with fixed format. This approach requires a minimum knowledge of the programs and programming.

The finite-element model for the input data is shown in Fig. 3. The structure is divided into several elements for application of the finite-element method. The mass distribution, bending and torsional stiffness, and angle of twist are the average values in the element. The unit system used should be consistent throughout the entire program.

This program calculates the natural frequencies and normal modes for five cases, including wing vibration and blade vibration with various boundary conditions (see Table 1). The parameter ICASE specifies the particular case in the program. The parameter IPUNCH specifies whether a punched card deck of the mode shapes is required for input to the program TILDYN.

Uncoupled mode shapes, instead of coupled mode shapes, can be generated, if necessary. The parameter IGUEST controls the initial assumed values for the purpose of generating the uncoupled mode shapes.

The value of M expresses the number of eigenvalues and mode shapes required by the user.

Parameters and variables are described in detail below:

DES A vector to express the test identifying information. The user can punch the run identification in the first column through the eightieth column of the first card. The format is 20A4.

ICASE A parameter to specify the calculation case:
ICASE=1; wing case with clamped boundary
conditions at the root.
ICASE=2; blade case with boundary conditions
clamped for the flapping motion and
clamped for the lagging motion at
the root.
ICASE=3; blade case, clamped for flapping and
hinged for lagging.
ICASE=4; blade case, hinged for flapping and
clamped for lagging.
ICASE=5; blade case, both hinged boundary
conditions.

It is punched in the integer format as I1 in the
first column of the second card.

IPUNCH A parameter to control whether the mode shapes are
punched out in cards for input to the TILDYN program.
IPUNCH=0; no punched output
IPUNCH=1; punched output

The parameter is punched in the integer format as
I1 in the first column of the third card.

IGUEST A parameter to control the mode-shape type coupled
or uncoupled, both for the blade and the wing.
IGUEST=0; coupled
IGUEST=1; uncoupled vertical bending (w)
IGUEST=2; uncoupled chordwise bending (v)
IGUEST=3; uncoupled torsion (ϕ)

It should be noted that the terms PB, RAMDA, COL
and THETA_E related to coupled motion should be
set to zero when uncoupled mode shapes are required.
The parameter is punched in the integer format as
I1 in the first column of the fourth card.

NET	Total number of elements, maximum number is 20. It is punched out in the integer format as I5 in the first through fifth columns in the fifth card.
NITR	The maximum number of iterations to be performed. If the number of iterations reaches NITR, yet the iteration is not converged, the program execution is terminated and a built-in message appears. Recommended value for NITR is 20. It is punched in the integer format as I5 in the 6th through the 10th columns of the fifth card.
M	Number of vibration modes required by the user. Recommended value for M is less than 10. If M = 10 to 20, NITR is recommended to be 50.
ERR	The error limit used to compare with $ (\lambda_{i+1} - \lambda_i)/\lambda_i $, where λ_i is the eigenvalue calculated at the i th iteration cycle. The iteration terminates if the calculated value is smaller than ERR. Recommended values for ERR are 0.001 to 0.01. It is punched in the real value format (F10.6) at the first through 10th columns of the sixth card.
OMEG	Rotational speed Ω in rad/sec, the direction of rotation is positive for the upward rotational vector when the aircraft configuration is in the helicopter mode. For the wing or non-rotating blade it is set to zero. It is punched in real value format (F10.6) in the first through the 10th columns of the seventh card.
RAMDA	Inflow ratio λ is defined as $(V + v)/\Omega R$. It determines the collective pitch of the blade. For the wing and non-rotating blade, it is set to zero. It is punched in real value format (F10.6) in the first through the 10th columns of the 8th card.

COL	Collective pitch angle in radians (θ_D in Ref. 1). For the wing case it is set to zero. It is punched in real value format (F10.6) in the first through the 10th columns of the 9th card.
SPKB	The flapwise spring constant at the root of the hinged rotor. If there is no spring, it is set to zero. It is punched in real value format (F10.6) in the 1st through the 10th columns of the 10th card.
SPKC	The lagwise spring constant at the root of the hinged rotor. If there is no spring, it is set to zero. It is punched in real value format (F10.6) in the 11th through 20th columns of the 10th card.
ALPHAH	The number is used to avoid a singularity of the stiffness matrix in the case of the hinged blade. The recommend value for ALPHAH is the squared value (λ^2) of the first non-zero eigenvalue. The value 5000.0 is appropriate for the first trial. It is punched in real value format (F10.6) in the first through the 10th columns of the 11th card.
EIBE	A vector to express the vertical bending stiffness $(EI)_B$ of the element. The length of the vector equals NET. It is punched in the exponent format (E15.7) and five data items can be included per card. These data occupy the 12th card through card $[10+(\text{NET}/5)]$ if NET is a multiple of 5. Otherwise, up to card $[11+(\text{NET}/5)]$ is occupied.
EICE	A vector to express the chordwise bending stiffness $(EI)_C$ of the element. The length of the vector is NET. It is punched in the exponent format (E15.7) and five data items can be included in a card. These data occupy $(\text{NET}/5)$ cards if NET is a multiple of 5, otherwise $[1+(\text{NET}/5)]$ cards.

THETAE	A vector to express the angle of twist θ_{AT} in radians of the structure element, positive nose up. It should be the average angle of twist over the element. The length of the vector is NET. Eight data items can be punched in real value format (F10.6) in each card. These data occupy (NET/8) cards if NET is a multiple of 8, otherwise [1+(NET/8)] cards.
AMASE	A vector to describe the mass distribution (mass/unit length); its length is NET. It is punched in real value format (F10.6), 8 data items on one card. These data occupy (NET/8) cards if NET is a multiple of 8, otherwise [1+(NET/8)] cards.
ESE	A vector to define the size of the beam element of the blade or wing and its length is NET. It is punched in real value format (F10.6), 8 data items on a card. These data occupy (NET/8) cards if NET is a multiple of 8, otherwise [1+(NET/8)] cards.
AMN	The number to express the tip mass. In the case of the wing, it includes the nacelle and all blade mass as
	$AMN = M_N + NM_B$
	in the symbols of Ref. 1. If a tip mass exists in the blade, it is also appropriate to use AMN. It is punched in real value format (F10.6) in the first through the 10th columns of the card. The next four numbers PIR, PIY, PIP and PBW are punched on the same card with AMN.
PIR	A number to express the rolling moment of inertia of the nacelle and blades at the wing tip:

$$PIR = I_{P_r} + NI_B$$

The format is (F10.6) and it is punched from the 11th to 20th columns.

PIY A number to express the yawing moment of inertia of the nacelle and blades at the wing tip:

$$\text{PIY} = I_{P_y} + \frac{N}{2} I_B + NM_B h^2$$

The format is (F10.6) and it is punched from the 21st to the 30th columns.

PIP A number to express the pitching moment of inertia of the nacelle and blades at the wing tip:

$$\text{PIP} = I_{P_p} + \frac{N}{2} I_B + NM_B h^2$$

The format is (F10.6) and it is punched from the 31st to the 40th columns.

PBW A number to express the mass coupling effect at the tip between the wing vertical bending and the torsion due to blade mass:

$$\text{PBW} = NM_B h$$

The format is (F10.6) and it is punched from the 41st to the 50th columns.

If the calculation case is the wing (ICASE=1), the next three data cards should be added:

GJ A vector to express the torsional rigidity: its length is NET. The format is (E15.7) and five data items can be included in a card. These data occupy (NET/5) cards if NET is a multiple of 5, otherwise [1+(NET/5)].

PI A vector to express wing mass moment of inertia about the elastic axis per unit length: its length is NET. The format is (E15.7) and five data items can be included in a card. These data occupy (NET/5) cards if NET is a multiple of 5, otherwise [1+(NET/5)].

PI12 A vector to express wing static mass moment of the segment to define the coupling motion between wing vertical bending and torsion. The vector length is NET and the format is (E15.7). Five data items can be included in a card and data occupy NET/5 cards if NET is a multiple of 5, otherwise [1+(NET/5)].

The data deck setup is shown in Fig. 5 and the example problem data listing is in Appendix B.

A few remarks will now be stated to avoid misuse of the program:

- 1) A consistent unit system must be adopted.
- 2) The maximum element number (NET) is 20.
- 3) Appropriate rotor rotational direction must be chosen. If OMEG is negative, RAMDA (inflow ratio) should be negative. However, COL (the collective pitch) and THETAE (angle of twist) should be positive nose up.
- 4) If uncoupled mode shapes are required, the coupling terms such as RAMDA, COL, THETA, PBW and PI12 should be set to zero.
- 5) If there are several cases to be dealt with, the data may consist of several data sets. After the execution of the first case, the computer automatically returns to the beginning of the program and reads the second input data set. Therefore, at the end of the entire calculation, the computer notes the absence of data sets and generates an error message.

3.2 Output Features

All input data are printed out for checking. The built-in messages and outputs in the FREEVI program are as follows:

(a) TENSION DUE TO CENTRIF. FORCE

This prints out the tension force at each nodal

(b) MASS = 0.XXXXXXXX

This indicates the total mass of the blade or wing.

(c) MOMENT OF INERTIA AT ROOT = 0.XXXXXXXX

This gives the mass moment of inertia of the blade or wing about the virtual hinge at the root.

(d) MAX. SIZE OF STF IS XXX SPECIFIED SIZE IS XXX

This prints out the specified value of the estimated length of the stiffness matrix and the actual required value for the stiffness matrix. If the specified value is smaller, the program stops. Check the input. If the required value is smaller, no remedy is needed.

(e) THE XXXXTH DIAG. AFTER FACT=0.0, INCOMPLETE FACT

This message appears when the factorization of the mass matrix is not complete. The program also stops. Check the input.

(f) NO. OF NEGATIVE DIAG. = XXXX, FACT COMPLETED

This prints out the number of negative diagonals of the factorized mass matrix. If the printed value is other than zero, the mass matrix is not positive definite. Check the input data.

(g) EIGENVALUES =

At each iteration, calculated eigenvalues are printed out. If eigenvalues satisfy the accuracy requirements, these results are printed out in eigenvalue format (the square value of the natural frequency), radian/second and Hertz.

(h) NO. OF ITERATION = XXXX CONVERGED WITHIN 0.XXXXXXXX

This indicates that the subspace iteration is completed. The first value printed is the number of the

iteration and the second value is the error limit input by the user.

(i) NO. OF ITERATION = XXXX NOT CONVERGED

This appears instead of (h) message if the user specified maximum number of iterations (NITR) has been reached, yet the eigenvalues have not converged to within the error limit set by the user. The user should check the input for possible errors or change the error limit (ERR) because the previous error limit may be too small to be achieved, or increase the maximum number of iteration (NITR).

(j) REDUCED MASS MATRIX

The lower triangular part of the reduced mass matrix is printed out.

(k) REDUCED STIF MATRIX

The lower triangular part of the reduced stiffness matrix is printed out.

(l) *****BLADE MODE SHAPES***** or *****WING MODE SHAPES*****

Mode shapes are printed out. Index I indicates the eigenvalue to which the mode shape corresponds and index J indicates the station number of the node. Symbols W(I,J), V(I,J), PW(I,J), and DV(I,J) are vertical bending (flapping motion), chordwise bending (lagging motion), slope of the vertical bending, and slope of the chordwise bending, for the case of blade vibration. In addition to those symbols, PHI(I,J) and DPHI(I,J) are used for the torsion and slope of the torsion for the wing vibration. The coordinate system is shown in Fig. 4.

(m) Punched Card Output

If IPUNCH is set equal to one, the punched card output is also performed. The format is E13.5 with six data items on a card. The order is W(1,1) of the first mode to last W(1,NET+1), punched on $[(NET+1)/6]$ cards if $(NET+1)$ is a multiple of 6, otherwise $[(NET+1)/6+1]$ cards. Next V(1,J), DW(1,J) and DV(1,J) groups are punched. After the first mode shape the group of the second mode shape is punched and it continues to the Mth mode shape. In the case of the wing, the output data of PHI(I,J), DPHI(I,J) are added in the same fashion after the set of DV(I,J).

3.3 Example Problems

Example problems cited here for the FREEVI program are taken from Ref. 1.

3.3.1 Application to the Wing

The free vibration of the Bell wing is considered in this report. Structural characteristics (mass distribution, bending stiffness and so on) are shown in Fig. 6. Mass moments of inertia of the nacelle and blades are tabulated in the "Bell" column of Table 3. The listing of both input and output are shown in Appendix B.

3.3.2 Application to the Blade

The hingeless rotor of the Boeing Vertol is studied here. It should be noted that the rotation direction is negative in this case. Structural characteristics are shown in Fig. 7. The listing of both input and output are shown in Appendix B.

SECTION 4

USER'S GUIDE FOR THE TILDYN PROGRAM

4.1 Input Data Requirements

This program has several parameters to designate the case being considered by the user. The first one is ITYPE, which specifies whether collective mode shapes of the blade different from the cyclic mode shapes are needed. If it is the gimballed rotor, the parameter instructs the computer to read more data for the collective mode shapes of the gimballed rotor. The parameter IFLT defines whether the case considered is powered flight or autorotation flight. The next parameter IDOF specifies the number of degrees of freedom. If it is nine, two blade modes (giving six degrees of freedom in the non-rotating system) and three wing modes are necessary. If IDOF is eighteen, two more modes for the blade and three more modes for the wing should be added to the nine degrees-of-freedom system. The parameter IRES specifies execution of the frequency response analysis. The user should decide whether the response based in terms of normal mode shapes or in terms of mode shapes normalized to unity at the blade tip. This is determined by the parameter IFRMAG. The last parameter IEIGEN specifies execution of the eigenvalue analysis.

Parameters and variables are described in input order below:

DES A vector to express the test identifying information.
The user can punch the run identification in the first column through the eightieth column of the first card.
The format is 80Al.

ITYPE A parameter to control the reading of input data depending upon the type of rotor.
ITYPE=0; the hingeless rotor in powered flight
ITYPE=1; the hingeless rotor in autorotational flight.
the gimballed rotor both in powered and autorotational flight.

The format is (I1) and it is punched in the first column of the second card.

IFLT A parameter to determine the flight condition.

IFLT=0; powered flight

IFLT=1; autorotation flight

The format is (I1) and it is punched in the first column of the third card.

IDOF A parameter to define the number of basic elastic deformation degrees of freedom and how many mode shapes are needed. It should be noted that the same number IDOF is used for both powered flight and autorotation flight.

IDOF=9; In the powered flight case, nine equations are constructed and two mode shapes for the blade and three mode shapes for the wing are necessary. In the autorotation flight (IFLT=1), ten equations are constructed, due to the addition of the rigid-body rotation of the blades.

The same number of mode shapes as for the powered flight is necessary.

IDOF=18; In powered flight, eighteen equations are formulated. In autorotation flight they become nineteen. In total, four mode shapes are necessary for the blade and six for the wing.

The format is (I1) and it is punched in the first two columns of the fourth card.

IRES A parameter to control whether the frequency response analysis is carried out.

IRES=0; it is not carried out.

IRES=1; it is carried out.

The format is (I1) and it is punched in the first column of the fifth card.

IFRMAG A parameter to control the type of mode shapes used for the output results.

IFRMAG=0; the frequency response and eigenvector results are based on mode shapes as follows: the predominant components of the blade-coupled-mode shape are normalized to R (rotor radius) at the maximum deflection point. The wing-bending-mode shapes are normalized to L (wing semispan) at the maximum deflection point, and the wing-torsion-mode shape is normalized to unity at the maximum deflection point. This type of normalization is for the purpose of obtaining results comparable with those described in Ref. 6.

IFRMAG=1; the frequency response and eigenvector results are based on the normal modes used as input data.

The format is (I1), and it is punched out in the first column of the sixth card.

IEIGEN A parameter to control whether the eigenvalue analysis is executed.

IEIGEN=0; it is not executed.

IEIGEN=1; it is executed.

The format is (I1) and it is punched in the first column of the seventh card.

NOBLD The blade number. The format is (I1) and it is punched in the first column of the eighth card.

ROH The air density. The format is (E10.0); the user can put a datum in either F format or E format in the first ten columns of the ninth card.

OMEGA The rotor rotational speed (radian/sec). The format is E10.0; the user can choose either E or F type. The datum is put in the eleventh column through the twentieth column of the ninth card. OMEGA can take positive or negative values corresponding to the rotational direction. The sign definition is the same as that of the FREEVI program.

RAMDA The inflow ratio. The sign should be consistent with the rotational direction of the rotor. The format is either in E or F type. The datum is put in the 21st through 30th column of the ninth card.

VEL The cruising speed of the aircraft. The format is either E or F type. The datum is put in the 31st through the 40th column of the ninth card.

R The blade radius. The format is either E or F type. It is punched in the first through the tenth column of the tenth card.

AIB The blade flapping moment of inertia. The format is either E or F type. It is punched in the eleventh through the 20th column of the tenth card.

CHOD The mean chord length of the blade. The format is either E or F type. It is punched in the 21st through the 30th column of the tenth card.

CL The lift-curve slope of the blade. The format is either E or F type. It is punched in the 31st through the 40th column of the tenth card.

CD The drag coefficient of the blade (C_{D_0}). The format is either E or F type. It is punched in the 41st through the 50th column of the tenth card.

HMAST	The mast height. The format is either E or F type. It is punched in the 51st through the 60th column of the tenth card.
DEL3	The rotor blade pitch-flap coupling (δ_3). The unit is radians. The format is either E or F type. It is punched in the 61st through the 70th column of the tenth card.
WL	The wing semispan length. The format is either E or F type. It is punched in the first through the tenth column of the eleventh card.
WCOD	The mean wing chord length. The format is either E or F type. It is punched in the eleventh through the 20th column of the eleventh card.
WCL	The wing lift curve slope. The format is either E or F type. It is punched in the 21st through the 30th column of the eleventh card.
WCD	The wing drag coefficient (C_{D_0} of the wing). The format is either E or F type. It is punched in the 31st through the 40th column of the eleventh card.
WCMO	The wing pitching moment coefficient (C_{m_0}). The format is either E or F type. It is punched out in the 41st through the 50th column of the eleventh card.
WCMA	The wing pitching moment curve slope (C_{m_a}). The format is either E or F type. It is punched in the 51st through the 60th column of the eleventh card.
EDIS	The distance (nondimensionalized by the wing chord) between the elastic axis and the aerodynamic center of the wing (positive if the aerodynamic center is ahead of the elastic axis). The format is either E or F type. It is punched in the 61st through the 70th column of the 11th card.

WTHET	The wing trim angle of attack in radians. The format is either E or F type. It is punched in the 71st through the 80th column of the eleventh card.
CGUST	A vector to express the magnitudes of the exciting force components shown in Eq. 2.3 as {e}.
	CGUST(1); vertical gust u_G/V
	CGUST(2); lateral gust v_G/V
	CGUST(3); longitudinal gust w_G/V
	CGUST(4); collective pitch control θ_o
	CGUST(5); cyclic cosine pitch control θ_{lc}
	CGUST(6); cyclic sine pitch control θ_{ls}
	If the user specifies 1.0 for one of these quantities, that gust or pitch control quantity becomes the exciting force. Each vector component has either E or F format and occupies ten columns each of the twelfth card.
BRAM	A vector to express the blade eigenvalues and its length is 4. The values are the squared values of the natural frequencies ($\text{rad}^2/\text{sec}^2$). If IDOF is set equal to 9, the latter two eigenvalue columns may have blanks. If the calculation case is the gimballed rotor (ITYPE=1), BRAM should include the cyclic mode eigenvalues of the blade. The format is either E or F type and each component occupies ten columns in order of the 13th card.
WRAM	A vector to express the wing eigenvalues and its length is 6. The values are the squared values of the natural frequencies ($\text{rad}^2/\text{sec}^2$). If IDOF is set equal to 9, the latter three eigenvalue columns may have blanks. The format is either E or F type and each component occupies ten columns in order of the 14th card.
NW	A number to specify the wing element quantity. The format is (I2) and it is punched in the first two columns of the 15th card.

EMSW	A vector to describe the wing element size. The vector length is NW and the element size, nondimensionalized by the wing semispan, should be input. The format is either E or F type (E10.0). Each vector component occupies ten columns from the 16th card. The number of the card for EMSW is NW/8 if NW is a multiple of 8. Otherwise [(NW/8) + 1] cards.
G	A matrix to describe the wing vertical bending mode shape (γ in Ref. 1) at the nodes. The size of the matrix is $MW \times (NW+1)$, where MW is 3 if IDOF=9 and 6 if IDOF=18. The format is E or F type (E13.5) and $G(1,1)$ expresses the vertical deflection at the root node of the first mode. $G(1,NW+1)$ is the one at the tip node of the first mode (Fig. 4). The data should be punched in order from the root node to the tip node value. One card can include 6 data.
Z	A matrix to describe the wing chordwise bending mode shape (ζ in Ref. 1) at the node. Other comments are the same as for G.
DG	A matrix to describe the wing vertical bending slope ($d\gamma/dy$ in Ref. 1). Other comments are the same as for G.
DZ	A matrix to describe the wing chordwise bending slope ($d\zeta/dy$ in Ref. 1). Other comments are the same as for G.
WPHI	A matrix to describe the wing torsion deflection (ϕ in Ref. 1). Other comments are the same as for G.
DWPHI	A matrix to describe the wing torsion slope ($d\phi/dy$ in Ref. 1). Other comments are the same as for G.

The output of the FREEVI program automatically satisfies the deck setup for the TILDYN program, but for convenience the card setup for the wing mode shapes are repeated as follows:

```

1st card contains G(1,1), G(1,2)..... G(1,6)
Next card contains G(1,7) .....G(1,NW+1)
New card contains Z(1,1)..... Z(1,6)
Z(1,7)..... Z(1,NW+1)
New card contains DG(1,1).....
DG(1,7).....
New card contains DZ(1,1).....
DZ(1,7).....
New card contains WPHI(1,1).....
WPHI(1,7).....
New card contains DWPHI(1,1).....
DWPHI(1,7).....
New card contains G(2,1)..... G(2,6)
G(2,7)
Z(2,1)
Z(2,7)
.
.
.
New card contains DWPHI(MW,1).....
Last card for the wing mode shape contains DWPHI(MW,7)...
DWPHI(MW,NW+1)

```

The wing mode shapes occupy N_W cards where

$$N_W = \begin{cases} 6MW[(NW+1)/6] & \text{if } (NW+1) \text{ is a multiple of 6} \\ 6MW[(NW+1)/6+1] & \text{if } (NW+1) \text{ is not a multiple of 6} \end{cases}$$

N A number to specify the blade element quantity. The format is (I2) and it is punched in the first two columns of the next card to the wing mode shapes.

EMS	A vector to describe the blade element size. The vector length is N and the element size, nondimensionalized by the rotor radius, should be input. The format is either E or F type (E10.0). Each vector component occupies ten columns, and the card number is N/8 if the N is a multiple of 8. Otherwise [N/8+1] cards.
AMASS	A vector to describe the mass distribution of the blade. The vector length is (N+1). The value should be the mass distribution (mass per unit length) expressed at the node. The format is either E or F type (E10.0). Each vector component occupies ten columns, and the card number is (N+1)/8 if (N+L) is a multiple of 8. Otherwise [(N+1)/8+1] cards.
THETN	A vector to describe the angle of twist of the blade. The vector length is (N+1). The value should be the angle of twist at the node and positive nose up. The format is either E or F type (E10.0). Each vector component occupies ten columns, and the card number is (N+1)/8 if (N+1) is a multiple of 8. Otherwise, [(N+1)/8+1] cards.
COL	A number to express the collective pitch angle (θ_D in Ref. 1) defined from the performance (trim) calculation. The format is either E or F type (E10.0), and it occupies the first ten columns of the next card to THETN.
W	A matrix to describe the blade out-of-plane bending mode shape (W_j in Ref. 1) at the node. The size of the matrix is MBx(N+1) where MB is 2 if IDOF=9 and 4 if IDOF=18. The format is E or F type (E13.5) and W(1,1) expresses the out-of-plane deflection at the root node of the first mode. W(1,N+1) is the one at the tip node of the first mode. The data should be punched in order from the root node to the tip node value. One card can include 6 data.

V A matrix to describe the blade inplane bending mode shape (V_j in Ref. 1) at the node. Other comments are the same as those for W.

DW A matrix to describe the blade out-of-plane bending mode shape slope (dW_j/dr in Ref. 1) at the node. Other comments are the same as those for W.

DV A matrix to describe the blade inplane bending mode shape slope (dV_j/dr in Ref. 1) at the node. Other comments are the same as those for W.

If the calculation case is the gimballed rotor (ITYPE=1), or auto-rotational flight (ITYPE=1 and IFLT=1), the above blade-mode shapes correspond to the cyclic mode shapes.

The output of the FREEVI program automatically satisfies the deck setup for the TILDYN program; however, for convenience, the card setup for blade mode shapes is repeated below:

1st card contains W(1,1), W(1,2),W(1,6)

Next card contains W(1,7).....W(1,N+1)

New card contains V(1,1).....

 V(1,7).....

 DW(1,1)

 DW(1,7)

 DV(1,1) DV(1,6)

 DV(1,7)..... DV(1,N+1)

 W(2,1)

 W(2,7)

 V(2,1)

 V(2,7)

 •

 •

 •

 •

 •

 •

 DV(MB,1)

Last card contains DV(MB,7) DV(MB,N+1)

The blade mode shapes occupy n_B cards where

$$n_B = \begin{cases} 4MB[(N+1)/6] & \text{if } (N+1) \text{ is a multiple of 6} \\ 4MB[(N+1)/6+1] & \text{if } (N+1) \text{ is not a multiple of 6} \end{cases}$$

If the computer calculation case is the gimballed rotor (ITYPE=1) or autorotational flight (ITYPE=1 and IFLT=1), the next five data cards as for the collective mode shapes of the blade should be added.

BRAMO A vector to express the blade collective mode eigenvalues and its length is 4. The values are the squared values of the natural frequencies ($\text{rad}^2/\text{sec}^2$). If INOF is set equal to 9, the latter two eigenvalue columns may have blanks. The format is either E or F type and each vector component occupies ten columns in order of the next card to the blade mode shapes.

WCOL A matrix to describe the blade collective out-of-plane bending mode shape (W_j^0 in Ref. 1) at the node. The size and other comments are the same as those for W.

VCOL A matrix to describe the blade collective inplane bending mode shape (V_j^0 in Ref. 1) at the node. Other comments are the same as those for W.

DWCOL A matrix to describe the blade collective out-of-plane mode shape slope (dW_j^0/dr in Ref. 1). Other comments are the same as those for W.

DVCOL A matrix to describe the blade collective inplane mode shape slope (dv_j^0/dr in Ref. 1). Other comments are the same as those for W.

The data deck setup is shown in Fig. 8, and an example problem data listing is given in Appendix B.

A few notes to supplement the input data definitions:

- a) The maximum element number (N or NW) is 20
- b) If rotor rotational direction is negative, RAMDA should be negative. However, THETN and COL are positive nose up as in the FREEVI program.
- c) The mode shapes used in the TILDYN program should be defined as normal modes. Those definitions appear in Eq. 4.7 for the blade and in Eq. 4.12 for the wing in Ref. 1. If modes are not normalized in this way, the calculation will give wrong answers.
- d) Output mode shapes from the FREEVI program sometimes include unnecessary mode shapes; for example, the rigid body mode for the collective mode shapes of the gimballed rotor if the user uses the clamped boundary condition for the flapping motion and the hinged boundary condition for the lagging motion to derive the collective mode for autorotational flight.
- e) If there are several cases, the data may consist of several data sets. The computer execution continues until it finds the absence of data.

4.2 Output Features

In the output, the identifying title is printed first, as punched in by the user. All input data are printed out below.

After the mode shape listing, the matrices A, B, C, and D of the equations of motion in Eq. 2.3 are listed. When the degrees of freedom of the equations are 18 or 19, the first 9 columns of the coefficient matrix are printed out, followed by the latter 9 or 10 columns of the matrix.

If the user has chosen the frequency response analysis (IRES=1), the results of that calculation appear next. Each

response magnitude is showed corresponding to a nondimensional frequency. If IFRMAG is set equal to zero, the response magnitudes are based on the mode shapes normalized to rotor radius and wing semispan (refer to the explanation of IFRMAG in Section 4.1). In autorotation flight, the rigid-body rotation response is added to the basic form. It should be noted that the rigid-body rotation response is the rotational speed perturbation response, not the deflection response. Therefore, it is termed $D(NUR)/DT$ (to express $\dot{\nu}_R$).

The eigenvalue analysis consists of the eigenvalue and eigenvector listing. All eigenvalues of the system are printed in the form of complex values with damping ratios, including pairs of complex conjugate values. The eigenvectors corresponding to the eigenvalue are printed. The maximum absolute values of the eigenvector components are normalized to unity. Real parts and imaginary parts express the phase angle between each eigenvector component. If IFRMAG is set to zero, the eigenvectors are expressed based on the mode shapes normalized by rotor radius and wing semispan (refer to the explanation of IFRMAG in Subsection 4.1) as in the frequency response. On the other hand, if IFRMAG is set to unity, all are in length, except ν_R (rigid-body rotation in autorotation flight). ν_R is an angle, in radians. Therefore, some attention should be paid to comparing the role of each eigenvector.

Only one built-in message is furnished for this program. If an error occurs in the eigenvalue analysis, the message below is automatically printed out after the title "EIGENVALUES":

IERROR=XXXXX

The error code is shown as follows:

<u>Value of IERROR</u>	<u>Error Significance</u>
I	The calculation of the Ith eigenvalue failed to converge. Eigenvalues I+1 ... N should be correct.
-I	The calculation of one or more eigenvectors, including the Ith, failed to converge. All eigenvalues and non-zero eigenvectors are correct.

4.3 Example Problems

Sample problems are carried out here for the Bell and Boeing tilt rotor wings. The flight condition is normal level flight cruising (around 200 kt) at sea level. The detail data is shown in Table 3. The input data listing in Appendix B includes the autorotation flight case for the Bell model and the powered flight case for the Boeing model. However, the output listing of only the Bell autorotation flight case is shown as an example in Appendix B.

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TABLE 1 BOUNDARY CONDITIONS AND OUTPUT DEFLECTIONS OF THE ROTOR AND WING IN THE FREEVI PROGRAM

		BOUNDARY CONDITIONS		OUTPUT DEFLECTIONS
		ROOT	TIP	
Wing		Clamped for all Deflections	Lumped Mass with Mass and Mass Moment of Inertia	Vertical Bending Chordwise Bending Torsion
Blade Powered				
Hingeless Rotor		Clamped for all Deflections	Free or Tip Mass if Necessary	Out-of-Plane Bending Inplane Bending
Gimballed Rotor				
Collective Mode		Clamped for all Deflections	"	"
Cyclic Mode		Hinged for Flapping, Clamped for Lagging	"	"
Autorotation				
Hingeless Rotor				
Collective Mode		Clamped for Flapping, Hinged for Lagging	"	"
Cyclic Mode		Clamped for all Deflections	"	"
Gimballed Rotor				
Collective Mode		Clamped for Flapping, Hinged for Lagging	"	"
Cyclic Mode		Hinged for Flapping, Clamped for Lagging	"	"

TABLE 2 DESCRIPTION OF VARIABLES

(a) Description of $\{x\}$ in Eq. 2.3

Total Degrees of Freedom				Description
Powered Flight	Autorotation Flight			
9 DOF	18DOF	10DOF	19DOF	
Q_{10}	Q_{10}	Q_{10}	Q_{10}	Blade Collective Motion of 1st Natural Frequency
Q_{1c}	Q_{1c}	Q_{1c}	Q_{1c}	Blade Cyclic Cosine Motion of 1st Natural Frequency
Q_{1s}	Q_{1s}	Q_{1s}	Q_{1s}	Blade Cyclic Sine Motion of 1st Natural Frequency
Q_{20}	Q_{20}	Q_{20}	Q_{20}	Blade Collective Motion of 2nd Natural Frequency
Q_{2c}	Q_{2c}	Q_{2c}	Q_{2c}	Blade Cyclic Cosine Motion of 2nd Natural Frequency
Q_{2s}	Q_{2s}	Q_{2s}	Q_{2s}	Blade Cyclic Sine Motion of 2nd Natural Frequency
	Q_{30}		Q_{30}	Blade Collective Motion of 3rd Natural Frequency
	Q_{3c}		Q_{3c}	Blade Cyclic Cosine Motion of 3rd Natural Frequency
	Q_{3s}		Q_{3s}	Blade Cyclic Sine Motion of 3rd Natural Frequency
	Q_{40}		Q_{40}	Blade Collective Motion of 4th Natural Frequency
	Q_{4c}		Q_{4c}	Blade Cyclic Cosine Motion of 4th Natural Frequency
	Q_{4s}		Q_{4s}	Blade Cyclic Sine Motion of 4th Natural Frequency
a_1	a_1	a_1	a_1	Wing Motion of 1st Natural Frequency
a_2	a_2	a_2	a_2	Wing Motion of 2nd Natural Frequency
a_3	a_3	a_3	a_3	Wing Motion of 3rd Natural Frequency
	a_4		a_4	Wing Motion of 4th Natural Frequency
	a_5		a_5	Wing Motion of 5th Natural Frequency
	a_6		a_6	Wing Motion of 6th Natural Frequency
	v_R	v_R		Rotor Rigid-Body Rotation

TABLE 2 CONCLUDED

(b) Description of $\{\epsilon\}$ in Eq. 2.3

Symbol	Description
u_G/V	Nondimensional Vertical Gust
v_G/V	Nondimensional Lateral Gust
w_G/V	Nondimensional Longitudinal Gust
θ_o	Collective Pitch Control
θ_{lc}	Lateral Cyclic Pitch Control
θ_{ls}	Longitudinal Cyclic Pitch Control

TABLE 3

DESCRIPTION OF THE BELL AND THE BOEING PROPROTOR DESIGNS
IN POWERED FLIGHT CONSIDERED IN THIS REPORT

	<u>BELL</u>	<u>BOEING</u>
ROTOR		
Type	gimballed, stiff inplane	cantilever, soft inplane
Number of blades, N	3	3
Radius, R	156 in.	150 in.
Chord, C_B	18.9 in.	14 in.
Lock number, γ	3.83	4.04
Solidity, σ	0.089	0.115
Pitch/flap coupling, δ_3	-15 deg.	0
Collective pitch, θ_D	1.25 deg.	1.0 deg.
Lift-curve slope, a	5.7	5.7
Drag Coefficient, C_{D0}	0.0065	0.0065
Rotor rotation direction, $\bar{\Omega}$	+1	-1
Inflow ratio,	0.7	-0.7
Rotational speed, $ \Omega $	458 RPM 48.9 rad/sec	386 RPM 40.4 rad/sec
Blade Natural Frequencies		
first, $\lambda_1/ \Omega $	1.02/rev (7.78Hz)	0.827/rev. (5.32Hz)
second, $\lambda_2/ \Omega $	1.34/rev (10.2Hz)	1.32/rev (8.49Hz)
third, $\lambda_3/ \Omega $	4.35/rev (33.2Hz)	3.40/rev (21.9Hz)

TABLE 3. CONTINUED

ROTOR (cont'd)	<u>BELL</u>	<u>BOEING</u>
fourth, $\lambda_4^{(o)}/ \Omega $	10.1/rev (77.1Hz)	6.77/rev (43.5Hz)
Collective Natural Frequency		
first, $\lambda_1^{(o)}/ \Omega $	1.31/rev (10.0Hz)	
second, $\lambda_2^{(o)}/ \Omega $	2.12/rev (16.2Hz)	
third, $\lambda_3^{(o)}/ \Omega $	4.93/rev (37.7Hz)	
fourth $\lambda_4^{(o)}/ \Omega $	10.6/rev (80.9Hz)	
Blade flapping inertia, I_B	105 slug-ft ²	150 slug-ft ²
One blade weight, M_B	133 lb	124 lb
WING		
Semispan, L	200 in.	200 in.
Chord, c_w	62.2 in.	62.2 in.
Mast height, h	51.3 in.	51.3 in.
Sweep	0	0
Dihedral	0	0
Lift-curve slope, a_w	5.7	5.7
Drag coefficient, C_{Dw}	0.004	0.004
Moment coefficient C_{mo}	-0.005	-0.005
Aerodynamic center, $\bar{e} = x_{Aw}/c_w$	0.01	0.01
Angle of attack, α_{wo}	2.0 deg	2.0 deg

TABLE 3. CONCLUDED

	<u>BELL</u>	<u>BOEING</u>
WING (cont'd)		
Natural Frequencies		
first, $\Lambda_1/ \Omega $	0.347/rev (2.65Hz)	0.365/rev (2.35Hz)
second, $\Lambda_2/ \Omega $	0.622/rev (4.75Hz)	0.653/rev (4.20Hz)
third, $\Lambda_3/ \Omega $	1.09/rev (8.32Hz)	1.11/rev (7.14Hz)
fourth, $\Lambda_4/ \Omega $	2.37/rev (18.1Hz)	2.47/rev (15.9Hz)
fifth, $\Lambda_5/ \Omega $	3.76/rev (28.7Hz)	3.95/rev (25.4Hz)
sixth, $\Lambda_6/ \Omega $	10.6/rev (80.9Hz)	12.5/rev (80.4Hz)
PYLON		
Weight, M_p	1420 lb	2000 lb
Yaw inertia, I_{py}	164.8 slug-ft ²	250.0 slug-ft ²
Pitch inertia, I_{pp}	190.0 slug-ft ²	250.0 slug-ft ²
Roll inertia, I_{pr}	42.4 slug-ft ²	30.0 slug-ft ²
FLIGHT CONDITION FOR CALCULATIONS, $\lambda = 0.7$		
Cruising speed, V	250 kt	218 kt
Cruising altitude	sea level	sea level

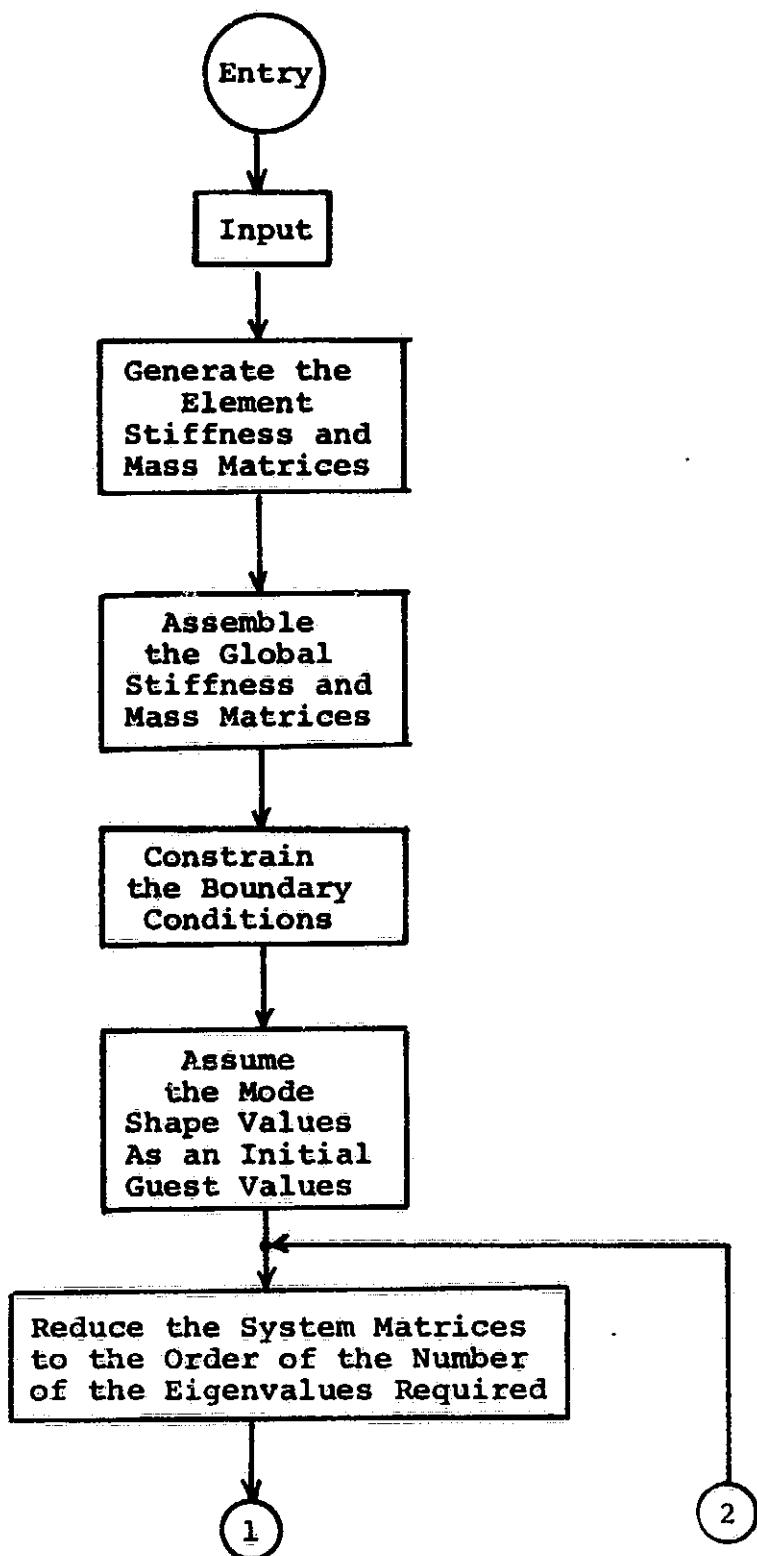


FIG. 1 FLOW CHART OF FREEVI PROGRAM FOR BLADE AND WING OF NATURAL FREQUENCIES AND MODE SHAPES

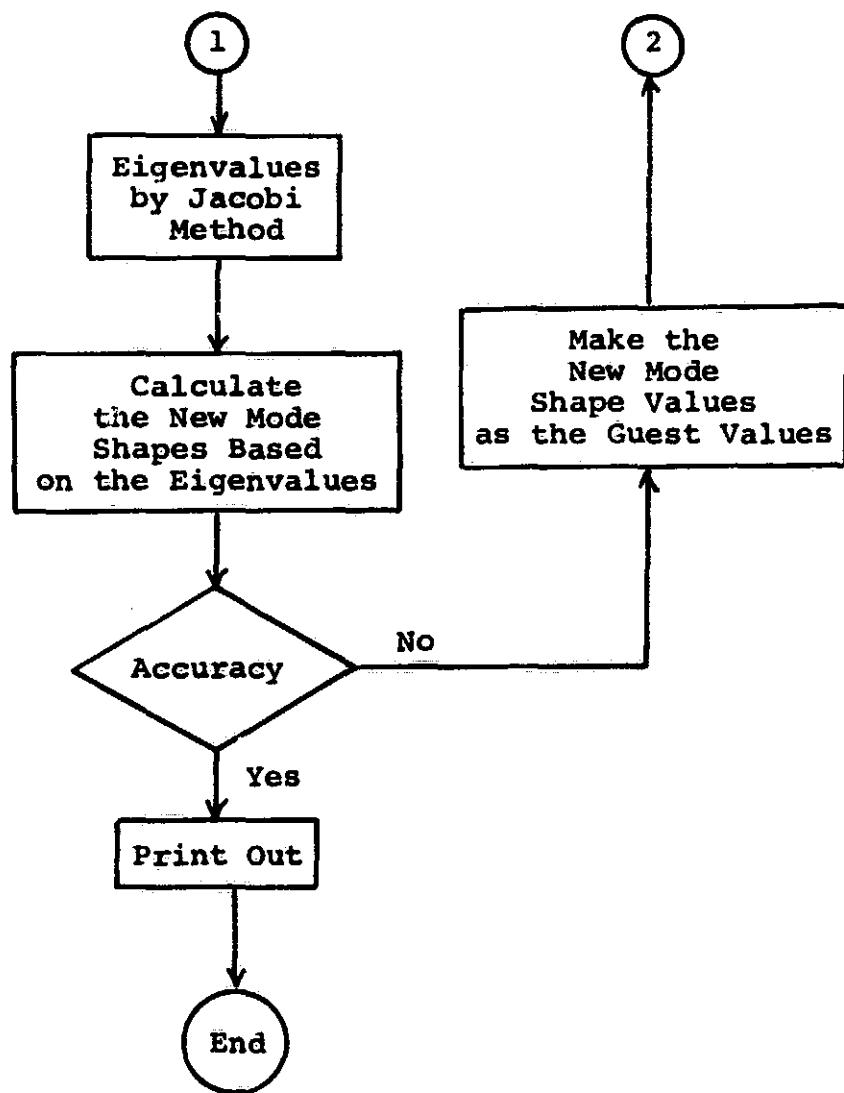


FIG. 1 CONCLUDED

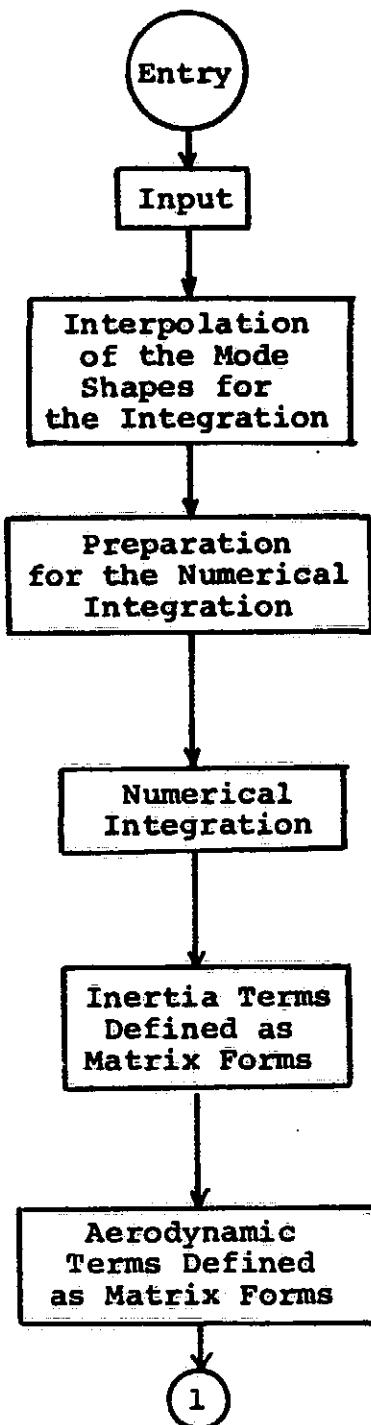


FIG. 2 FLOW CHART OF TILDYN PROGRAM FOR ANALYSIS OF
TILT ROTOR AIRCRAFT DYNAMICS

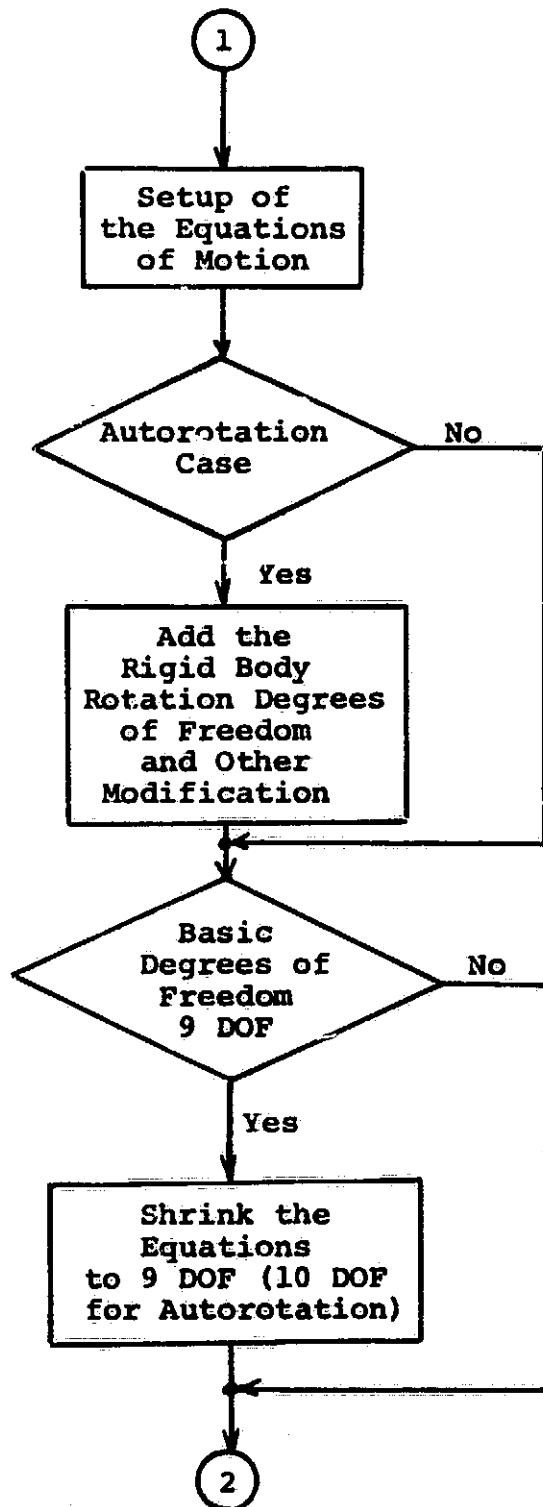


FIG. 2 CONTINUED

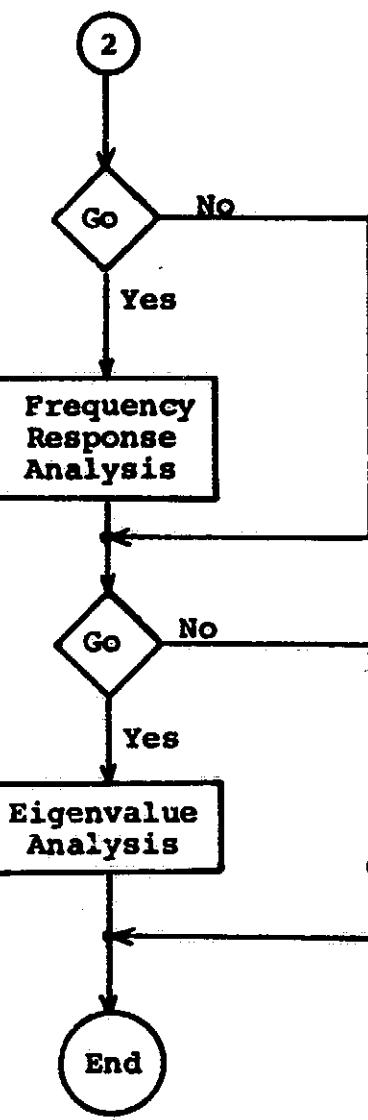


FIG. 2 CONCLUDED

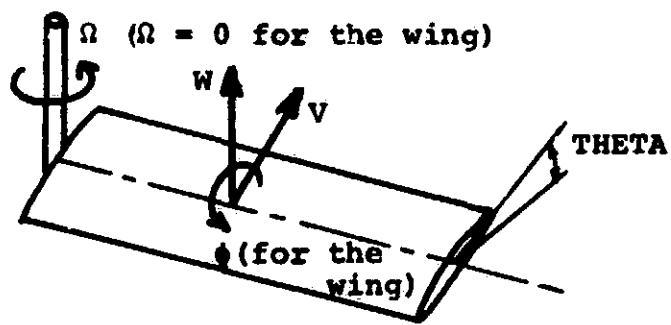


FIG. 3 COORDINATE SYSTEM FOR FREEVI PROGRAM

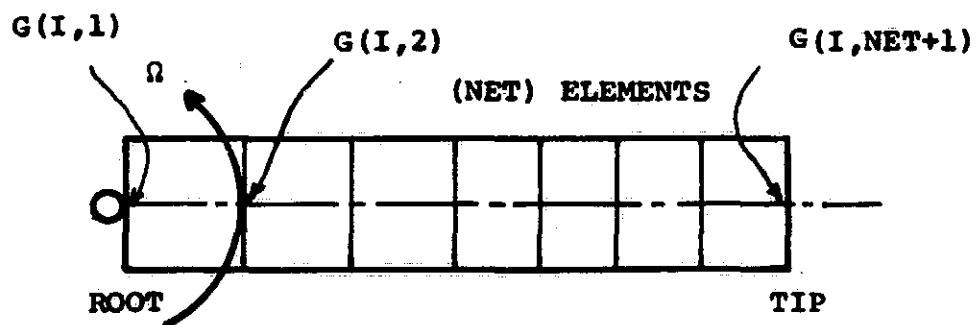


FIG. 4 FINITE ELEMENT REPRESENTATION WITH BEAM ELEMENTS

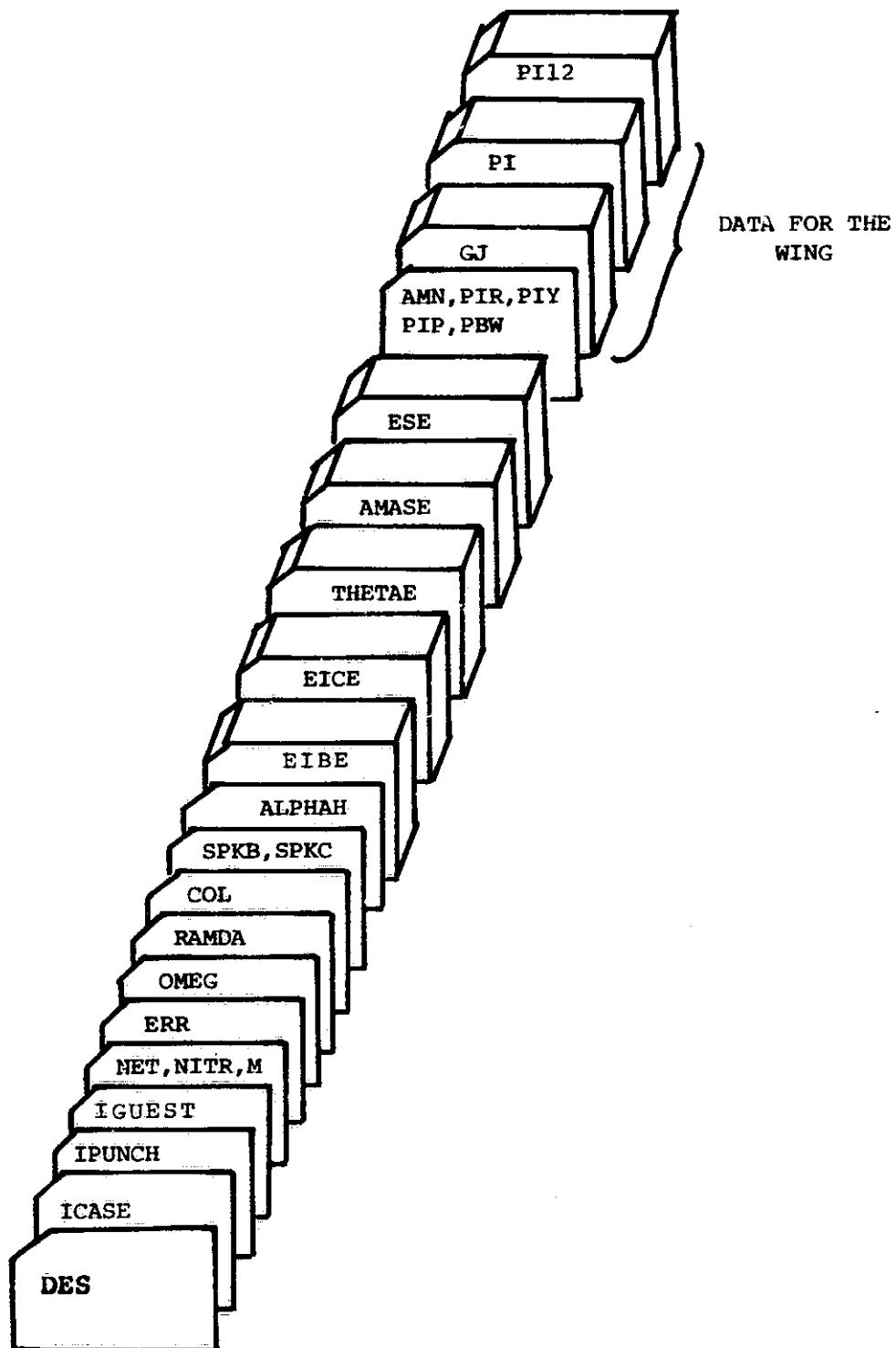
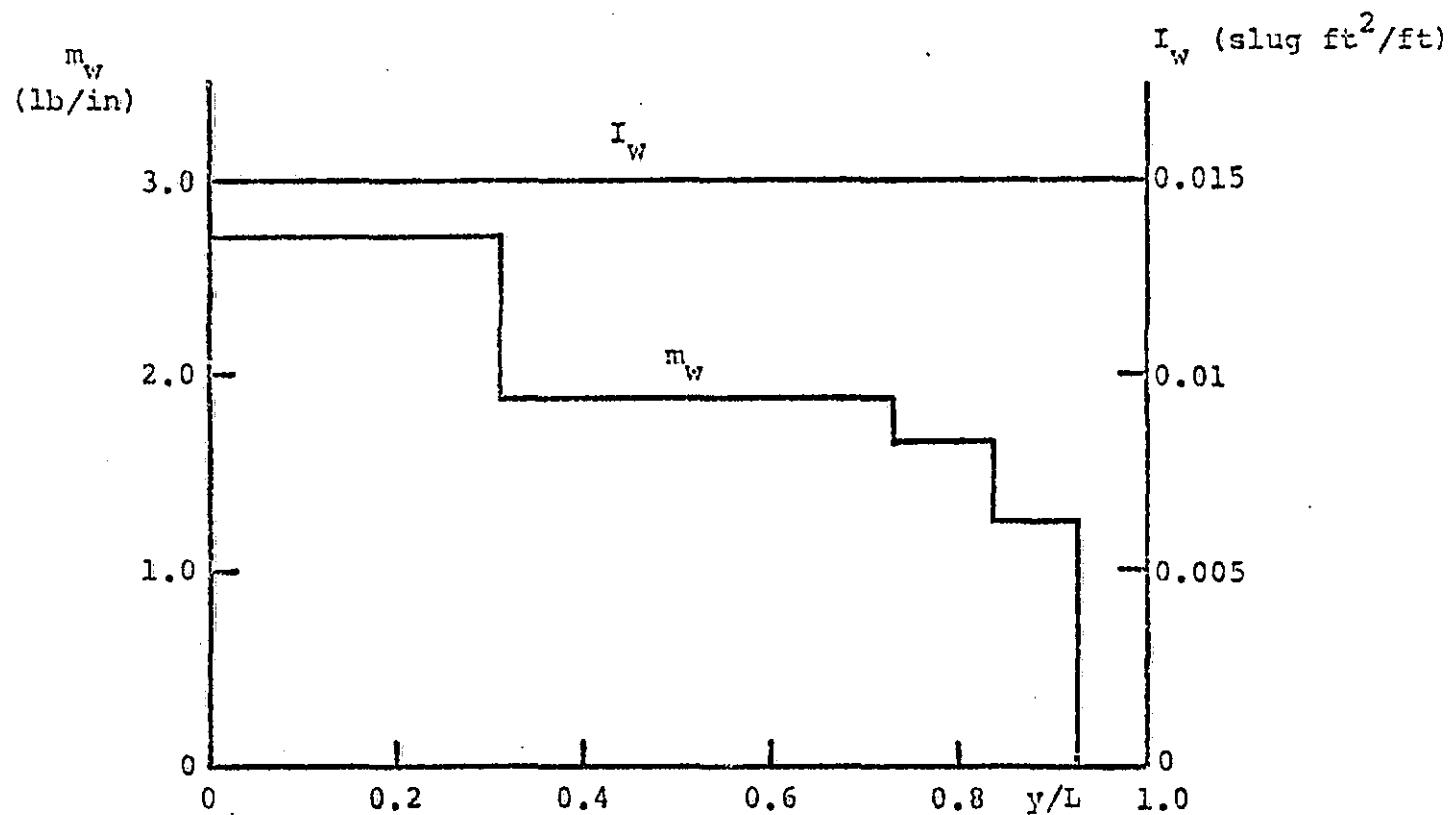
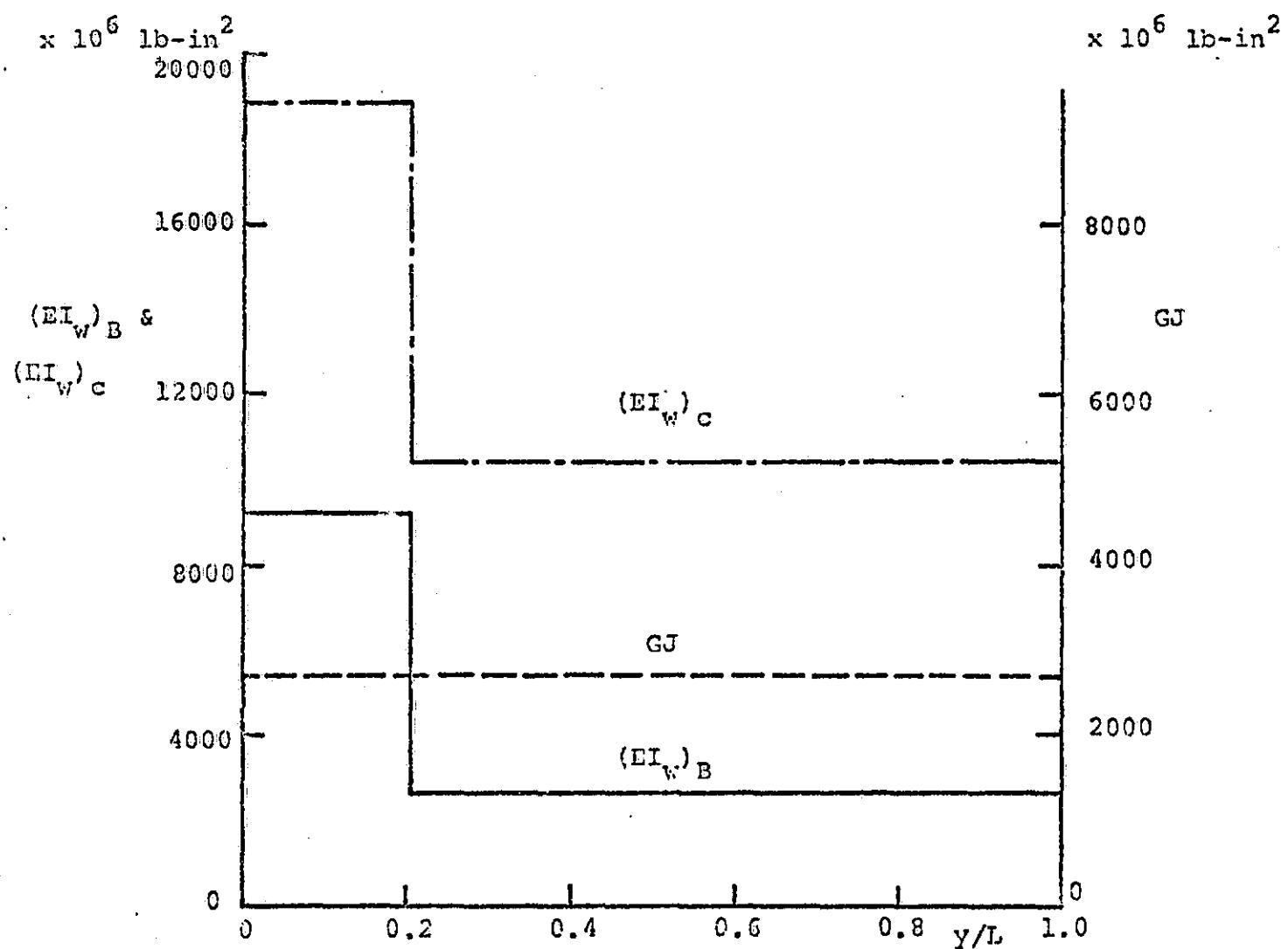


FIG. 5 DATA DECK SETUP FOR THE FREEVI PROGRAM



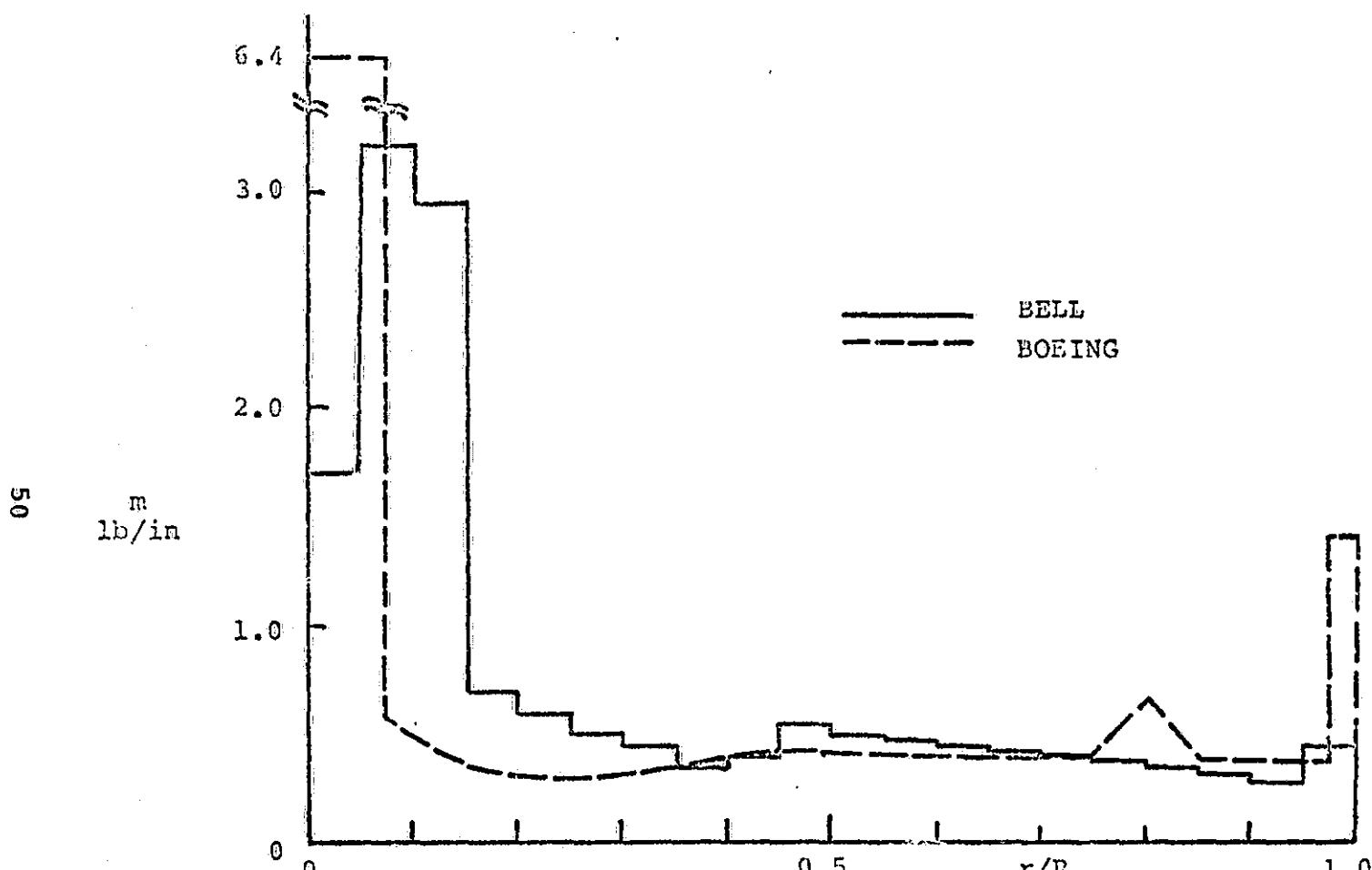
(a) Mass and Cross-Sectional Moment of Inertia Distribution

FIG. 6 STRUCTURAL CHARACTERISTICS OF THE WING



(b) Stiffness Distribution: Vertical Bending Stiffness $(EI_w)_B$,
 Chordwise Bending Stiffness $(EI_w)_C$, and Torsional Rigidity GJ

FIG. 6 CONCLUDED



(a) Section Mass Distribution

FIG. 7 STRUCTURAL CHARACTERISTICS OF TWO PROPROTOR BLADES

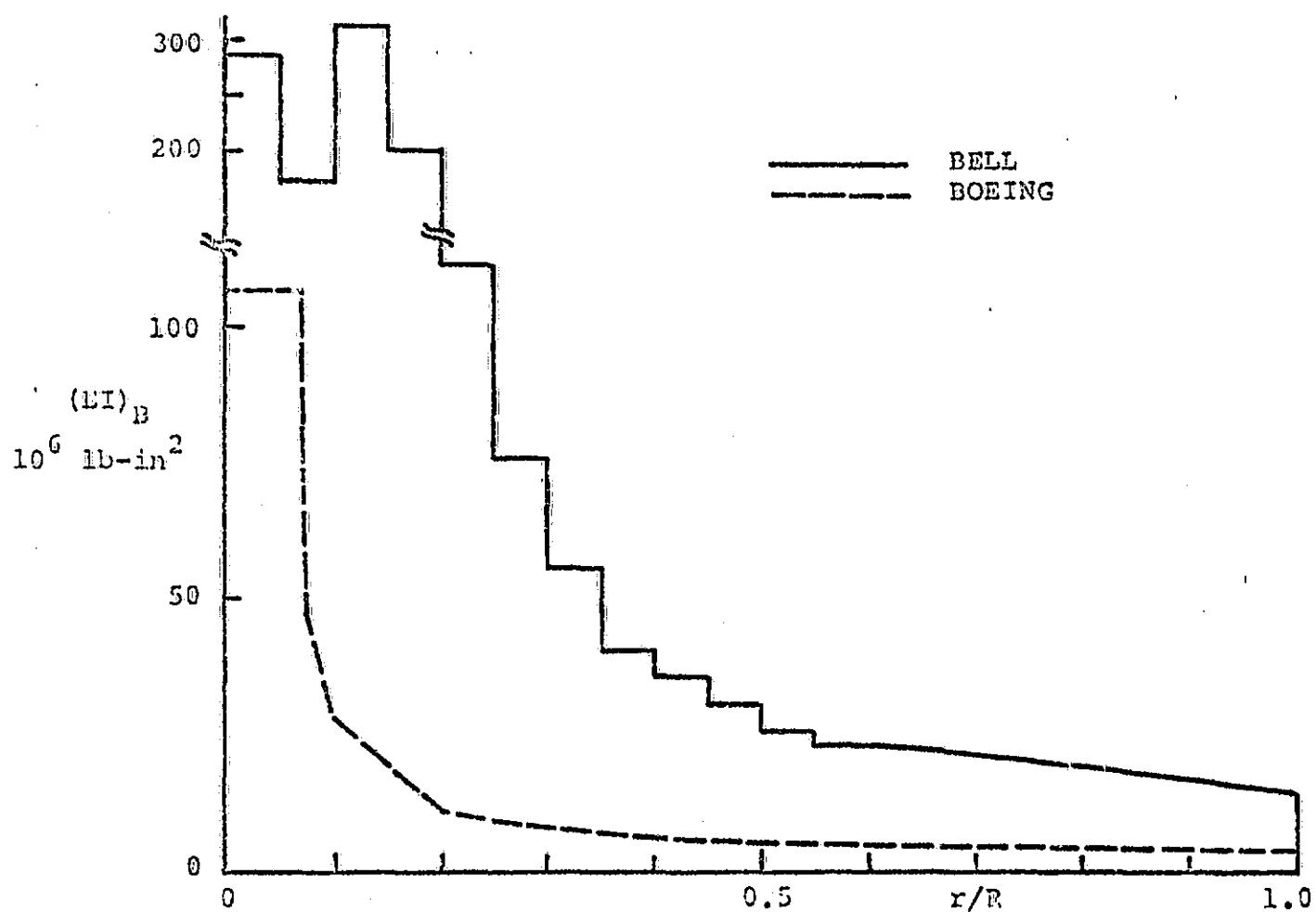
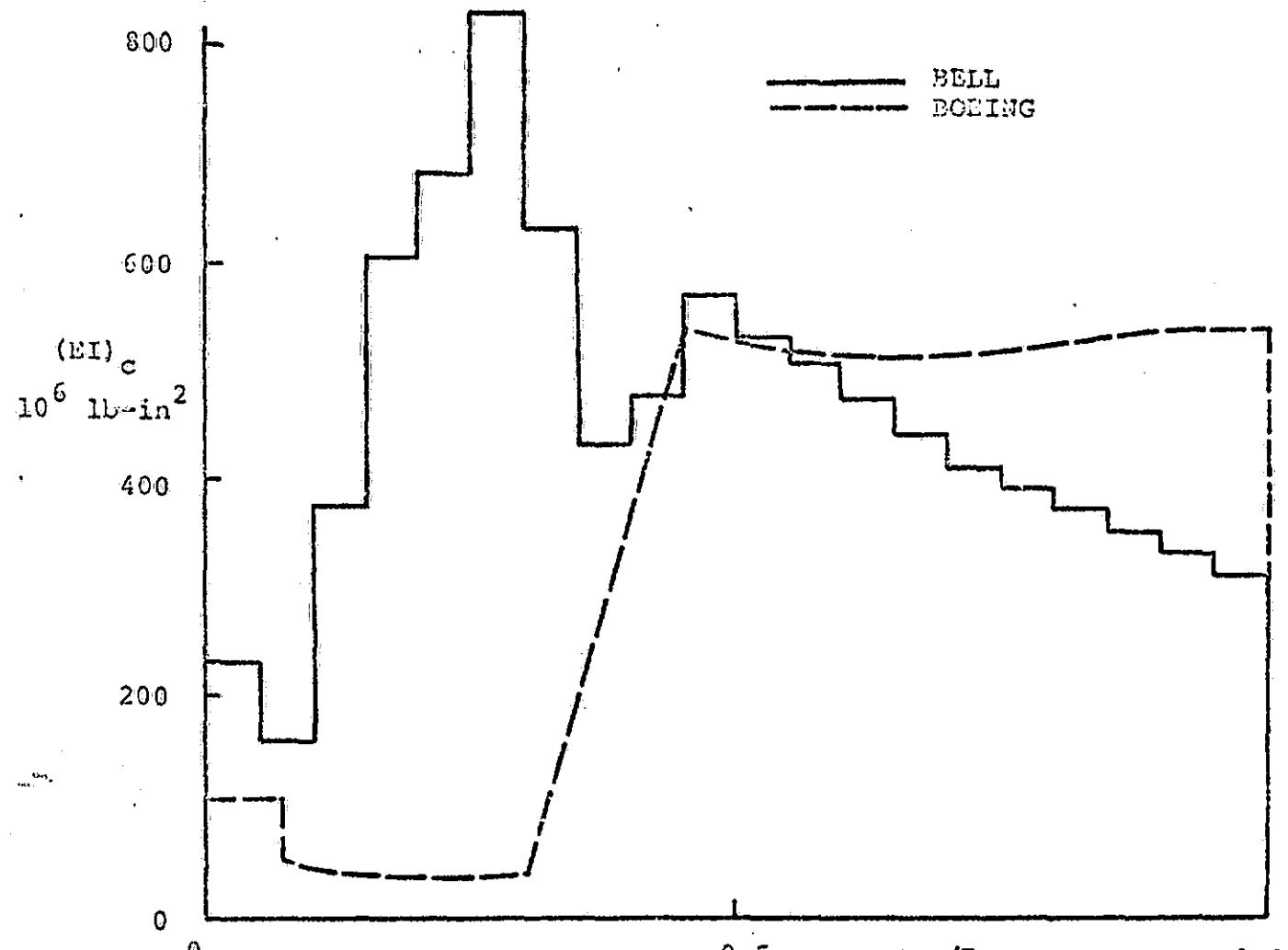
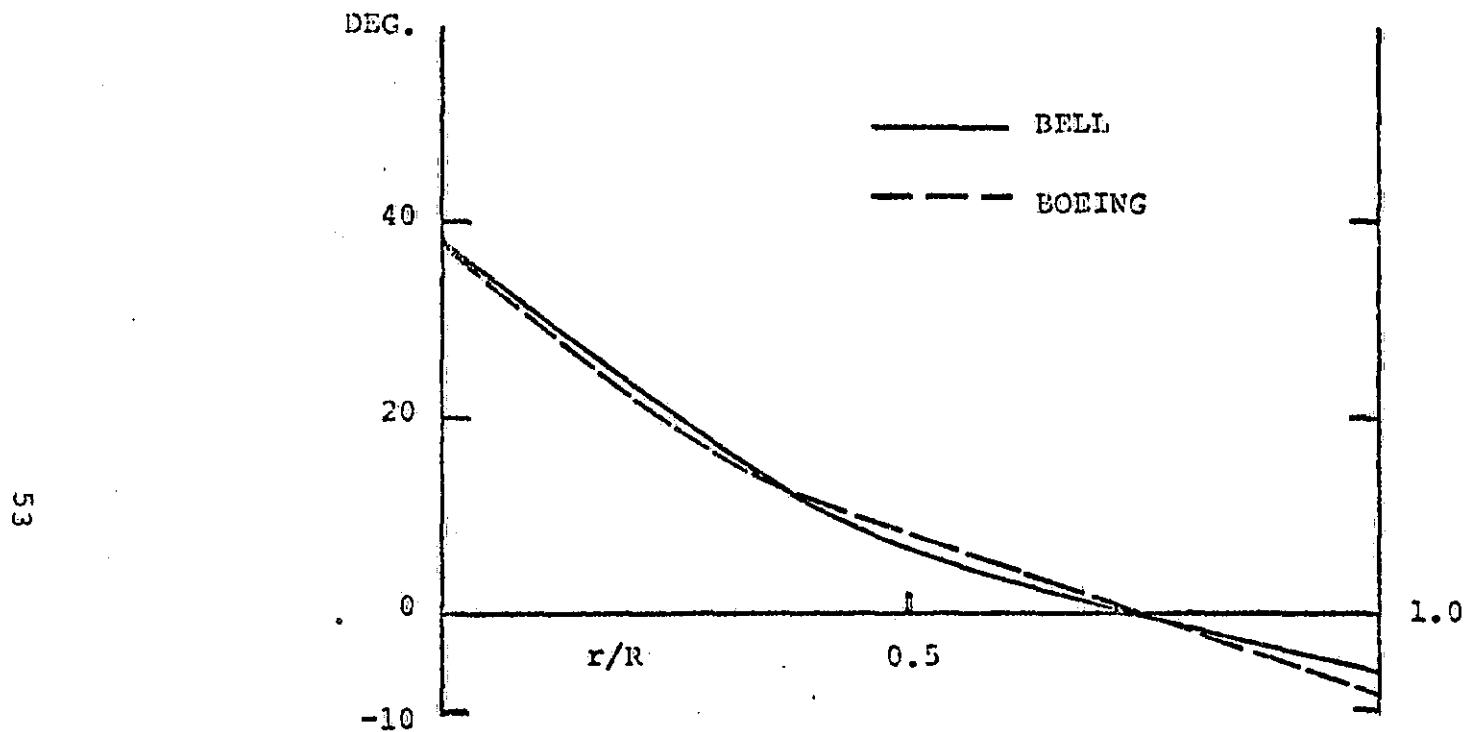


FIG. 7 CONTINUED



(c) Section Chordwise Bending Stiffness Distribution

FIG. 7 CONTINUED



(d) Angle of Twist

FIG. 7 CONCLUDED

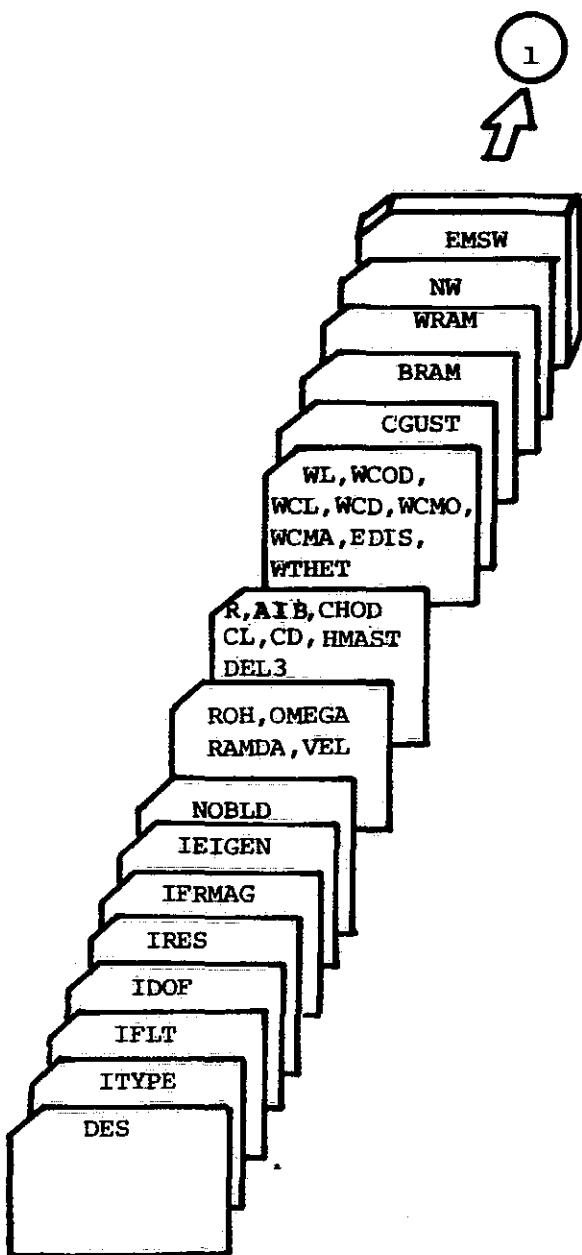


FIG. 8 DATA DECK SETUP FOR THE TILDYN PROGRAM

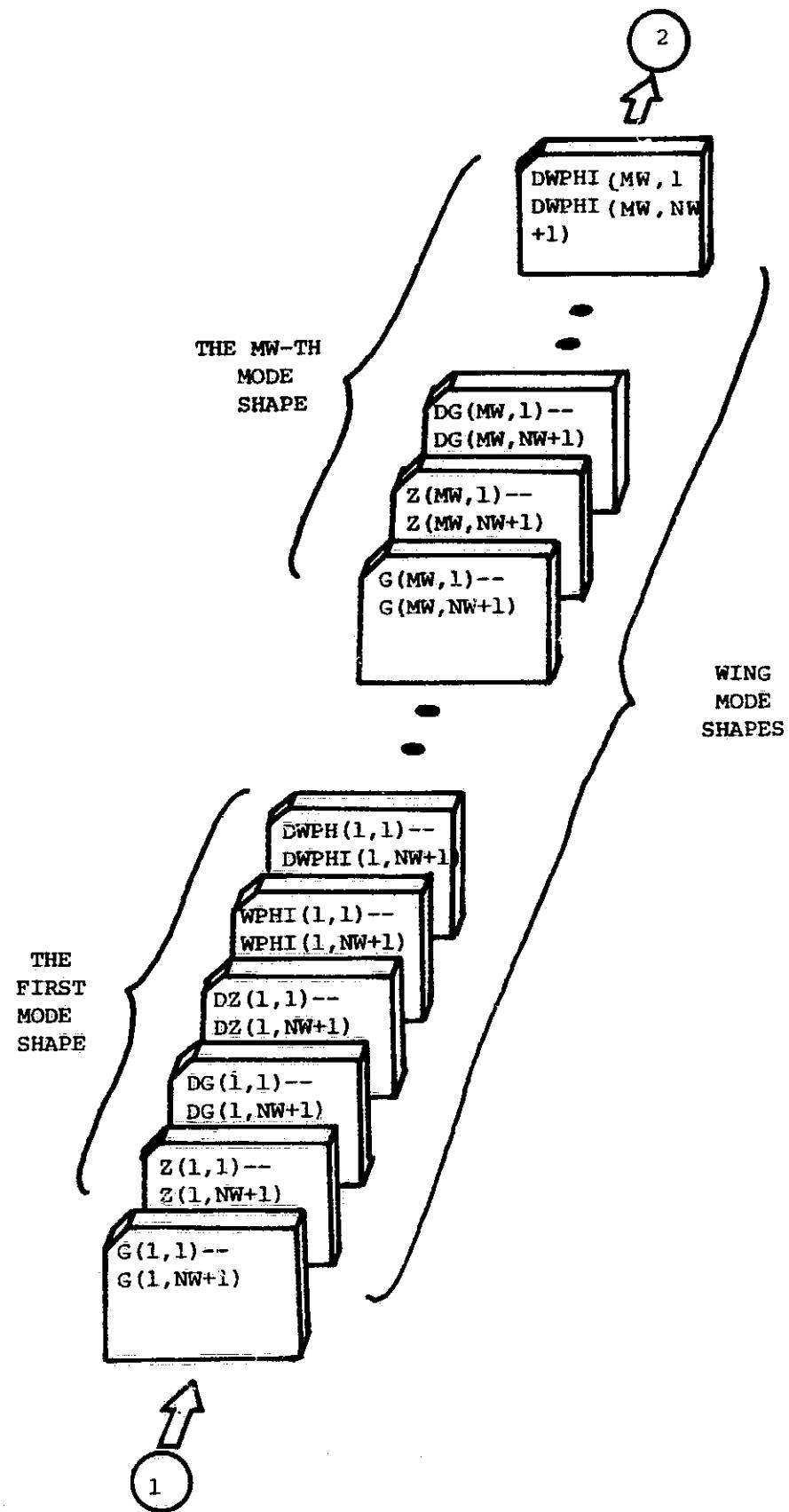


FIG. 8 CONTINUED

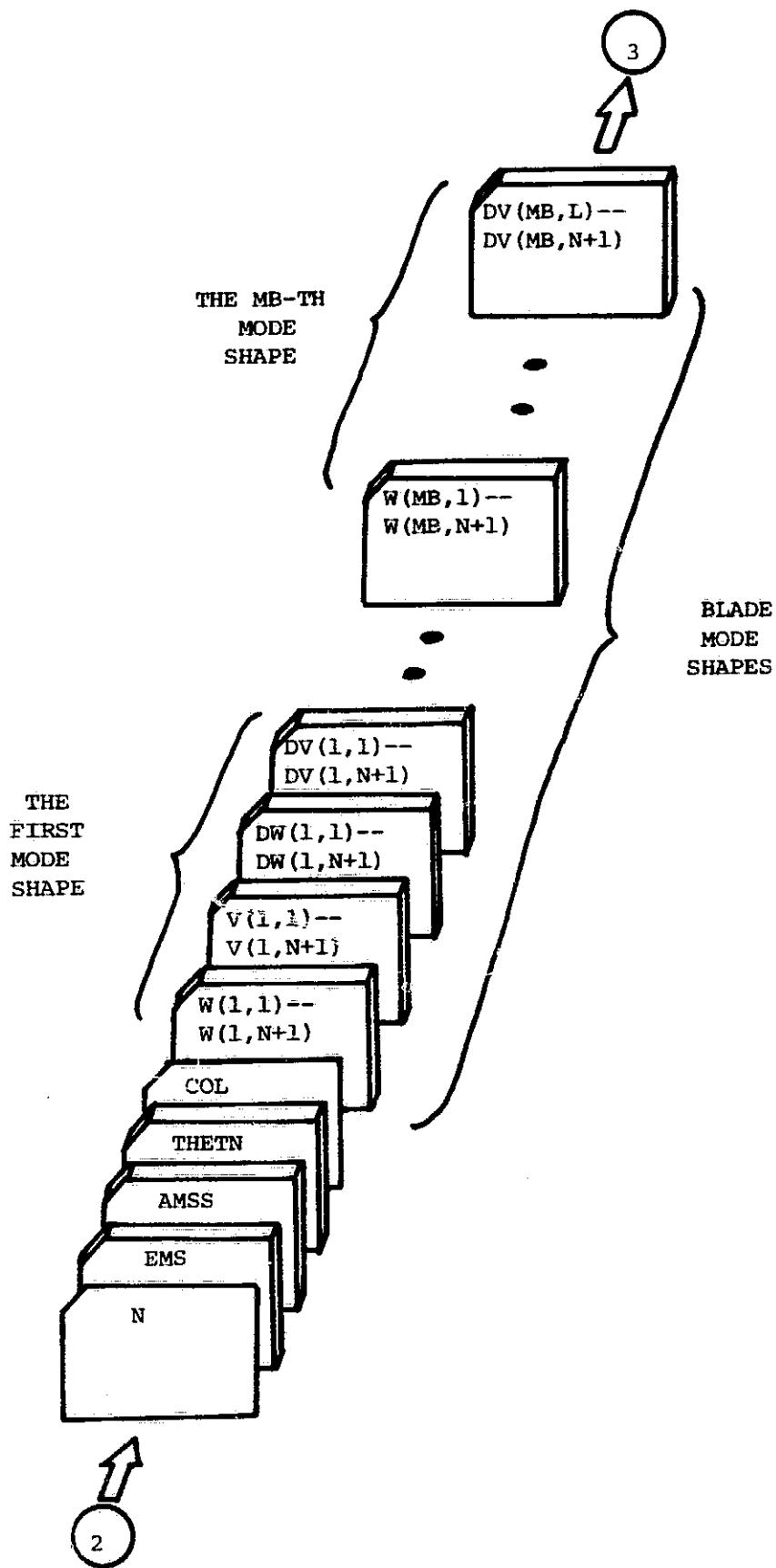
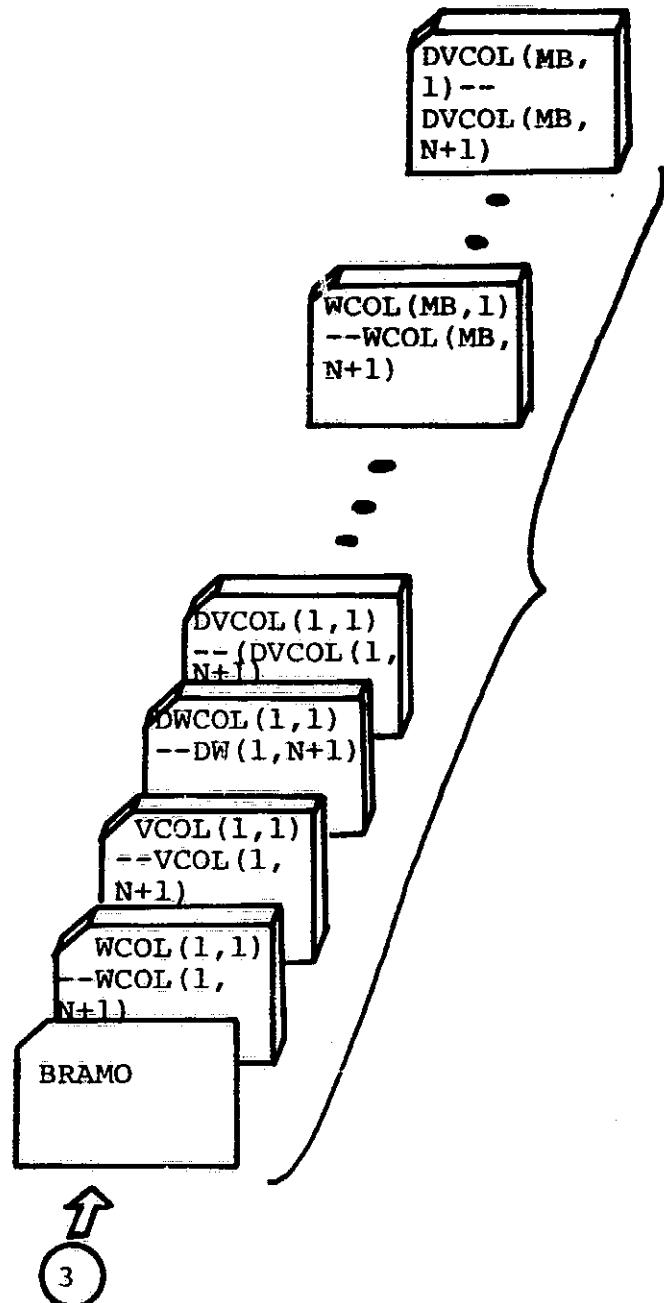


FIG. 8 CONTINUED



BLADE COLLECTIVE
MODE SHAPE DATA
IS FURNISHED IF
THE CASE IS AUTO-
ROTATION FLIGHT
(IFLT=1, ITYPE=1) OR
GIMBALLED ROTOR IN
POWERED FLIGHT (IFLT=0,
ITYPE=1)

FIG. 8 CONCLUDED

APPENDIX A
PROGRAM LISTING

A.1 The FREEVI Program Listing

```

C ***** ****
C
C      PROGRAM  ROTOR
C      PART 1 ;  PROGRAM  FREEVI
C ***** ****
C
C      PURPOSE
C      TO OBTAIN THE NATURAL FREQUENCIES AND MODE SHAPES
C      OF THE ROTOR BLADE AND WING OF THE TILT-ROTOR AIRCRAFT
C
C      DEVELOPED BY MASAHIRO YASUE
C      OF AEROELASTIC AND STRUCTURES RESEARCH LABORATORY
C      AUGUST 1974
C      ADDRESS :  BLG 41-211
C                  MASSACHUSETTS INSTITUTE OF TECHNOLOGY
C                  CAMBRIDGE, MASS. 02139
C
C      IMPLICIT REAL*8(A-H,O-Z)
C      DIMENSION NDPE(20), NNCDE(252), NOD(126), ICOL(126), INUM(126)
C      DIMENSION STK(1550), STM(1550), EK(78), EM(78), XLR(1200), X(1200)
C      DIMENSION Y(1200), U(126), EIG(9), LCH(9), RM(81), RK(81), RV(81)
C      DIMENSION SRM(81), SRK(81)
C      CALL TEIGEN(NDPE,          NOD,NNODE,ICOL,INUM,STK,STM,EK,EM,
1      XLR,U,EIG,LCH,RM,RK,RV,SRM,SRK,X,Y)
C      GO TO 1
C      END
C ***** ****
C      MAIN001
C      MAIN002
C      MAIN003
C      MAIN004
C      MAIN005
C      MAIN006
C      MAIN007
C      MAIN008
C      MAIN009
C      MAIN010
C      MAIN011
C      MAIN012
C      MAIN013
C      MAIN014
C      MAIN015
C      MAIN016
C      MAIN017
C      MAIN018
C      MAIN019
C      MAIN020
C      MAIN021
C      MAIN022
C      MAIN023
C      MAIN024
C      MAIN025
C      MAIN026
C      MAIN027
C      MAIN028
C      MAIN029

```

SUBROUTINE TEIGEN(NDPE, NOO,NNODE,ICOL,INUM,STK,STM,EK
E,EM, XLR,U,EIG,LCH,RM,RK,RV,SRM,SRK,X,Y)

TO CALCULATE THE MORAL MODES AND FREQUENCIES

IMPLICIT REAL*8(A-H,O-Z)

COMMON /BW/ ICASE , IGUEST

COMMON/HELP/ALPHAH

DIMENSION NDPE(1), NBCU(1),NOD(1),NNODE(1),ICOL(1)

DIMENSION INUM(1),STK(1),STM(1),EK(1),EM(1), XLR(1)

DIMENSION U(1),EIG(1),LCH(1)

DIMENSION RM(1),RK(1),RV(1),SRK(1),SRM(1),X(1)

DIMENSION Y(1)

DIMENSION SQU(20),CYC(20)

CALL INPUT(IEQ,NDPE,NET,NDT,MNC,NNODE,NBU, INUM,ERR,NITR,M)

CALL MESH(NDPE,NET,NCT,NCDT,MNC,MN, NOD,NNODE,ICOL,INUM,NBU

INDEX)

IF(INDEX .EQ. 0) GO TO 99

CALL ASBV(STK,STM,IEQ,EK,EM, NDPE,NDT,NCDT,NNODE,MN,NET,INUM)

MA=M

N=NCDT

NP=NCDT*M

MM=M*M

CALL FAC(STK,N,NNDG,ICOL,INUM,U)

IF(NDG .LT. 0) GO TO 99

DO 3 I=1,M

3 EIG(I)= .0

DO 74 K=1,M

II=(K-1)*N

IY=K*2-1

DO 74 I=1,N

IX=IY

IY=IX*65539

IF(IY) 75,76,76

75 IY=IY+2147483647+1

76 YFL=IY

TEIG0001

TEIG0002

TEIG0003

TEIG0004

TEIG0005

TEIG0006

TEIG0007

TEIG0008

TEIG0009

TEIG0010

TEIG0011

TEIG0012

TEIG0013

TEIG0014

TEIG0015

TEIG0016

TEIG0017

TEIG0018

TEIG0019

TEIG0020

TEIG0021

TEIG0022

TEIG0023

TEIG0024

TEIG0025

TEIG0026

TEIG0027

TEIG0028

TEIG0029

TEIG0030

TEIG0031

TEIG0032

TEIG0033

TEIG0034

TEIG0035

TEIG0036

74 XLR(II+II)=YFL*0.46566130-9-0.50+00 TEIG0037
 IF(IGUFST.EQ.0) GO TO 200 TEIG0038
 GO TO (210,220,230,240,220),ICASE TEIG0039
 210 GO TO (310,320,330),IGUEST TEIG0040
 C-----W ONLY TEIG0041
 310 IX=N/6 TEIG0042
 DO 301 K=1,M TEIG0043
 II=NCDT*K-NCDT TEIG0044
 XLR(II+1)=0.0D+00 TEIG0045
 DO 301 KK=1,IX TEIG0046
 JJ=KK*6-5 TEIG0047
 XLR(II+JJ+2)=0.0D+00 TEIG0048
 XLR(II+JJ+4)=0.0D+00 TEIG0049
 XLR(II+JJ+5)=0.0D+00 TEIG0050
 301 XLR(II+JJ+6)=0.0D+00 TEIG0051
 GO TO 200 TEIG0052
 C-----V ONLY TEIG0053
 320 IX=N/6 TEIG0054
 DO 302 K=1,M TEIG0055
 II=NCDT*K-NCDT TEIG0056
 XLR(II+1)=0.0D+00 TEIG0057
 DO 302 KK=1,IX TEIG0058
 JJ=KK*6-5 TEIG0059
 XLP(II+JJ+1)=0.0D+00 TEIG0060
 XLP(II+JJ+3)=0.0D+00 TEIG0061
 XLP(II+JJ+5)=0.0D+00 TEIG0062
 302 XLP(II+JJ+6)=0.0D+00 TEIG0063
 GO TO 200 TEIG0064
 C-----PHI ONLY TEIG0065
 330 IX=N/6 TEIG0066
 DO 303 K=1,M TEIG0067
 II=NCDT*K-NCDT TEIG0068
 DO 303 KK=1,IX TEIG0069
 JJ=KK*6-5 TEIG0070
 DO 303 KKK=1,4 TEIG0071
 303 XLP(II+JJ+KKK)=0.0D+00 TEIG0072

GO TO 200 TEIGO073
 220 GO TO (221,222),IGUEST TEIGO074
 C----W ONLY TEIGO075
 221 IX=N/2 TEIGO076
 DO 201 K=1,M TEIGO077
 II=N*K-N TEIGO078
 DO 201 I=1,IX TEIGO079
 201 XLR(II+2*I)=0.000 TEIGO080
 GO TO 200 TEIGO081
 C----V ONLY TEIGO082
 222 IX=N/2 TEIGO083
 DO 202 K=1,M TEIGO084
 II=K*N-N TEIGO085
 DO 202 I=1,IX TEIGO086
 202 XLR(II+2*I-1)=0.000 TEIGO087
 GO TO 200 TEIGO088
 230 GO TO (231,232),IGUEST TEIGO089
 C----W ONLY TEIGO090
 231 IX=N/2 TEIGO091
 DO 233 K=1,M TEIGO092
 II=N*K-N TEIGO093
 XLR(II+1)=0.000 TEIGO094
 DO 233 KK=1,IX TEIGO095
 233 XLR(II+2*KK+1)=0.000 TEIGO096
 GO TO 200 TEIGO097
 C----V ONLY TEIGO098
 232 IX=N/2 TEIGO099
 DO 234 K=1,M TEIGO100
 II=N*K-N TEIGO101
 DO 234 KK=1,IX TEIGO102
 234 XLR(II+2*KK)=0.000 TEIGO103
 GO TO 200 TEIGO104
 240 GO TO (241,242),IGUEST TEIGO105
 C----W ONLY TEIGO106
 241 IX=N/2 TEIGO107
 DO 243 K=1,M TEIGO108

63
 II=N*K-N TEIG0109
 DO 243 KK=1,IX TEIG0110
 243 XLR(II+2*KK+1)=0.000 TEIG0111
 GO TO 200 TEIG0112
 C-----V ONLY TEIG0113
 242 IX=N/2 TEIG0114
 DO 244 K=1,M TEIG0115
 II=N*K-N TEIG0116
 XLR(II+1)=0.000 TEIG0117
 DO 244 KK=1,IX TEIG0118
 244 XLR(II+2*KK)=0.000 TEIG0119
 200 CONTINUE TEIG0120
 IST=1 TEIG0121
 DO 21 KKK=1,NITR TEIG0122
 IT=(IST-1)*N+1 TEIG0123
 DO 1 I=IT,MM TEIG0124
 1 Y(I)=XLR(I) TEIG0125
 CALL SOLZ(STK,Y,N,M-IST+1,ICOL,INUM,IST) TEIG0126
 DO 11 K=IST,M TEIG0127
 K1=K-1 TEIG0128
 II=(K-1)*N TEIG0129
 XM=0.0 TEIG0130
 LCH(K)=0 TEIG0131
 DO 7 I=1,N TEIG0132
 D=DABS(Y(II+I)) TEIG0133
 IF(D-XM)7,7,S TEIG0134
 9 XM=D TEIG0135
 LCH(K)=I TEIG0136
 7 CONTINUE TEIG0137
 IF(LCH(K) .EQ. 0) GO TO 99 TEIG0138
 E=Y(II+LCH(K)) TEIG0139
 E=1.0/E TEIG0140
 DO 11 I=1,N TEIG0141
 III=I+II TEIG0142
 Y(III)=Y(III)*E TEIG0143
 11 XLR(III)=XLR(III)*E TEIG0144

```

CALL MTRTR(M,N,RK,Y,XLR,IST)          TEIGO145
DO 31 I=1,M                            TEIGO146
31 X(I)=Y(I)                          TEIGO147
CALL MLLTZ(STM,X,U,N,M-IST+1,ICOL,INUM,IST)  TEIGO148
CALL MTRTR(M-N,RM,Y,X,IST)            TEIGO149
DO 39 I=1,MM                          TEIGO150
SRM(I)=RM(I)                         TEIGO151
39 SRK(I)=RK(I)                      TEIGO152
CALL DNRROT(M,RM,RK,U,RV)            TEIGO153
DO 40 I=1,M                          TEIGO154
40 U(I)=1./U(I)-ALPHAH              TEIGO155
WRITE(6,41) (U(I),I=1,M)            TEIGO156
41 FORMAT(12X,'EIGENVALUES=',/,12X,10D13.5)  TEIGO157
DO 22 I=IST,MA                      TEIGO158
IST=I                                TEIGO159
IF(DABS(EIG(I))/U(I)-1.0) .GT. ERR) GO TO 23
22 CONTINUE                           TEIGO160
DC 504 I=1,M                          TEIGO161
SQU(I)=ESQRT(DABS(U(I)))            TEIGO162
CYC(I)=SCU(I)*0.5D0/3.141592D0    TEIGO163
504 CONTINUE                           TEIGO164
WRITE(6,505)(SQU(I),I=1,M)          TEIGO165
505 FORMAT(15X,'RADIAN/SEC',/,12X,10D13.5)  TEIGO166
506 FORMAT(15X,'HERTZ      ',/,12X,10D13.5)  TEIGO167
WRITE(6,506)(CYC(I),I=1,M)          TEIGO168
DO 10 I=1,NCDT                      TEIGO169
DO 10 J=1,M                          TEIGO170
JJ=(J-1)*NCDT                      TEIGO171
XLR(I+JJ)=0.0                         TEIGO172
DO 10 K=1,M                          TEIGO173
10 XLR(I+JJ)=XLR(I+JJ)+Y(I+(K-1)*N)*RV((J-1)*M+K)  TEIGO174
DO 15 I=1,M                          TEIGO175
II=(I-1)*M                           TEIGO176
DO 15 J=1,M                          TEIGO177
JJ=(J-1)*M                           TEIGO178
IJ=JJ+I                             TEIGO179

```

```

PM(IJ)=0.0 TEIGO181
RK(IJ)=0.0 TEIGO182
DO 15 K=1,M TEIGO183
  KK=(K-1)*M TEIGO184
  RM(IJ)=RM(IJ)+SRM(KK+I)*RV(JJ+K) TEIGO185
15  RK(IJ)=RK(IJ)+SRK(KK+I)*RV(JJ+K) TEIGO186
    CALL MTRTR(M,M,SRM,RV,RM,1) TEIGO187
    CALL MTRTR(M,M,SRK,RV,RK,1) TEIGO188
    DO 42 I=1,M TEIGO189
      KK=M*I-M+I TEIGO190
      Y(I)=1./DSQRT(SRM(KK)) TEIGO191
      II=I*NCDT-NCDT TEIGO192
      DO 42 J=1,NCDT TEIGO193
42    XLR(II+J)=XLR(II+J)*Y(J) TEIGO194
      DO 17 I=1,M TEIGO195
        KK=I*M-M TEIGO196
        DO 17 J=1,I TEIGO197
          E=Y(I)*Y(J) TEIGO198
          IJ=KK+J TEIGO199
          SRM(IJ)= E*SRM(IJ) TEIGO200
17    SRK(IJ) = E*SRK(IJ) TEIGO201
      CALL      OUTPUT(KKK,M,NCDT,NDT,NOD,NNODE,ERR,XLR,U,SRM,SRK) TEIGO202
      GO TO 99 TEIGO203
23    DO 25 I=1,M TEIGO204
25    EIG(I)= U(I) TEIGO205
      IF(IST.EQ.1) GO TO 45 TEIGO206
      IQ=IST-1 TEIGO207
      DO 44 I=1,IQ TEIGO208
        II=(I-1)*M TEIGO209
        DO 44 J=1,IQ TEIGO210
          IJI=II+J TEIGO211
          RM(IJI)=SRM(IJI) TEIGO212
44    RK(IJI)=SRK(IJI) TEIGO213
45    CONTINUE TEIGO214
      DO 34 I=1,N TEIGO215
      DO 34 J=IST,M TEIGO216

```

```
JJ=(J-1)*N          TEIGO217
XLR(I+JJ)=0.0       TEIGO218
DO 34 K=1,M          TEIGO219
34 XLR(I+JJ)=XLR(I+JJ)+X(I+(K-1)*N)*RV((J-1)*M+K)  TEIGO220
21 CONTINUE          TEIGO221
WRITE(6,26) KKK      TEIGO222
26 FFORMAT(/2X,'NO. OF ITERATION=',I4,2X,'NOT CONVERGED') TEIGO223
55 RETURN            TEIGO224
END                 TEIGO225
```

SUBROUTINE INPUT(IEQ,NDPE,NET,NDT,MNC,NODE,NBU,NBCU,ERR,NITR,M) INPU0001

TO SUPPLY INPUT INFORMATION INPU0002

DES COMMENTS AND DESCRIPTIONS INPU0003

ICASE=1 WING INPU0004

ICASE=2 BLADE B.C. CANTILEVER+CANTILEVER INPU0005

ICASE=3 BLADE B.C. CANTILEVER+HINGE INPU0006

ICASE=4 BLADE B.C. HINGE+CANTILEVER INPU0007

ICASE=5 BLADE B.C. HINGE+HINGE INPU0008

IPUNCH=0 NO PUNCH OUTPUT INPU0009

IPUNCH=1 PUNCH OUTPUT INPU0010

IGUEST=0 COUPLED MODE SHAPES GENERATED INPU0011

IGUEST=1 W DEFLECTION ONLY INPU0012

IGUEST=2 V DEFLECTION ONLY INPU0013

IGUEST=3 PHI DEFLECTION ONLY INPU0014

--CAUTION-- TO DERIVE UNCOUPLED MODES, COUPLING TERMS SHOULD BE INPU0015

--CAUTION-- SET AT ZERO. INPU0016

--CAUTION-- PR IN THE WING, RAMDA,COL,THETAF IN THE BLADE INPU0017

NET NO OF ELEMENTS INPU0018

NTTR = NO OF ITERATION ALLOWED INPU0019

M= NO OF MODES WANTED INPU0020

ERR ERROR TOLERANCE FOR ITERATION INPU0021

OMEG ROTATION FREQ IN RAD / SEC INPU0022

RAMDA=INFLOW RATIO INPU0023

COL=COLLECTIVE PITCH ANGLE DETERMINED BY PERFORMANCE ANALYSIS INPU0024

SPKB,SPKC =SPRING CONSTANT OF THE HINGED PLADE (BEAMWISE
E CHORDWISE) INPU0025

ALPHAH=HELPER TO AVOID THE SINGULARITY OF THE STIFFNESS MATRIX INPU0026

EIBE= EI FOR SPANWISE BENDING INPU0027


```

1 PIR,PIY,PIP,PBW,BM,BI,R,NETT          INPU0073
DIMENSION DES(20)                      INPU0074
10 FORMAT (16I5)                         INPU0075
1   FORMAT (8E10.6)                      INPU0076
4 FORMAT(5E15.7)                        INPU0077
149 FORMAT(20A4)                         INPU0078
150 FORMAT(11)                           INPU0079
1E0=0                                     INPU0080
READ(5,149)(DES(I),I=1,20)              INPU0081
READ(5,150)ICASEF                      INPU0082
READ(5,150)IPUNCH                      INPU0083
READ(5,150)      TQUEST                INPU0084
READ(5,10)      NET,NITR,M              INPU0085
TF(ICASE, EQ.1)  GO TO 192              INPU0086
NDFN=4                                     INPU0087
GO TO 193                                INPU0088
192  NDFN=6                               INPU0089
9 193  CONTINUE                           INPU0090
NETT=NET                                 INPU0091
READ(5,1) ERR                           INPU0092
READ(5,1) QMEG                           INPU0093
READ(5,1) RAMDA                          INPU0094
READ(5,1) COL                            INPU0095
READ(5,1) SPKR,SPKC                      INPU0096
READ(5,1)      ALPHAH                INPU0097
READ(5,4) (  SIRF(I),I=1,NET)          INPU0098
READ(5,4) (  ETCE(I),I=1,NET)          INPU0099
READ(5,1) ( THETAF(I),I=1,NET)          INPU0100
READ(5,1) (  AMASE(I),I=1,NET)          INPU0101
READ(5,1) (  ESE(I),I=1,NET)           INPU0102
READ(5,1)  AMN,PIP,PIY,PTP,PBW          INPU0103
TF ( NDFN .EQ. 4) GO TO 100             INPU0104
READ(5,4) ( GJ(I),I=1,NET)              INPU0105
READ(5,4) ( PI(I),I=1,NET)              INPU0106
READ(5,4) ( PI12(I),I=1,NET)            INPU0107
100  CONTINUE                           INPU0108

```

```

181  WRITE(6,181)
181  FORMAT(//5X,45(1H*1)/)
181  GO TO (151,152,153,154,155),ICASE
151  WRITE(6,171)
171  FORMAT(9X,'WING')
171  GO TO 180
152  WRITE(6,172)
172  FORMAT(9X,'BLADE',3X,'BEAM*CANTI',3X,'CHORD*CANTI')
153  GO TO 180
153  WRITE(6,173)
173  FORMAT(9X,'BLADE',3X,'BEAM*CANTI',3X,'CHORD*HINGE')
154  GO TO 180
154  WRITE(6,174)
174  FORMAT(9X,'BLADE',3X,'BEAM*HINGE',3X,'CHORD*CANTI')
155  GO TO 180
155  WRITE(6,175)
175  FORMAT(9X,'BLADE',3X,'BEAM*HINGE',3X,'CHORD*HINGE')
180  CONTINUE
180  WRITE(6,182)(DES(I),I=1,20)
182  FORMAT(/5X,45(1H*1)//15X,20A4//)
182  WRITE(6,9)
182  WRITE(6,6(1))IPUNCH ,IGUEST
600  FORMAT(1X,'IPUNCH=',I1 ,5X,'IGUEST=',I1)
600  WRITE(6,16)NDPM, NFT,NITR,M,EPR
600  WRITE(6,114)OMEG
114  FORMAT(6H OMEG=,F15.5)
114  WRITE(6,300)RAMDA
300  FORMAT(8H LAMRDA=,F15.5)
300  WRITE(6,301)COL
301  FORMAT(18H COLLECTIVE PITCH=,F15.5)
301  WRITE(6,299)SPKR,SPKC
299  FORMAT(1X,'SPRING= ',F15.5,F15.5)
299  WRITE(6,298)ALPHAH
298  FORMAT(1X,'ALPHAH= ',D15.5)
298  WRITE(6,183)
183  FORMAT(1X,'--FLAPPING RENDING STIFFNESS--')

```

```

      WRITE(6,105) ( EIBE(I),I=1,NET)           INPU0145
      WRITE(6,184)                               INPU0146
184   FORMAT(1X,'--CHORDWISE BENDING STIFFNESS--')
      WRITE(6,105) ( EICE(I),I=1,NET)           INPU0147
      WRITE(6,185)                               INPU0148
185   FORMAT(1X,'--ANGLE OF TWIST--')
      WRITE(6,104) ( THETAE(I),I=1,NFT)         INPU0149
      THE=ATAN(R4MDA*4.0/3.0)+COL.*SIGN(1.0,0MEG)
      DO 302 I=1,NFT
302   THETAF(I)=THETAE(I)*SIGN(1.0,0MEG)+THE
      WRITE(6,186)
186   FORMAT(1X,'--MASS DISTRIBUTION--')
      WRITE(6,104) ( AMASE(I),I=1,NET)           INPU0150
      WRITE(6,188)
188   FORMAT(1X,'--ELEMENT SIZE--')
      WRITE(6,104) ( ESE(I),I=1,NET)             INPU0151
      WRITE(6,187)
187   FORMAT(8X,'TIP MASS',T19,'ROLL INERTIA',T34,'YAW INERTIA',
71      &          T49,'PITCH INERTIA',T64,'MASS COUPLING')
      WRITE(6,104) AMN,PIR,PIY,PIP,PBW
      NN=NET+1
104   FORMAT(8F15.5)
105   FORMAT(5X,7E15.7)
      IF (NDPN .EQ. 4) GO TO 14
      WRITE(6,189)
189   FORMAT(1X,'--TORSIONAL RIGIDITY--')
      WRITE(6,105) ( GJ(I),I=1,NET)             INPU0160
      WRITE(6,190)
190   FORMAT(1X,'--MOIMENT OF INERTIA--')
      WRITE(6,105) ( OT(I),I=1,NET)             INPU0161
      WRITE(6,191)
191   FORMAT(1X,'--MASS COUPLING ALONG SPAN--')
      WRITE(6,105) ( PI12(I),I=1,NET)            INPU0162
9     FORMAT(1/8H * * * /12H INPUT DATA //)
16     FORMAT(25H NO OF DEGRE PER NODE=      , I3/
1     17H NO OF ELEMENTS=,I3/24H NO OF MAX ITER ALLOWED=,I3
                                         INPU0163
                                         INPU0164
                                         INPU0165
                                         INPU0166
                                         INPU0167
                                         INPU0168
                                         INPU0169
                                         INPU0170
                                         INPU0171
                                         INPU0172
                                         INPU0173
                                         INPU0174
                                         INPU0175
                                         INPU0176
                                         INPU0177
                                         INPU0178
                                         INPU0179
                                         INPU0180

```

2 /14H NO OF MODES=, 13/ 6H ERR=, F15.51 INPU0181
 14 NDE=NDPN+NDPN INPU0182
 NDT=NFT*NDPN+NDPN INPU0183
 MNC=NDT*NDE-(NDE*NDE-NDE)/2 INPU0184
 DO 5 I=1,NFT INPU0185
 NDE(I)=NDE INPU0186
 NII=NDE*I-NDE INPU0187
 NDD=NDPN*I-NDPN INPU0188
 NODE(NII+1)=NDD+1 INPU0189
 NCDE(NII+5)=NDD+2 INPU0190
 NODE(NII+2)=NDD+3 INPU0191
 NODE(NII+6)=NDD+4 INPU0192
 NODE(NII+3)=NDD+NDPN+1 INPU0193
 NODE(NII+7)=NDD+NDPN+2 INPU0194
 NODE(NII+4)=NDD+NDPN+3 INPU0195
 NCDE(NII+8)=NDD+NDPN+4 INPU0196
 IF (NDPN EQ 4) GO TO 5 INPU0197
 NODE(NII+9)=NDD+5 INPU0198
 NODE(NII+10)=NDD+6 INPU0199
 NODE(NII+11)=NDD+NDPN+5 INPU0200
 NODE(NII+12)=NDD+NDPN+6 INPU0201
 5 CONTINUE INPU0202
 GO TO (501,502,503,504,505),ICASE INPU0203
 501 NBU=NDPN-1 INPU0204
 GO TO 506 INPU0205
 502 NBU=4 INPU0206
 506 DO 6 I=1,NBU INPU0207
 6 NBCU(I)=1 INPU0208
 GO TO 507 INPU0209
 503 NBU=3 INPU0210
 NBCU(1)=1 INPU0211
 NBCU(2)=2 INPU0212
 NBCU(3)=3 INPU0213
 GO TO 507 INPU0214
 504 NBU=3 INPU0215
 NBCU(1)=1 INPU0216

```

      NBCU(2)=2          INPU0217
      NBCU(3)=4          INPU0218
      GO TO 507          INPU0219
505      NBCU=2          INPU0220
      NBCU(1)=1          INPU0221
      NBCU(2)=2          INPU0222
507      CONTINUE        INPU0223
      R=0                INPU0224
      DO 2 I=1,NET        INPU0225
2      R=R+ESE(I)
      TN(NET+1)=AMN*R*OMEG*OMEG
      DO 3 I=1,NET
3      II=NET-I+1
      P=R-ESE(II)
      TN(II)= TN(II+1) +AMASE(II)*(R+.5*ESE(II)) *ESE(II)*OMFG*OMEG
      WRITE (6,15)
      WRITE(6,104) (   TN(I),I=1,NN)
      FORMAT(///' TENSION DUE TO CENTRIF FORCE')
      15      R=0.
      73      BI=0.
      RM=0
      DO 11 I=1,NFT
      BM=BM+ AMASE(I)*ESE(I)
      RR=R+ESE(I)
      BI= BI+ AMASE(I)*(PR**3-R**3)*.3333333
      11      R=RR
      BM=RM+AMN
      RI=BI+AMN*R**R
      WRITE (6,12) BM,BI,R
      12      FORMAT(/' MASS =',E13.5/ ' MOMENT OF INERTIA AT ROOT=',F13.5/
      1 ' TOTAL LENGTH OF THE BEAM=',F13.5)
      RETURN
      END

```

SUBROUTINE ELEMK (EKT, EMT, NDE, NE)

ELEM0001

C TO CONTROL THE GENERATION OF ELEMENT STIFFNESS AND MASS
C MATRICES

ELEM0002

C NDE=8 FOR BLADE MODE

ELEM0003

C NDE=12 FOR WING MODE

ELEM0004

CCMMON/SPRING/SPKH,SPKC

ELEM0005

CCMMON/HELP/ALPHAH

ELEM0006

DCUBLE PRECISION ALPHAH

ELEM0007

DOUBLE PRECISION EKT,EMT

ELEM0008

DIMENSION EKC(4,4), ETC(4,4), EMC(4,4), EKT(1), EMT(1)

ELEM0009

DIMENSION EIBE(20), EICE(20), THETAE(20), AMASE(20), ESE(20), TN(21)

ELEM0010

DIMENSION GJ(20), PI(20), PI12(20)

ELEM0011

COMMON /ELEM/ OMEG, EIBE, EICE, THETAE, AMASE, ESE, TN, GJ, PI, PI12, AMN,

ELEM0012

1 PIR, PIY, PIP, PBW, BM, BI, R, NETT

ELEM0013

NET=NETT

ELEM0014

EIB=EIBE(NE)

ELEM0015

EIC=EICE(NE)

ELEM0016

THETA=THETAE(NE)

ELEM0017

AMAS=AMASE(NE)

ELEM0018

ES=ESE(NE)

ELEM0019

T= (TN(NE)+ TN(NE+1))*.5

ELEM0020

ESS=ES*ES

ELEM0021

IF (NDE .EQ. 8) GO TO 9

ELEM0022

GJE=GJ(NE)/ES

ELEM0023

PIE=PI(NE) *ES

ELEM0024

PI12E=PI12(NE) *ES

ELEM0025

EKC(1,1)=12.

ELEM0026

EKC(2,1)=6.*ES

ELEM0027

EKC(3,1)=-12.

ELEM0028

EKC(4,1)=6.*ES

ELEM0029

EKC(2,2)=4.*ESS

ELEM0030

EKC(3,2)=-6.*ES

ELEM0031

EKC(4,2)=2.*ESS

ELEM0032

EKC(3,3)=12.

ELEM0033

9

ELEM0034

EKC(4,3)=12.

ELEM0035

EKC(3,4)=-12.

ELEM0036

EKC(4,3)=-6.*ES ELEM0037
 EKC(4,4)=4.*ESS ELEM0038
 ETC(1,1)=1.2 ELEM0039
 ETC(2,1)=.1*ES ELEM0040
 ETC(3,1)=-1.2 ELEM0041
 ETC(4,1)=.1*ES ELEM0042
 ETC(2,2)=.13333333*ESS ELEM0043
 ETC(3,2)=-.1*ES ELEM0044
 ETC(4,2)=-.03333333*ESS ELEM0045
 ETC(3,3)=1.2 ELEM0046
 ETC(4,3)=-.1*ES ELEM0047
 ETC(4,4)=.13333333*ESS ELEM0048
 EMC(1,1)=156./420. ELEM0049
 EMC(2,1)=22./420.*ES ELEM0050
 EMC(3,1)=54./420. ELEM0051
 EMC(4,1)=-13./420.*ES ELEM0052
 EMC(2,2)=4./420.*ESS ELEM0053
 EMC(3,2)=-EMC(4,1) ELEM0054
 EMC(4,2)=-3./420.*ESS ELEM0055
 EMC(3,3)=EMC(1,1) ELEM0056
 EMC(4,3)=-EMC(2,1) ELEM0057
 EMC(4,4)=EMC(2,2) ELEM0058
 CC 10 I=1,4 ELEM0059
 CC 10 J=1,1 ELEM0060
 EMC(J,I)= EMC(I,J) ELEM0061
 EKC(J,I)= EKC(I,J) ELEM0062
 ESSS=ESS*ES ELEM0063
 SI=SIN(THETA) ELEM0064
 CC=COS(THETA) ELEM0065
 B=(EIB*CO*CO + EIC*SI*SI)/ESSS ELEM0066
 C=(ETC*CC*CO + EIB*SI*SI)/ESSS ELEM0067
 BC=(EIC-EIB)*SI*CO/ESSS ELEM0068
 TE=T/ES ELEM0069
 AM=OMEG*OMEG*AMAS*ES ELEM0070
 AMAE =AMAS*ES ELEM0071
 CC 5 I=1,4 ELEM0072

76
 11= (I*I-I)/2 ELEM0073
 14= (I+4)*(I+3)/2 ELEM0074
 DO 1 J=1,I ELEM0075
 EKT(I+J)= B*EKC(I,J)+TE*ETC(I,J) ELEM0076
 EMT(I+J)= AMAE*EMC(I,J) ELEM0077
 EKT(I4+J+4)= C*EKC(I,J) + TE*ETC(I,J) -AM*EMC(I,J) ELEM0078
 1 EMT(I4+J+4)= AMAE*EMC(I,J) ELEM0079
 DO 2 J=1,4 ELEM0080
 EMT(I4+J)=0. ELEM0081
 2 EKT(I4+J)=BC*EKC(I,J) ELEM0082
 IF (NDE .EQ. 8) GO TO 5 ELEM0083
 1E=(I+8)*(I+7)/2 ELEM0084
 DO 3 J=1,I ELEM0085
 EKT(I8+J+8)=GJE*ETC(I,J) ELEM0086
 3 EMT(I8+J+E)= PIE *EMC(I,J) ELEM0087
 DO 4 J=1,4 ELEM0088
 EKT(I8+J)=0. ELEM0089
 EKT(I8+J+4)=0. ELEM0090
 EMT(I8+J+4)=0. ELEM0091
 4 EMT(I8+J)=PI12E*EMC(I,J) ELEM0092
 5 CCNT1NU ELEM0093
 IF(NE.LT.NET) GO TO 100 ELEM0094
 EMT(6)= EMT(6)+AMN ELEM0095
 EMT(28) =EMT(28)+AMN ELEM0096
 IF(NDE.EQ.8) GO TO 100 ELEM0097
 EMT(10) =EMT(10)+ PIR ELEM0098
 EMT(36) =EMT(36)+ PIY ELEM0099
 EMT(66)= EMT(66)+PIP ELEM0100
 EMT(58)= EMT(58)+ PBW ELEM0101
 100 IF(NE.GT.1) GO TO 101 ELEM0102
 EKT(3)=EKT(3)+SPKB ELEM0103
 EKT(21)=EKT(21)+SPKC ELEM0104
 101 DO 102 I=1,36 ELEM0105
 102 EKT(I)=EKT(I)+EMT(I)*ALPHAH ELEM0106
 RETURN ELEM0107
 END ELEM0108

```

SUBROUTINE MESH(NDPE,NET,NDT,NCDT,MNC,MN,
  &NBU,      INDEX)          NUD,NNODE,ICOL,INUM,
                           NDPE(1)

      TO CALCULATE MESH INFORMATION OF THE FINITE ELEMENT

      DIMENSION      NUD(1),NNODE(1),ICOL(1),INUM(1),      NDPE(1)
      IF(NBU .GT. 0) GO TO 100
      DO 99 I=1,NDT
99  NUD(I)=1
      NCDT=NDT
      GO TO 98
100  DO 22 I=1,NBU
      IF (I .GE. NBU) GO TO 101
      II=I+1
      DO 21 J=II,NBU
      IF (INUM(I).NE.INUM(J)) GO TO 21
      IF (J.GE.NBU) GO TO 20
      J1=J+1
      DO 19 K=J1,NBU
      INUM(K-1)= INUM(K)
19  NBU=NBU-1
      J=J-1
21  CONTINUE
22  CONTINUE
101 DO 1 I=1,NDT
1  NUD(I)=1
      DO 2 I=1,NBU
      II=INUM(I)
2  NUD(II)=0
      DO 3 I=2,NDT
3  NUD(I)=NUD(I)+NUD(I-1)
      NCDT=NDT-NBU
      DO 4 I=1,NBU
      II=INUM(I)
4  NUD(II)=NCDT+I
98  CONTINUE

```

```

14=c
DO 5 I=1,NET
JJ=NDPE(I)
DO 54 J=1,JJ
54 ICOL(J)=NNODE(J+II)
DO 55 J=1,JJ
J1=ICOL(J)
55 NNODE(J+II)=NJC(J1)
5 II=II+JJ
DO 6 I=1,NCDT
6 ICOL(I)=I
II=0
DO 88 I=1,NET
JJ=NDPF(I)
ININ=NDT
DO 7 J=1,JJ
IN=NNODE(J+II)
7 IF(IN .LT. IMIN) IMIN=IN
DO 8 J=1,JJ
ID=NNODE(J+II)
8 IF(ICOL(ID) .GT. IMIN) ICOL(ID)=IMIN
38 II=II+JJ
INUM(1)=0
DO 9 I=2,NCDT
9 INUM(I)=INUM(I-1)+I-ICOL(I)
MN=INUM(NCDT)+NCDT
WRITE(6,10) MN,MNC
10 FORMAT(1/2X,*MAX. SIZE OF STF IS*,I6,5X,*SPECIFIED SIZE IS *,I6)
INDEX=1
IF(MNC .LT. MN) INDEX=2
RETURN
END

```

MESH0037
MESH0038
MESH0039
MESH0040
MESH0041
MESH0042
MESH0043
MESH0044
MESH0045
MESH0046
MESH0047
MESH0048
MESH0049
MESH0050
MESH0051
MESH0052
MESH0053
MESH0054
MESH0055
MESH0056
MESH0057
MESH0058
MESH0059
MESH0060
MESH0061
MESH0062
MESH0063
MESH0064
MESH0065
MESH0066
MESH0067
MESH0068

SUBROUTINE ASBV(STK,STM,IEQ,EK,EM, NDPE,NDT,NCDT,NNODE,MN,NET,IN
 NUM)
 C
 C TO ASSEMBLE AND CONSTRAIN BOUNDARY CONDITIONS
 C
 IMPLICIT REAL*8(A-H,O-Z)
 DIMENSION STK(1),STM(1),EK(1),EM(1), NDPE(1),NNODE(1),INUM(1)
 ID=NCDT+1
 DO 1 I=1,MN
 STK(I)=0.0
 1 STM(I)=0.0
 II=0
 DO 15 N=1,NET
 JJ=NDPE(N)
 IF(IEQ .EQ. 0) GO TO 3
 IF(N .GT. 1) GO TO 8
 3 CALL FLEMK(EK,EM,JJ,N)
 8 DO 14 I=1,JJ
 KI=(I*I-1)/2
 KNA=NNODE(II+I)
 IF(KNA .GE. ID) GO TO 14
 DO 13 J=1,I
 KNA=NNODE(II+J)
 IF(KNA .GE. ID) GO TO 13
 KA=INUM(KNA)+KNA
 IF(KNA .GT. KMA) KA=INUM(KNA)+KMA
 STK(KA)=STK(KA)+EK(KI+J)
 STM(KA)=STM(KA)+EM(KI+J)
 13 CONTINUE
 14 CONTINUE
 15 II=JJ+1
 RETURN
 END

ASBV001
 ASBV002
 ASBV003
 ASBV004
 ASBV005
 ASBV006
 ASBV007
 ASBV008
 ASBV009
 ASBV010
 ASBV011
 ASBV012
 ASBV013
 ASBV014
 ASBV015
 ASBV016
 ASBV017
 ASBV018
 ASBV019
 ASBV020
 ASBV021
 ASBV022
 ASBV023
 ASBV024
 ASBV025
 ASBV026
 ASBV027
 ASBV028
 ASBV029
 ASBV030
 ASBV031
 ASBV032
 ASBV033

```

C SUBROUTINE FAC(STF,NDT,NNDG,ICOL,INUM,U) FACT0001
C FACTORING A SYMMETRIC MATRIX INTO LDL* FACT0002
C
C IMPLICIT REAL*8(A-F,D-Z) FACT0003
C DIMENSION STF(1),ICOL(1),INUM(1),U(1) FACT0004
C NNDG=0 FACT0005
C IF(STF(1).LT.0) 2,1,3 FACT0006
C
1 IZR=1 FACT0007
99 WRITE(6,100) IZR FACT0008
100 FORMAT(1ZX,'THE',14,'TH DIAG. AFTER FACT.=0.0,INCOMPLETE FACT.') FACT0009
NNDG=-1 FACT0010
RETURN FACT0011
2 NNDG=1 FACT0012
3 IF(NDT.LT.2) GO TO 11 FACT0013
DO 10 IR=2,NDT FACT0014
II=ICOL(IR)
IF(II.EQ. IR) GO TO 10 FACT0015
JR=INUM(IR)
IE=IR-1
DO 5 IC=II,IE FACT0016
IMAX=II
IF(II.LT. ICOL(IC)) IMAX=ICOL(IC) FACT0017
JE=IC-1
SUM=STF(JR+IC)
IF(JE.LT. IMAX) GO TO 55 FACT0018
JC=INUM(IC)
DO 4 J=IMAX,JE FACT0019
4 SUM=SUM-L(J)*STF(JC+J) FACT0020
55 U(IC)=SUM FACT0021
5 STF(JR+IC)=SUM/STF(INUM(IC)+IC) FACT0022
JJ=JR+IR
DO 6 J=II,IE FACT0023
6 STF(JJ)=STF(JJ)-L(J)*STF(JR+J) FACT0024
IF(STF(JJ)).LT.0.0001 GO TO 10 FACT0025
7 IZR=IR FACT0026

```

```
GO TO 99  
8 NNDG=NNDG+1  
10 CONTINUE  
11 WRITE(6,101) NNDG  
101 FORMAT(12X,'NO. OF NEGATIVE DIAGS.=',I4,5X,'FACT. COMPLETED')  
      RETURN  
      END
```

```
FACT0037  
FACT0038  
FACT0039  
FACT0040  
FACT0041  
FACT0042  
FACT0043
```

```

SUBROUTINE MTRTR(M,N,RM,XLR,K,IST)
      MATRIX MULTIPLICATION

      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION RM(1),XLR(1),X(1)
      DO 2 I=IST,M
      II=(I-1)*N
      IJ=(I-1)*M
      DO 2 J=1,I
      JJ=(J-1)*N
      RM(IJ+J)=C.0
      DO 2 K=1,N
2     RM(IJ+J)=RM(IJ+J)+XLR(II+K)*X(JJ+K)
      DO 3 I=IST,M
      JJ=(I-1)*M
      DO 3 J=1,I
3     RM((J-1)*M+I)=RM(JJ+J)
      RETURN
      END

```

MTRT0001
MTRT0002
MTRT0003
MTRT0004
MTRT0005
MTRT0006
MTRT0007
MTRT0008
MTRT0009
MTRT0010
MTRT0011
MTRT0012
MTRT0013
MTRT0014
MTRT0015
MTRT0016
MTRT0017
MTRT0018
MTRT0019
MTRT0020

SUBROUTINE MULTZ(STF,X,Y,NDT,M,ICOL,INUM,MM)

MULT0001

C MATRIX MULTIPLICATION

MULT0002

C

```
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION STF(1),X(1),Y(1),ICOL(1),INUM(1)
DO 1 I=1,NDT
1 Y(I)=0.0
MMM=M+MM-1
DO 4 I=MM,MMM
II=(I-1)*NDT
DO 3 IR=1,NDT
IS=INUM(IR)
IC=ICOL(IR)
IF=IR-1
IF(IC .GT. IF) GO TO 3
DO 2 J=IC,IF
S=STF(IS+J)
Y(IR)=Y(IR)+S*X(II+J)
2 Y(J)=Y(J)+S*X(II+IR)
3 Y(IP)=Y(IR)+STF(IS+IP)*X(II+IR)
DO 4 J=1,NDT
X(II+J)=Y(J)
4 Y(J)=0.0
RETURN
END
```

MULT0003

MULT0004

MULT0005

MULT0006

MULT0007

MULT0008

MULT0009

MULT0010

MULT0011

MULT0012

MULT0013

MULT0014

MULT0015

MULT0016

MULT0017

MULT0018

MULT0019

MULT0020

MULT0021

MULT0022

MULT0023

MULT0024

MULT0025

MULT0026

```

SUBROUTINE SOLZ(STF,U,NDT,M,ICOL,INUM,MM) SOLZ0001
C SOLZ0002
C SOLZ0003
C SOLZ0004
C SOLZ0005
C SOLZ0006
C SOLZ0007
C SOLZ0008
C IMPLICIT REAL*8(A-F,O-Z) SOLZ0009
C DIMENSION STF(1),U(1),ICOL(1),INUM(1) SOLZ0010
C MMM=M+MM-1 SOLZ0011
C IF(NDT .LT. 2) GO TO 3 SOLZ0012
C DO 2 IR=2,NDT SOLZ0013
C JI=ICOL(IR) SOLZ0014
C JE=IR-1 SOLZ0015
C IF(JI .GT. JE) GO TO 2 SOLZ0016
C DO 1 I=MM,MMM SOLZ0017
C II=(I-1)*NDT SOLZ0018
C IS=II+IR SOLZ0019
C DO 1 J=JI,JE SOLZ0020
C 1 U(IS)=U(IS)-STF(INUM(IR)+J)*U(II+J) SOLZ0021
C 2 CONTINUE SOLZ0022
C 3 DO 4 I=MM,MMM SOLZ0023
C 4 II=(I-1)*NDT SOLZ0024
C 4 DO 4 IR=1,NDT SOLZ0025
C 4 U(II+IR)=U(II+IR)/STF(INUM(IR)+IR) SOLZ0026
C 4 IF(NDT .LT. 2) GO TO 7 SOLZ0027
C 4 DO 6 IK=2,NDT SOLZ0028
C 4 IR=NDT-IK+2 SOLZ0029
C 4 JI=ICOL(IR) SOLZ0030
C 4 JE=IR-1 SOLZ0031
C 4 IF(JI .GT. JE) GO TO 6 SOLZ0032
C 4 DO 5 I=MM,MMM SOLZ0033
C 5 II=(I-1)*NDT SOLZ0034
C 5 IS=II+IR SOLZ0035
C 5 DO 5 J=JI,JE SOLZ0036
C 5 U(II+J)=U(II+J)-STF(INUM(IR)+J)*U(IS)
C 6 CONTINUE
C 7 RETURN
C END

```

```

C SUBROUTINE DNRC01(M,A,N,XL,X)
C
C EIGENVALUE ANALYSIS ROUTINE
C
C DIMENSION A(1),B(1),XL(1),X(1)
C DOUBLE PRECISION A,B,XL,X,SUMV
C K=1
C DO 100 J=2,M
C L=M*(J-1)
C DO 100 I=1,J
C L=L+1
C K=K+1
100 B(K)=B(L)
C MV=0
C CALL EIGEN (B,X,M,MV)
C L=0
C DO 110 J=1,M
C L=L+J
C 110 XL(J)=1.0/DSQRT(CABS(B(L)))
C K=J
C DO 115 J=1,M
C DO 115 I=1,M
C K=K+1
C 115 B(K)=X(K)*XL(J)
C DO 120 I=1,M
C N2=0
C DO 120 J=1,M
C NL=M*(I-1)
C L=M*(J-1)+I
C X(L)=0.0
C DO 120 K=1,M
C N1=N1+1
C N2=N2+1
C 120 X(L)=X(L)+B(N1)*A(N2)
C L=0
C DO 130 J=1,M

```

DNR00001
 DNR00002
 DNR00003
 DNR00004
 DNR00005
 DNR00006
 DNR00007
 DNR00008
 DNR00009
 DNR00010
 DNR00011
 DNR00012
 DNR00013
 DNR00014
 DNR00015
 DNR00016
 DNR00017
 DNR00018
 DNR00019
 DNR00020
 DNR00021
 DNR00022
 DNR00023
 DNR00024
 DNR00025
 DNR00026
 DNR00027
 DNR00028
 DNR00029
 DNR00030
 DNR00031
 DNR00032
 DNR00033
 DNR00034
 DNR00035
 DNR00036

```

DO 130 I=1,J
N1=I-M
N2=M*(J-1)
L=L+1
A(L)=0.0
DO 130 K=1,M
N1=N1+M
N2=N2+1
130 A(L)=A(L)+X(N1)*B(N2)
CALL EIGEN (A,X,M,MV)
L=I
DO 140 I=1,M
L=L+1
140 XL(I)=A(L)
DO 150 I=1,M
N2=0
DO 150 J=1,M
N1=I-M
N2=N2+1
N1=M*(J-1)+I
A(L)=0.0
DO 150 K=1,M
N1=N1+M
N2=N2+1
150 A(L)=A(L)+B(N1)*X(N2)
L=0
K=0
DO 180 J=1,M
SUMV=0.0
DO 170 I=1,M
L=L+1
170 SUMV=SUMV+A(L)*A(L)
175 SUMV=DSQRT(SUMV)
DO 180 I=1,M
K=K+1
180 X(K)=A(K)/SUMV
RETURN
END

```

DNR00037
 DNR00038
 DNR00039
 DNR00040
 DNR00041
 DNR00042
 DNR00043
 DNR00044
 DNR00045
 DNR00046
 DNR00047
 DNR00048
 DNR00049
 DNR00050
 DNR00051
 DNR00052
 DNR00053
 DNR00054
 DNR00055
 DNR00056
 DNR00057
 DNR00058
 DNR00059
 DNR00060
 DNR00061
 DNR00062
 DNR00063
 DNR00064
 DNR00065
 DNR00066
 DNR00067
 DNR00068
 DNR00069
 DNR00070
 DNR00071
 DNR00072
 DNR00073

SUBROUTINE EIGEN(A,R,N,MV)

EIGE0001

C
C EIGENVALUE ANALYSIS ROUTINE NEEDED IN DNROOT
C
DIMENSION A(1),R(1)
DOUBLE PRECISION A,R,ANORM,ANRMX,THR,X,Y,SINX,SINX2,COSX,
1 COSX2,SINC,S, RANGE
2 RANGE=1.0E-12
3 IF(MV-1) 10,25,10
10 IQ=-N
DO 20 J=1,N
10=IQ+N
DO 20 I=1,N
IJ=IQ+I
R(IJ)=0.0
IF(I-J) 20,15,20
15 R(IJ)=1.0
20 CONTINUE
25 ANORM=0.0
DO 35 I=1,N
DO 35 J=1,N
IF(I-J) 30,35,30
30 IA=I+(J-I)/2
ANORM=ANORM+A(IA)*A(IA)
35 CONTINUE
IF(ANORM) 165,165,4L
40 ANCRM=1.414*DSCRT(ANORM)
ANRMX=ANCRM*RANGE/FLCAT(N)
IND=0
THR=ANORM
45 THR=THR/FLOAT(N)
50 L=1
55 M=L+1
60 MO=(M+M-M)/2
LQ=(L+L-L)/2
LM=L+MO

EIGE0002

EIGE0003

EIGE0004

EIGE0005

EIGE0006

EIGE0007

EIGE0008

EIGE0009

EIGE0010

EIGE0011

EIGE0012

EIGE0013

EIGE0014

EIGE0015

EIGE0016

EIGE0017

EIGE0018

EIGE0019

EIGE0020

EIGE0021

EIGE0022

EIGE0023

EIGE0024

EIGE0025

EIGE0026

EIGE0027

EIGE0028

EIGE0029

EIGE0030

EIGE0031

EIGE0032

EIGE0033

EIGE0034

EIGE0035

EIGE0036

```

52 IF(DARS(A(LM))-THR) 130,65,65 EIGE0037
65 IND=1 EIGE0038
    LL=L+LQ EIGE0039
    MM=M+NQ EIGE0040
    X=0.5*(A(LL)-A(MM)) EIGE0041
63 Y=-A(LM)/DSQRT(A(LM)*A(LM)+X*X) EIGE0042
    IF(X) 70,75,75 EIGE0043
70 Y=-Y EIGE0044
75 SINX=Y/DSQRT(2.0*(1.0+(DSQRT(1.0-Y*Y)))) EIGE0045
    SINX2=SINX*SINX EIGE0046
78 COSX=DSQRT(1.0-SINX2) EIGE0047
    COSX2=COSX*COSX EIGE0048
    SINCS =SINX*COSX EIGE0049
    ILQ=N*(L-1) EIGE0050
    IMQ=N*(M-1) EIGE0051
    DC 125 I=1,N EIGE0052
    IO=(I+I-1)/2 EIGE0053
    IF(I-L) 80,115,80 EIGE0054
80 80 IF(I-M) 85,115,90 EIGE0055
85 IM=I+MQ EIGE0056
    GO TO 95 EIGE0057
90 IM=M+IO EIGE0058
95 IF(I-L) 100,105,105 EIGE0059
100 IL=I+LQ EIGE0060
    GO TO 110 EIGE0061
105 IL=L+IO EIGE0062
110 X=A(IL)*COSX-A(IM)*SINX EIGE0063
    A(IM)=A(IL)*SINX+A(IM)*COSX EIGE0064
    A(IL)=X EIGE0065
115 IF(MV-1) 120,125,120 EIGE0066
120 ILR=ILQ+I EIGE0067
    IMR=IMQ+I EIGE0068
    X=R(ILR)*COSX-R(IMR)*SINX EIGE0069
    R(IMR)=R(ILR)*SINX+R(IMR)*COSX EIGE0070
    R(ILR)=X EIGE0071
125 CONTNUF EIGE0072

```

```

X=2.0*A(LM)*SINCS          EIGE0073
Y=A(LL)*COSX2+A(MM)*SINX2-X EIGE0074
X=A(LL)*SINX2+A(MM)*CCSX2+X EIGE0075
A(LM)=(A(LL)-A(MM))*SINCS+A(LM)*(COSX2-SINX2) EIGE0076
A(LL)=Y                      EIGE0077
A(MM)=X                      EIGE0078
130 IF(M=N) 135,140,135      EIGE0079
135 M=M+1
    GO TO 60
140 IF(L-(N-1)) 145,150,145 EIGE0082
145 L=L+1
    GO TO 45
150 IF(TND=1) 160,155,160  EIGE0085
155 TND=0
    GO TO 50
160 IF(THR=ANRMX) 165,165,45 EIGE0088
165 IQ=-N
    DO 185 I=1,N
    IQ=IQ+N
    LL=I+(I-I)/2
    JG=N*(I-2)
    DO 185 I=1,N
    JQ=JQ+N
    JM=J+(J-J)/2
    IF(A(LL)-A(MM)) 170,185,185 EIGE0097
170 X=A(LL)
    A(LL)=A(MM)
    A(MM)=X
    IF(MV=1) 175,185,175  EIGE0101
175 DO 180 K=1,N
    ILR=IQ+K
    IMR=JQ+K
    X=R(ILR)
    R(ILR)=R(IMR)          EIGE0106
180 R(IMR)=X                EIGE0107
185 CONTINUE
    RETURN
    END

```

```

C SUBROUTINE OUTPUT(KKK,M,NCDT,NOT,NOD,NNODE,EPR,XLR,U,SRM,SRK) OUTP0001
C
C          OUTPUT ROUTINE
C
COMMON /PUNCH/    IPUNCH
COMMON /BW/         ICASE      ,  IGUEST
DOUBLE PRECISION XLR,SRM,SRK ,U      ,ERR
DIMENSION XLR(1),U(1),           SRM(1), SRK(1)
DIMENSION NOD(1),NNODE(1)
DIMENSION XXLF(15,120)
IDERUG=0
WRITE(6,24) KKK,ERR
24 FORMAT(1/2X,'NO. OF ITERATION=',I4,2X,'CONVERGED WITHIN',D13.5)
IF(IDERUG.EQ.0) GO TO 15
WRITE(6,12)
12 FORMAT(1/2X,'EIGENVECTORS=',/)
DO 14 I=1,M
II=(I-1)*NCDT
14 WRITE(6,13) (XLR(II+J),J=1,NCDT)
13 FORMAT(1/(2X,10D13.5))
15  CONTINUE
WRITE(6,20)
DO 18 I=1,M
KK=I*M-M
18  WRITE (6,16) (SRM(J+KK) , J=1,I)
WRITE(6,21)
DO 19 I=1,M
KK=I*M-M
19  WRITE (6,16) (SRK(J+KK) , J=1,I)
16  FORMAT      (2X,10D13.5)
20  FORMAT (1/ 23H  REDUCED MASS MATRIX    /)
21  FORMAT (1/ 23H  REDUCED STIF MATRIX    /)
NBU=NCDT-NCCT
GO TO (101,101,101,102,101),ICASE
101 DO 106 I=1,M
DO 201 J=1,NBU

```

^
/
P

201	XXLR(I,J)=0.0	OUTP0037
	CONTINUE	OUTP0038
	DO 202 J=1,NCDT	OUTP0039
202	XXLR(I,NBU+J)=XLR((I-1)*NCDT+J)	OUTP0040
100	CONTINUE	OUTP0041
	GO TO 205	OUTP0042
102	DO 203 I=1,M	OUTP0043
	DO 206 J=1,NBU	OUTP0044
206	XXLR(I,J)=0.0	OUTP0045
	XXLR(I,3)=XLR((I-1)*NCDT+1)	OUTP0046
	DO204 J=2,NCDT	OUTP0047
204	XXLR(I,J+NBU)=XLR((I-1)*NCDT+J)	OUTP0048
203	CONTINUE	OUTP0049
205	CONTINUE	OUTP0050
	IF(ICASE.EQ.1) GO TO 333	OUTP0051
	NOM=4	OUTP0052
	NODE=NDT/NOM	OUTP0053
	WRITE(6,350)	OUTP0054
T6	350 FORMAT(//1X,'**** BLADE MODE SHAPES ****')	OUTP0055
	DO 351 I=1,M	OUTP0056
	WRITE(6,450C)I	OUTP0057
4500	FORMAT(//1X,'I=',I2//)	OUTP0058
	WRITE(6,490C)	OUTP0059
4900	FORMAT(T5,'K',T12,'W(I,J)',T33,'V(I,J)', T53,'DW(I,J)', T73,	OUTP0060
&	'DV(I,J)')	OUTP0061
	DO351 K=1,NODE	OUTP0062
	WRITE(6,352) K,(XXLR(I,NOM*(K-1)+J),J=1,NOM)	OUTP0063
352	FORMAT(1X,I4,E15.7))	OUTP0064
351	CONTINUE	OUTP0065
	GO TO 360	OUTP0066
333	CONTINUE	OUTP0067
	NOM=6	OUTP0068
	NODE=NDT/NOM	OUTP0069
	WRITE(6,353)	OUTP0070
353	FORMAT(//1X,'**** WING MODE SHAPES ****')	OUTP0071
	DO 354 I=1,M	OUTP0072

4901	WRITE(6,45(0))	CUTP0073
	WRITE(6,4901)	CUTP0074
	FORMAT(T5,'K',T13,'W(I,J)',T33,'V(I,J)',T53,'DW(I,J)',T73,	CUTP0075
	& 'DV(I,J)',T93,'PHI(I,J)',T113,'DPHI(I,J)')	CUTP0076
	DO 355 K=1,NODE	CUTP0077
355	WRITE(6,352) K,(XXLR(I,NOM*(K-1)+J),J=1,NOM)	CUTP0078
354	CONTINUE	CUTP0079
360	CONTINUE	CUTP0080
	CONTINUE	CUTP0081
	IF(IFUNCH.EQ.0) GO TO 370	CUTP0082
	DO 359 I=1,M	CUTP0083
	DO 358 K=1,NOM	CUTP0084
	WRITE(7,357)(XXLR(I,NOM*(J-1)+K),I=1,NODE)	CUTP0085
357	FORMAT(6E13.5)	CUTP0086
358	CONTINUE	CUTP0087
359	CONTINUE	CUTP0088
370	CONTINUE	CUTP0089
	WRITE(6,371)	CUTP0090
371	FORMAT(1H1)	CUTP0091
	RETURN	CUTP0092
	END	CUTP0093

A.2 The TILDYN Program Listing

C PROGRAM RUTOR
C PART 2 : PROGRAM TILEDYN
C *****
C PURPOSE
C TO ANALYZE THE TILT-ROTOR DYNAMIC SYSTEM BY MEANS
C OF FREQUENCY RESPONSE AND EIGENVALUES IN POWERED
C AND AUTOROTATION FLIGHT
C
C DEVELOPED BY MASAHIRO YASUE
C OF AERODYNAMIC AND STRUCTURES RESEARCH LABORATORY
C AUGUST 1974
C ADDRESS : BLG 41-211
C MASSACHUSETTS INSTITUTE OF TECHNOLOGY
C CAMBRIDGE, MASS. 02139
C
C *****
C
C MAIN PROGRAM
C
C TO DEFINE THE SEQUENCE OF THE PROGRAM
C
C
C COMMON/DDF18/AAY(19,19),BRY(19,19),CCY(19,19),CDY(19,6)
C DIMENSION CGUST(6) ,DCZ(19)
C COMMON /PARMT/ ITYPE ,IFLT
1 CONTINUE
5001 FORMAT(1F11)
CALL INITL
CALL CUEFF
CALL INPUT(CGUST,DDDF,IRES,IEIGEN)
CALL INTPL
WRITE(6,S001)
C MAIN001
C MAIN002
C MAIN003
C MAIN004
C MAIN005
C MAIN006
C MAIN007
C MAIN008
C MAIN009
C MAIN010
C MAIN011
C MAIN012
C MAIN013
C MAIN014
C MAIN015
C MAIN016
C MAIN017
C MAIN018
C MAIN019
C MAIN020
C MAIN021
C MAIN022
C MAIN023
C MAIN024
C MAIN025
C MAIN026
C MAIN027
C MAIN028
C MAIN029
C MAIN030
C MAIN031
C MAIN032
C MAIN033
C MAIN034
C MAIN035
C MAIN036

CALL AERO01
CALL ORDINT
WRITE(6,5001)
CALL AINER
CALL AEROMT
CALL EQMTX(IDOF)
IF (IFLT.EQ.0) GO TO 400
CALL AUTO(IDOF)
400 CONTINUE
IDIM=IDOF+IFLT
IF (IRES.EQ.0) GO TO 200
WRITE(6,5001)
CALL GUST01(GUST,DDY,IDIM,DDZ)
CALL FRQRFS(IDIM,AAY,BBY,CCY,DDZ,IFLT,DOF)
200 CONTINUE
IF (IEIGEN.EQ.0) GO TO 1000
WRITE(6,5001)
CALL EIGEN(IDIM,AAY,BBY,CCY,DDY,DOF)
1000 CONTINUE
WRITE(6,5001)
GO TO 1
END

MAIN0037
MAIN0038
MAIN0039
MAIN0040
MAIN0041
MAIN0042
MAIN0043
MAIN0044
MAIN0045
MAIN0046
MAIN0047
MAIN0048
MAIN0049
MAIN0050
MAIN0051
MAIN0052
MAIN0053
MAIN0054
MAIN0055
MAIN0056
MAIN0057
MAIN0058

BLOCK DATA

BLOC0001

BLOC0002

BLOC0003

BLOC0004

TO INITIALIZE THE COEFFICIENTS OF GAUSSIAN QUADRATURE

BLOC0005

COMMON /AREA2/NPT,XXX(20),A(20)

BLOC0006

DATA NPT/11/

BLOC0007

DATA A(1),A(2),A(3),A(4),A(5),A(6)/0.055668,

0.125580 ,0.186290, 0.233193 ,0.262804 , 0.272925 /

END

BLOC0008

BLOC0009

SUBROUTINE INITIE	INIT0001
C	INIT0002
C	INIT0003
C	INIT0004
COMMON/DOF13/AAY(19,19),BBY(19,19),CCY(19,19),DDY(19,6)	INIT0005
COMMON/INERTI/TTMT(4,6,3),TTCTJ(4,6,3),AMJT(4,3,6),CJT(4,3,6)	INIT0006
COMMON /ARR/WGUST(4,6),DAMX(6,6),AMX(6,6),DQ(4,6,3),Q(4,6,3)	INIT0007
a ,DHMAX(4,3,6),HMAX(4,3,6)	INIT0008
COMMON/WINGAR/TSOS(20,6,6),TSAS(20,6,6),TSAG(20,6,3)	INIT0009
DO 10 I=1,4	INIT0010
DO 10 J=1,6	INIT0011
DO 10 K=1,3	INIT0012
TTMT(I,J,K)=0.0	INIT0013
TTCTJ(I,J,K)=0.0	INIT0014
AMJT(I,K,J)=0.0	INIT0015
CJT(I,K,J)=0.0	INIT0016
DQ(I,J,K)=0.0	INIT0017
Q(I,J,K)=0.0	INIT0018
DHMAX(I,K,J)=0.0	INIT0019
HMAX(I,K,J)=0.0	INIT0020
1. CONTINUE	INIT0021
DO 11 I=1,6	INIT0022
DO 11 J=1,6	INIT0023
wGUST(I,J)=0.0	INIT0024
DAMX(I,J)=0.0	INIT0025
AMX(I,J)=0.0	INIT0026
DO 11 K=1,20	INIT0027
TSOS(K,I,J)=0.0	INIT0028
TSAS(K,I,J)=0.0	INIT0029
11 CONTINUE	INIT0030
DO 12 I=1,20	INIT0031
DO 12 J=1,6	INIT0032
DO 12 K=1,3	INIT0033
TSAG(I,J,K)=0.0	INIT0034
12 CONTINUE	INIT0035
DO 13 I=1,19	INIT0036

```
DO 14 J=1,19
AAV(I,J)=0.0
RBV(I,J)=0.0
CCV(I,J)=0.0
14  CONTINUE
DO 15 K=1,6
DDV(I,K)=0.0
15  CONTINUE
13  CONTINUE
      RETURN
      END
```

```
INIT0037
INIT0038
INIT0039
INIT0040
INIT0041
INIT0042
INIT0043
INIT0044
INIT0045
INIT0046
INIT0047
```

SUBROUTINE COEFF

COEF0001
COEF0002
COEF0003
COEF0004
COEF0005
COEF0006
COEF0007
COEF0008
COEF0009
COEF0010
COEF0011
COEF0012
COEF0013
COEF0014
COEF0015
COEF0016
COEF0017
COEF0018
COEF0019
COEF0020
COFF0021
COEF0022
COEF0023
COEF0024
COEF0025
COEF0026
COEF0027
COEF0028
COEF0029
COEF0030
COEF0031
COEF0032
COEF0033

C
C TO DEFINE THE POINTS AND COEFFICIENTS OF GAUSSIAN QUADRATURE
C
DIMENSION Y(20),YY(20)
COMMON /AREA2/NPT,XXX(20),A(20)
NPTH=NPT/2
IF((FLOAT(NPTH)-NPT/2.0).NE.0.0)GO TO 100
READ(5,5000)(Y(I),I=1,NPTH),(A(J),J=1,NPTH)
5000 FORMAT(8F10.5)
DO 10 II=1,NPTH
Y(NPTH+II)=-Y(NPTH-II+1)
A(NPTH+II)=A(NPTH-II+1)
10 CONTINUE
GO TO 200
100 NPTH1=NPTH+1
DATA Y(1),Y(2),Y(3),Y(4),Y(5),Y(6)/0.978228,
* 0.897002 , 0.730152 , 0.519096 , 0.269543 , 0.0 /
DO 20 MM=1,NPTH
A(NPTH+MM+1)=A(NPTH-MM+1)
Y(NPTH+MM+1)=-Y(NPTH-MM+1)
20 CONTINUE
200 DO 50 KK=1,NPT
YY(KK)=Y(KK)
50 CONTINUE
DO 60 IN=1,NPT
Y(IN)=YY(NPT-IN+1)
60 CONTINUE
DO 30 JJJ=1,NPT
XXX(JJJ)=(Y(JJJ)+1.0)/2.0
30 CONTINUE
RETURN
END

SUBROUTINE INPUT(CGUST, IDOF, TRES, IEIGEN)

TO SUPPLY INPUT INFORMATION

DES = IDENTIFYING INFORMATION

ITYPE=0: HINGELESS ROTOR IN POWERED FLIGHT

ITYPF=1: HINGELESS ROTOR IN AUTOROTATIONAL FLIGHT

GYMBALLED ROTOR IN BOTH FLIGHTS

IFLT =0 : POWERED FLIGHT IFLT=1 : AUTOROTATION FLIGHT

IDOF =9 : BASIC DEGREES OF FREEDOM IS 9 IDOF=18 : DOF IS 18

IRFS =0 : FREQUENCY RESPONSE OFF IRFS=1 : RESPONSE ON

IFRMAG=0 : MODE NORMALIZED ROTOR RADIUS AND WING SEMISPAN

IFPMAG=1 : NORMAL MODES

IEIGEN=0 : EIGENANALYSIS OFF IEIGEN=1 : EIGENANALYSIS ON

NBLD= NUMBER OF BLADES

POH= AIR DENSITY

OMEGA= ROTATIONAL SPEED (RAD/SEC)

RAMDA= INFLOW RATIO

VEI= CRUISING FLIGHT SPEED

R= ROTOR RADIUS

AIB= BLADE FLAPPING MOMENT OF INERTIA

CHOD= BLADE CHORD

CL= BLADE LIFT CURVE SLOPE

CD= BLADE DRAG COEFFICIENT

HMAST= MAST HEIGHT

DFL3= PITCH-FLAP COUPLING COEFFICIENT (RADIAN)

WL= WING SEMISPAN

WCOD= WING CHORD

WCL= WING LIFT CURVE SLOPE

WCD= WING DRAG COEFFICIENT

WCMD= WING PITCHING MOMENT COEFFICIENT

WCMA= WING PITCHING MOMENT CURVE SLOPE

EDIS=DISTANCE BETWEEN AERODYNAMIC CENTER AND ELASTIC AXIS

INPU0001

INPU0002

INPU0003

INPU0004

INPU0005

INPU0006

INPU0007

INPU0008

INPU0009

INPU0010

INPU0011

INPU0012

INPU0013

INPU0014

INPU0015

INPU0016

INPU0017

INPU0018

INPU0019

INPU0020

INPU0021

INPU0022

INPU0023

INPU0024

INPU0025

INPU0026

INPU0027

INPU0028

INPU0029

INPU0030

INPU0031

INPU0032

INPU0033

INPU0034

INPU0035

INPU0036

TOT

C (NONDIMENSIONALIZED BY WING CHORD, POSITIVE AERODYNAMIC
C CENTER AHEAD) INPU0037
C
C WTHET= WING TRIM ANGLE OF ATTACK (RADIAN) INPU0038
C
C CGUST= EXCITING FORCE COMPONENTS INPU0039
C
C BRAM= (BLADE NATURAL FREQUENCY)**2 (RADIAN/SEC)**2 INPU0040
C WRAM= (WING NATURAL FREQUENCY)**2 (RADIAN/SEC)**2 INPU0041
C
C NWE= WING ELEMENT NUMBER INPU0042
C EMSW= WING ELEMENT SIZE NORMALIZED BY THE SEMISPAN INPU0043
C G= VERTICAL BENDING MODE COMPONENT AT THE NODE OF THE WING INPU0044
C Z= CHORDWISE BENDING MODE COMPONENT AT THE NODE OF THE WING INPU0045
C DG= VERTICAL BENDING MODE SLOPE AT THE NODE OF THE WING INPU0046
C DZ= CHORDWISE BENDING MODE SLOPE AT THE NODE OF THE WING INPU0047
C WPHI= TORSION MODE COMPONENT AT THE NODE OF THE WING INPU0048
C DWPHI= TORSION MODE SLOPE AT THE NODE OF THE WING INPU0049
C
C N= BLADE ELEMENT NUMBER INPU0050
C EMS=BLADE ELEMENT SIZE NORMALIZED BY THE ROTOR RADIUS INPU0051
C AMASS= MASS DISTRIBUTION AT THE NODE OF THE BLADE INPU0052
C THETN= ANGLE OF TWIST AT THE NODE OF THE BLADE INPU0053
C COL= COLLECTIVE PITCH ANGLE DETERMINED BY THE PERFORMANCE (RADIAN) INPU0054
C W=OUT-OF-PLANE MODE COMPONENT AT THE NODE OF THE WING INPU0055
C V= INPLANE MODE COMPONENT AT THE NODE OF THE BLADE INPU0056
C DW= OUT-OF- PLANE MODE SLOPE COMPONENT AT THE NODE OF THE BLADE INPU0057
C DV= INPLANE MODE SLOPE COMPONENT AT THE NODE OF THE BLADE INPU0058
C
C PRAMO= (COLLECTIVE MODE NATURAL FREQUENCY OF THE BLADE)**2 INPU0059
C (RADIAN/SEC)**2 INPU0060
C WCOL= OUT-OF-PLANE COMPONENT OF THE BLADE COLLECTIVE MODE AT THE NODE INPU0061
C VCOL= INPLANE COMPONENT OF THE BLADE COLLECTIVE MODE AT THE NODE INPU0062
C DWCOL= OUT-OF-PLANE SLOPE COMPONENT OF THE BLADE COLLECTIVE MODE INPU0063
C AT THE NODE INPU0064
C DVCOL=INPLANE SLOPE COMPONENT OF THE BLADE COLLECTIVE MODE AT THE NODE INPU0065
C INPU0066
C INPU0067
C INPU0068
C INPU0069
C INPU0070
C INPU0071
C INPU0072

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C
DIMENSTON RMAX(4),BMAX(4),WMAX(6),RIG(6)          INPU0073
DIMENSTON CGUST(6) ,SRM0(4),SBM(4),SWG(6),DES(80) INPU0074
COMMON /PARMT/ ITYPE ,IFLT                      INPU0075
COMMON /AMATIC/ TT(6,5),C(6,6) ,T(5,6)          INPU0076
COMMON /AREA1/OMEGA,R,VFL,CL,CD,PARMA,SNOMEG    INPU0077
COMMON /AREA6/NORLD,ROH,CHOD,ATB,CK,HMAST ,ALOCK ,AND,HR INPU0078
COMMON /ARFAB/BLAM(4),WLAM(6),BRAM(4),WRAM(6),BLAM0(4),BRAM0(4) INPU0079
COMMON /GIN/   V(4,21),W(4,21),DV(4,21),DW(4,21),THETA(21), INPU0080
%EMS(20),AMASS (20),N,NDP                         INPU0081
COMMON /GINO/   VCOL(4,21),WCOL(4,21),WCOL(4,21),WCOL(4,21) INPU0082
COMMON /WING/ NW,NDPW,FMSW(20),G(6,21),DG(6,21),Z(6,21),DZ(6,21), INPU0083
*WPHI(6,21),DWPHI(6,21)                         INPU0084
COMMON /WICH/WL,WCD,WCL,WCD,WCMO,WCM,EDIS,WTHET,VV INPU0085
COMMON /COMPL/ AKPC(4),AKPD(4)                   INPU0086
COMMON /FRMAG/   FRB(4),FRBD(4),FRW(6) ,IFRMAG    INPU0087
COMMON /THF/THETN(21) ,MR,MW                     INPU0088
IFRHG=0                                            INPU0089
MR=2                                              INPU0090
MW=3                                              INPU0091
READ(5,5003)(DES(I),I=1,80)                      INPU0092
READ(5,5001) ITYPE                               INPU0093
READ(5,5001) IFLT                               INPU0094
READ(5,2034) IDOF                               INPU0095
IE(IDOF.EQ.9) GO TO 62                          INPU0096
MP=4                                              INPU0097
MW=6                                              INPU0098
CONTINUE                                         INPU0099
READ(5,5001) IRES                               INPU0100
READ(5,5001) IFRMAG                            INPU0101
READ(5,5001) IEIGEN                            INPU0102
READ(5,5001) NORLD                            INPU0103
READ(5,5000) ROH,OMEGA,PARMA,VEL               INPU0104
READ(5,5000) R,ATB,CHOD,CL,CD,HMAST,DEL3     INPU0105
READ(5,5000) WL,WCD,WCL,WCD,WCMO,WCM,EDIS,WTHET INPU0106
READ(5,5000) CGUST                            INPU0107

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INPU0108
INPU0073
INPU0074
INPU0075
INPU0076
INPU0077
INPU0078
INPU0079
INPU0080
INPU0081
INPU0082
INPU0083
INPU0084
INPU0085
INPU0086
INPU0087
INPU0088
INPU0089
INPU0090
INPU0091
INPU0092
INPU0093
INPU0094
INPU0095
INPU0096
INPU0097
INPU0098
INPU0099
INPU0100
INPU0101
INPU0102
INPU0103
INPU0104
INPU0105
INPU0106
INPU0107
INPU0108

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READ(5,5000)BRAM           INPU0109
READ(5,5000)WRAM           INPU0110
READ(5,2034)NW              INPU0111
NDPW=NW+1                   INPU0112
READ(5,5000)(EMSW(K),K=1,NW) INPU0113
DO 60 I=1,MW
  READ(5,1001)(   G(I,J),J=1,NDPW) INPU0114
  READ(5,1001)(   Z(I,J),J=1,NDPW) INPU0115
  READ(5,1001)(   DG(I,J),J=1,NDPW) INPU0116
  READ(5,1001)(   DZ(I,J),J=1,NDPW) INPU0117
  READ(5,1001)( WPHI(I,J),J=1,NDPW) INPU0118
  READ(5,1001)(DWPHI(I,J),J=1,NDPW) INPU0119
60 CONTINUE                   INPU0120
  READ(5,2034)N               INPU0121
  NDP=N+1                   INPU0122
  READ(5,5000)(FMS(K),K=1,N) INPU0123
  READ(5,5000)(AMASS(J),J=1,NDP) INPU0124
  READ(5,5000)(THETN(J),J=1,NDP) INPU0125
103 READ(5,5000)COL           INPU0126
  DO 50 I=1,MR
    READ(5,1001)(   W(I,J),J=1,NDP ) INPU0127
    READ(5,1001)(   V(I,J),J=1,NDP ) INPU0128
    READ(5,1001)(   DW(I,J),J=1,NDP ) INPU0129
    READ(5,1001)(   DV(I,J),J=1,NDP ) INPU0130
    AKP0(I)=DW(I,1)*TAN(DEL3)*(-1.0) INPU0131
50 CONTINUEF                  INPU0132
  IF(ITYPF.EQ.1) GO TO 100 INPU0133
  READ(5,5000)PRAM0          INPU0134
  DO 52 I=1,MR
    READ(5,1001)( WCOL(I,J),J=1,NDP ) INPU0135
    READ(5,1001)( VCOL(I,J),J=1,NDP ) INPU0136
    READ(5,1001)( DWCOL(I,J),J=1,NDP ) INPU0137
    READ(5,1001)( DVCOL(I,J),J=1,NDP ) INPU0138
    AKP0(I)=DWCOL(I,1)*TAN(DEL3)*(-1.0) INPU0139
52 CONTINUE                   INPU0140
  DO 200 I=1,4               INPU0141

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	BLAM0(I)=BRAM0(I)/OMEGA**2	INPU0145
	SRM0(I)=SORT(BLAM0(I))	INPU0146
200	CONTINUE	INPU0147
100	CONTINUE	INPU0148
	IF(INDF.EQ.18) GO TO 101	INPU0149
	DO 305 I=4,6	INPU0150
	DO 305 J=1,NDPW	INPU0151
	G(I,J)=0.0	INPU0152
	DG(I,J)=0.0	INPU0153
	Z(I,J)=0.0	INPU0154
	DZ(I,J)=0.0	INPU0155
	WPHI(I,J)=0.0	INPU0156
	DWPHI(I,J)=0.0	INPU0157
305	CONTINUE	INPU0158
	DO 307 I=3,4	INPU0159
	DO 306 J=1,NDP	INPU0160
	W(I,J)=0.0	INPU0161
	DW(I,J)=0.0	INPU0162
	V(I,J)=0.0	INPU0163
306	DV(I,J)=0.0	INPU0164
307	AKPC(I)=0.0	INPU0165
	IF(ITYPE.EQ.0) GO TO 101	INPU0166
	DO 308 I=3,4	INPU0167
	DO 309 J=1,NDP	INPU0168
	WCOL(I,J)=0.0	INPU0169
	DWCOL(I,J)=0.0	INPU0170
	VCOL(I,J)=0.0	INPU0171
309	DVCOL(I,J)=0.0	INPU0172
308	AKPOL(I)=0.0	INPU0173
101	CONTINUE	INPU0174
	DO 22 I=1,NDP	INPU0175
	THETA(I)=THETN(I)+COL	INPU0176
22	CONTINUE	INPU0177
	DO 6 I=1,4	INPU0178
	BLAM(I)=BRAM(I)/OMEGA**2	INPU0179
6	SBM(I)=SORT(BLAM(I))	INPU0180

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DO 5 I=1,6 INPU0181
WLAM(I)=WRAM(I)/OMEGA**2 INPU0182
5 SWG(I)=SQRT(WLAM(I)) INPU0183
DO 30 I=1,6 INPU0184
TT(I,1)=G(I,NDPW) INPU0185
TT(I,2)=Z(I,NDPW) INPU0186
TT(I,3)=DZ(I,NDPW) INPU0187
TT(I,4)=WPHT(I,NDPW) INPU0188
TT(I,5)=-DG(I,NDPW) INPU0189
CONTINUE INPU0190
IF(TFLT.EQ.0.0) GO TO 23 INPU0191
DO 24 I=1,6 INPU0192
24 TT(I,5)=0.0 INPU0193
23 CONTINUE INPU0194
DO 40 I=1,6 INPU0195
DO 40 J=1,6 INPU0196
40 C(I,J)=DZ(I,NDPW)*WPHT(J,NDPW)-DZ(J,NDPW)*WPHT(I,NDPW) INPU0197
ALOCK=ROH*CL*CHOD*R**4/AIB INPU0198
AND=FLOAT(NOBLD) INPU0199
HR=HMAST/R INPU0200
SNOMEG=SIGN(1.0,OMEGA) INPU0201
2034 FORMAT(12) INPU0202
5003 FORMAT(80A1) INPU0203
5001 FORMAT(11) INPU0204
5000 FORMAT(1E10.0) INPU0205
1001 FORMAT(6F13.5) INPU0206
C **** * PRINT OUT OF INPUT DATA **** *
5002 WRITE(6,5002) (DES(I),I=1,80) INPU0208
5002 FORMAT(//10X,100(1H*),//20X,80A1,//10X,100(1H*)//1 INPU0209
5004 WRITE(6,5004) ITYPE,TFLT, TDOF,IRFS,IEIGEN ,IFRMAG INPU0210
5004 FORMAT(//10X,'ITYPE=',I2,3X,'IFLT=',I2-3X,'TDOF=',I2-3X,'IRFS=',I2-3X,'IEIGEN=',I2-3X,'IFRMAG=',I2-3X) INPU0211
5004 & WRITE(6,1)NOBLD,ROH,CHOD,AIB ,HMAST,ALOCK INPU0212
1 FORMAT(// T4,'NO OF BLADES',T25,'ROH',T41,'CHORD',T59,'IB' INPU0213
$ ,T74,'HMAST',T94,'LOCK NO', INPU0214
</// T7,I2,T18,5(1PF15.7,2X)) INPU0215
1 INPU0216

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1      WRITE(6,2)OMEGA,R,VFL,CL,CD,PARMA
2      FORMAT(/// T6,'OMEGA',T25,'P',T41,'VFL',T59,'CL',T74,'CD'
#,T94,'PARMA'           //1X, 6(1PE15.7,2X))
3      WRITE(6,61) COL    ,DEL3
4      FORMAT(///T6,'COLLECTIVE PITCH',T25,'DEL3'  //1X,2(1PE15.7,2X))
5      WRITE(6,3)WL,WODD,WCL,WCD,WCMD,WCMR
6      FORMAT(/// T6,'WING L',T25,'WING CHOD',T41,'WING CL',T59,'WING CD'
%,T74,'WING CMO',T94,'WING CMA'
*///1X ,6(1PE15.7,2X))
7      WRITE(6,4)EDTS,WTHET
8      FORMAT(/// T6,'DISTANCE AC FA',T25,'WING ALPHAH'
@///1X ,2(1PE15.7,2X))
9      WRITE(6,250)
10     FORMAT(///1X,35(1H-)//1X,'EIGENVALUES ( NATURAL FREQUENCIES )'
11       /1X,35(1H-)//2X,'--( RAD/SEC )**2--')
12     IF(ITYPE.EQ.0) GO TO 254
13     WRITE(6,251)(RRA(1),I=1,MR)
14
15  251     FORMAT(/1X,' **BLADE COLLECTIVE**'/4X,4(F12.3,3X))
16     WRITE(6,252)
17  252     FORMAT(/1X,' **BLADE CYCLIC**')
18     GO TO 255
19  254     WRITE(6,253)
20  253     FORMAT(/1X,' **BLADE**')
21  255     WRITE(6,256)(RRA(1),I=1,MR)
22  256     FORMAT(4X,4(F12.3,3X))
23  257     WRITE(6,257)(WRA(1),J=1,MW)
24  257     FORMAT(/1X,' **WTNG**'/4X,6(F12.3,3X))
25  258     WRITE(6,408)
26  408     FORMAT(/2X,'-- RAD/SEC/OMEGA --')
27     IF(ITYPE.EQ.0) GO TO 354
28     WRITE(6,351)(SBM(1),J=1,MR)
29  351     FORMAT(/1X,' **BLADE COLLECTIVE/OMEGA**'/4X,4(F12.3,3X))
30     WRITE(6,352)
31  352     FORMAT(/1X,' **BLADE CYCLIC/OMEGA**')
32     GO TO 355
33  354     WRITE(6,353)

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353 FORMAT(1X,' **BLADE/OMEGA**') INPU0253
355 WRITE(6,356)(SBM(I),I=1,MB) INPU0254
356 FORMAT(4X,4(F12.3,3X)) INPU0255
357 WRITE(6,357)(SWG(I),I=1,MW) INPU0256
357 FORMAT(1X,' **WTNG/OMEGA**')/4X,6(F12.3,3X)) INPU0257
357 WRITE(6,409) INPU0256
409 FORMAT(//1X,'EXCITING FORCE COMPONENTS') INPU0259
409 WRITE(6,358)CGUST INPU0260
358 FORMAT( //T6,'U GUST',T25,'V GUST', T41,'W GUST', T59,
*           'THETA 0',T74,'THETA 10', T94,'THETA 15',/ /1X,
*           6(1PE15.7,2X)) INPU0261
358 DO 420 I=1,MR INPU0262
420 DO 431 J=1,NDP INPU0263
420 PIG(I)=0.0 INPU0264
420 PA=ABS(W(I,J)) INPU0265
420 IF(PA .GT. PIG(I)) 460,460,461 INPU0266
420 PIG(I)=PA INPU0267
420 PA=ABS(V(I,J)) INPU0268
420 IF(PA .GT. PIG(I)) 431,431,462 INPU0269
420 BIG(I)=PA INPU0270
420 CONTINUE INPU0271
431 462 BIG(I)=PA INPU0272
431 CONTINUE INPU0273
430 463 BMAX(I)=BIG(I) INPU0274
430 DO 435 I=1,MW INPU0275
430 DO 436 J=1,NDPW INPU0276
430 BIG(I)=0.0 INPU0277
430 PA=ABS(G(I,J)) INPU0278
430 IF(PA .GT. BIG(I)) 465,465,466 INPU0279
430 PIG(I)=PA INPU0280
430 PA=(Z(I,J)) INPU0281
430 IF(PA .GT. PIG(I)) 436,436,467 INPU0282
430 BIG(I)=PA INPU0283
436 CONTINUE INPU0284
435 467 WMAX(I)=BIG(I) INPU0285
435 IF(ITYPE.EQ.0) GO TO 480 INPU0286
435 DO 440 I=1,MR INPU0287
435 DO 441 J=1,NDP INPU0288

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801
      PIG(I)=0.0
      PA=ABS(WCOL(I,J))
      IF(PA      -RIG(I)) 470,470,471
      BIG(I)=PA
      471 PA=ABS(VCOL(I,J))
      IF(PA      -RIG(I)) 441,441,472
      BIG(I)=PA
      472 CONTINUE
      441 BOMAX(I)=RIG(I)
      GO TO 487
      480 DO 481 I=1,MB
      481 BOMAX(I)=BMAX(I)
      487 CONTINUE
      DO 475 I=1,MB
      FRB(I)=BMAX(I)      /R
      FRB0(I)=BOMAX(I)    /R
      475 CONTINUE
      DO 476 I=1,MW
      FRW(I)=WMAX(I)      /WL
      476 CONTINUE
      FPW(3)=ABS(WPHI(3,NDPW))
      IDEBUG=0
      IF( IDEBUG.EQ.0) GO TO 477
      WRITE(6,50051)(BMAX(I),I=1,MB),(BOMAX(I),I=1,MB),(WMAX(I),I=1,MW)
      5005 FORMAT(///(10X,E15.7/))
      477 CONTINUE
      RETURN
      END
      INPU0289
      INPU0290
      INPU0291
      INPU0292
      INPU0293
      INPU0294
      INPU0295
      INPU0296
      INPU0297
      INPU0298
      INPU0299
      INPU0300
      INPU0301
      INPU0302
      INPU0303
      INPU0304
      INPU0305
      INPU0306
      INPU0307
      INPU0308
      INPU0309
      INPU0310
      INPU0311
      INPU0312
      INPU0313
      INPU0314
      INPU0315
      INPU0316

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SUBROUTINE INTPL INTPO001
 C INTPO002
 C INTERPOLATION FOR THE NUMERICAL INTEGRATION INTPO003
 C INTPO004
 C INTERPOLATION FUNCTION-----HERMIT INTERPOLATION(2 POINTS) INTPO005
 C INTERPOLATION FUNCTION---LAGRANGIAN INTERPOLATION FOR THE ANGLE OF TWIST INTPO006
 COMMON/THE/THETN(21),MB,MW INTPO007
 COMMON /PARMT/ ITYPE,IFLT INTPO008
 COMMON /AREA1/DMEGA,R,VEL,CL,CD,RAMDA,SNOMFG INTPO009
 COMMON/WICH/WL,WCDP,WCL,WCD,WCMO,WCMC,EDIS,WTHET,VV INTPO010
 DIMENSION WX(21) INTPO011
 COMMON/WING/ NW,NDPW,EMSW(20),G(6,21),DG(6,21),Z(6,21),DZ(6,21), INTPO012
 *WPHI(6,21),DWPHI(6,21) INTPO013
 DIMENSION GT(6,20),ZI(6,20),WPHII(6,20) INTPO014
 COMMON/WIMOD/STR(20,3,6),TSTR(20,6,3) INTPO015
 DIMENSION XX(21) INTPO016
 COMMON/GIN/ V(4,21),W(4,21),DV(4,21),DW(4,21),THETA(21), INTPO017
 *EMS(20),AMASS(20),N,NDP INTPO018
 COMMON/GINO/ VCOL(4,21),WCOL(4,21),DVCOL(4,21),DWCOL(4,21) INTPO019
 COMMON/AREA3/V1(4,20),WI(4,20),THETAI(20),AMASSI(20) INTPO020
 * ,VICOL(4,20),WICOL(4,20) INTPO021
 COMMON /AREA2/NPT,XXX(20),A(20) INTPO022
 IDEBUG=0 INTPO023
 WRITE(6,50) INTPO024
 50 FORMAT(//1X,'***** BLADE MODE SHAPES *****') INTPO025
 XX(1)=0,0 INTPO026
 DU 8; I=1,N INTPO027
 XX(I+1)=XX(I)+EMS(I) INTPO028
 80 CONTINUE INTPO029
 IF(ITYPE.EQ.1) GOTO 100 INTPO030
 WRITE(6,51) INTPO031
 51 FORMAT(1X,'--- COLLECTIVE MODES ---') INTPO032
 DO 36 I=1,MB INTPO033
 WRITE(6,4500) INTPO034
 WRITE(6,4999) INTPO035
 WRITE(6,30)(J,XX(J),VCOL(I,J),DVCOL(I,J),WCOL(I,J),DWCOL(I,J), INTPO036

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*      J=1,NDP)
36  CONTINUE
      WRITE(6,52)
52  FORMAT(//1X,'--- CYCLIC MODES ---')
100 CONTINUE
      DO 35 I=1,MR
      WRITE(6,4500)I
4500 FORMAT(// 1X,'I=' ,I1)
      WRITE(6,4999)
4999 FORMAT(  T5,'J',T13,'XX(J)',T33,'V(I,J)',T53,'DV(I,J)',T73,'W(I
%,J)',T93,'DW(I,J)')
      WRITE(6,3)(J,XX(J),V(I,J),DV(I,J),W(I,J),DW(I,J),J=1,NDP)
3   FORMAT(1X,      I4,5(5X,E15.7)))
35  CONTINUE
      WRITE(6,5999)
5999 FORMAT(// T5,'J',T13,'XX(J)',T33,'THETN(J)',T53,'AMASS(J)')
      WRITE(6,4)(J,XX(J),THETN(J),AMASS(J),J=1,NDP)
4   FORMAT(1X,      I4,3(5X,E15.7)))
      DO 70 II=1,NPT
      DO 60 I=1,NDP
      IF(XX(I).GE.XXX(II)) GO TO 110
60  CONTINUE
110 EA=XX(I)-XX(I-1)
      EB=XX(I)+XX(I-1)
      XKSI=2.0/EA*XXX(II)-EB/EA
      F1=(XKSI+2.0)*(XKSI-1.0)**2/4.0
      F2=(2.0-XKSI)*(XKSI+1.0)**2/4.0
      G1=(XKSI+1.0)*(XKSI-1.0)**2/4.0
      G2=(XKSI-1.0)*(XKSI+1.0)**2/4.0
      F1L=(1.0-XKSI)/2.0
      F2L=(1.0+XKSI)/2.0
      DO 90 JJ=1,4
      VI(JJ,II)=V(JJ,I-1)*F1+V(JJ,I)*F2+(DV(JJ,I-1)*G1+DV(JJ,I)*G2)
      &*EA/2.0*R
      WI(JJ,II)=W(JJ,I-1)*F1+W(JJ,I)*F2+(DW(JJ,I-1)*G1+DW(JJ,I)*G2)
      &*EA/2.0*R

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INTP0037
INTP0038
INTP0039
INTP0040
INTP0041
INTP0042
INTP0043
INTP0044
INTP0045
INTP0046
INTP0047
INTP0048
INTP0049
INTP0050
INTP0051
INTP0052
INTP0053
INTP0054
INTP0055
INTP0056
INTP0057
INTP0058
INTP0059
INTP0060
INTP0061
INTP0062
INTP0063
INTP0064
INTP0065
INTP0066
INTP0067
INTP0068
INTP0069
INTP0070
INTP0071
INTP0072

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IF(ITYPE.EQ.0)GO TO 90                                INTP0073
VICOL(JJ,II)=VCOL(JJ,I-1)*F1+VCOL(JJ,I)*F2+(DVCOL(JJ,I-1)*G1
* +DVCOL(JJ,I)*G2)*EA/2.0*R                         INTP0074
WICOL(JJ,II)=WCOL(JJ,I-1)*F1+WCOL(JJ,I)*F2+(DWCOL(JJ,I-1)*G1
* +DWCOL(JJ,I)*G2)*EA/2.0*R                         INTP0075
90 CONTINUE                                              INTP0076
AMASSI(II)=AMASS(I-1)*F1L+AMASS(I)*F2L                INTP0077
THETAI(II)=THETA(I-1)*F1L+THETA(I)*F2L                INTP0078
70 CONTINUE                                              INTP0079
IF(IDEBUG.EQ.0) GO TO 400                            INTP0080
WRITE(6,5048)                                         INTP0081
5048 FORMAT(/// T5,'J',T13,'XXX(J)',T33,'VI(1,J)',T53,'WI(1,J)',T73,
@'VI(2,J)',T93,'WI(2,J)')
WRITE(6,3)(JJ,XXX(JJ),VI(1,JJ),WI(1,JJ),VI(2,JJ),WI(2,JJ),JJ=1,
%NPT)                                                 INTP0082
WRITE(6,5047)                                         INTP0083
5047 FORMAT(/// T5,'J',T13,'XXX(J)',T33,'VI(3,J)',T53,'WI(3,J)',T73,
@'VI(4,J)',T93,'WI(4,J)')
WRITE(6,3)(JJ,XXX(JJ),VI(3,JJ),WI(3,JJ),VI(4,JJ),WI(4,JJ),JJ=1,
%NPT)                                                 INTP0084
WRITE(6,5046)                                         INTP0085
5046 FORMAT(/// T5,'J',T13,'XXX(J)',T33, 'AMASSI(J)',T53,'THETAI(J)')
WRITE(6,4)(JJ,XXX(JJ),AMASSI(JJ),THETAI(JJ),JJ=1,NPT) INTP0086
400 CONTINUE                                              INTP0087
WRITE(6,53)                                         INTP0088
53 FORMAT(///1X,'***** WING MODE SHAPES *****')
WX(1)=0.0                                              INTP0089
DO 81 I=1,NW                                         INTP0090
WX(I+1)=WX(I)+EMSW(I)                                INTP0091
81 CONTINUE                                              INTP0092
DO 38 II=1,MW                                         INTP0093
WRITE(6,7000)II                                         INTP0094
7000 FORMAT(/// 1X,'II=',II)
WRITE(6,7001)                                         INTP0095
7001 FORMAT(     T5,'J',T9,'WX(J)',T25,'G(II,J)',T41,'DG(II,J)',T57,
* 'Z(II,J)',T73,'DZ(II,J)',T89,'WPHI(II,J)',T105,'DWPHI(II,J)') INTP0096
* INTP0097
* INTP0098

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      WRITE(6,5)(J,WX(J),G(IJ,J),DG(IJ,J),Z(IJ,J),DZ(IJ,J),WPHI(IJ,J),
5      %DWPHI(IJ,J),J=1,NPT)
      FORMAT((1X,        T4,7(1X,E15.7)))
      CONTINUE
      DO 10 II=1,NPT
      DO 20 I=1,NDPW
      IF(WX(I).GE.XXX(I)) GO TO 220
20      CONTINUE
      220  WEA=WX(I)-WX(I-1)
      WEB=WX(I)+WX(I-1)
      XKSI=2.0/WEA*XXX(I)-WEB/WEA
      F1=(XKSI+2.0)*(XKSI-1.0)**2/4.0
      F2=(2.0-XKSI)*(XKSI+1.0)**2/4.0
      G1=(XKSI+1.0)*(XKSI-1.0)**2/4.0
      G2=(XKSI-1.0)*(XKSI+1.0)**2/4.0
      DO 37 IJ=1,6
      GI(IJ,II)=G(IJ,I-1)*F1+G(IJ,I)*F2+(DG(IJ,I-1)*G1+DG(IJ,I)*G2)*
      *WEA/2.0 *WL
      ZI(IJ,II)=Z(IJ,I-1)*F1+Z(IJ,I)*F2+(DZ(IJ,I-1)*G1+DZ(IJ,I)*G2)*
      *WEA/2.0 *WL
      WPHII(IJ,II)=WPHI(IJ,I-1)*F1+WPHI(IJ,I)*F2+(DWPHI(IJ,I-1)*G1+
      @DWPHI(IJ,I)*G2)*WEA/2.0*WL
      STR(IJ,1,IJ)=GI(IJ,II)
      STR(IJ,2,IJ)=ZI(IJ,II)
      STR(IJ,3,IJ)=WPHII(IJ,II)
      TSTR(IJ,IJ,1)=GI(IJ,II)
      TSTR(IJ,IJ,2)=ZI(IJ,II)
      TSTR(IJ,IJ,3)=WPHII(IJ,II)
37      CONTINUE
10      CONTINUE
      IF(105BUG.E0.0) GO TO 401
      WRITE(6,7)03)
7003  FORMAT(/// T5,'J',T9,'XXX(J)',T25,'GI(1,J)',T41, 'HI(1,J)',T57,
      %'WPHII(1,J)',T73,'GI(2,J)',T89,'H(2,J)',T105,'WPHII(2,J)')
      WRITE(6,5)(J,XXX(J),GI(1,J),ZI(1,J),WPHI(1,J),GI(2,J),ZI(2,J),
      @WPHII(2,J),J=1,NPT)

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	WRITE(6,7004)	INTP0145
7004	FORMAT(/// T5,'J',T9,'XXX(J)',T25,'GI(3,J)',T41, 'HI(3,J)',T57, 8'WPHII(3,J)',T73,'GI(4,J)',T89,'H(4,J)',T105,'WPHII(4,J)' WRITE(6,5)(J,XXX(J),GI(3,J),ZI(3,J),WPHII(3,J),GI(4,J),ZI(4,J), @WPHII(4,J),J=1,NPT) WRITE(6,7005)	INTP0146 INTP0147 INTP0148 INTP0149 INTP0150
7005	FORMAT(/// T5,'J',T9,'XXX(J)',T25,'GI(5,J)',T41, 'HI(5,J)',T57, 8'WPHII(5,J)',T73,'GI(6,J)',T89,'H(6,J)',T105,'WPHII(6,J)' WRITE(6,5)(J,XXX(J),GI(5,J),ZI(5,J),WPHII(5,J),GI(6,J),ZI(6,J), @WPHII(6,J),J=1,NPT)	INTP0151 INTP0152 INTP0153 INTP0154
401	CONTINUE RETURN END	INTP0155 INTP0156 INTP0157

SUBROUTINE AERODT

C TO DEFINE THE AERODYNAMIC COEFFICIENTS AT THE POINTS OF GAUSSIAN
 C QUADRATURE

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COMMON /PARMT/  ITYPE ,IFLT
COMMON /AREAL/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /AREA6/NORLD,RCH,CHOD,AIB,CK,FMAST ,ALOCK ,AND,HR
COMMON /AREA2/NPT,XXX(20),A(20)
COMMON /AREA3/VI(4,20),WI(4,20),THETAI(20) ,AMASSI(20)
1           ,VICOL(4,20),WICCL(4,20)
COMMON/AREA4/H(4,4,20),HI(4,20),HII(4,20),HRZ(4,20),HNR(4,20),
%WO(4,20),VO(4,20),W1(4,20),VI(4,20)
2           ,OHI(4,4,20),OWO(4,20),OV1(4,20),OHIII(4,20),CHIII(4,20)
3           ,CHV(4,20),OHIV(4,20)
COMMON/AKKH/FT1P1(20),FT1P0(20),FT2P1(20), FZ2P0(20),
/FZ2P0(20),FZ1P1(20),FZ2P2(20)
4           ,FT3P0(20),FT3P1(20),FZ3P0(20),FZ3P1(20)
COMMON/ADFE/HIII(4,20),HIV(4,20),HV(4,20),HVI(4,20),HVII(4,20)
COMMON/WINDD/STR(20,3,6),TSTR(20,6,3)
COMMON/WICH/WL,WCD,WCL,WCD,WCMD,WCMA,EDIS,WTHET,VV
COMMON/WINGAR/TSDS(20,6,6),TSAS(20,6,6),TSAG(20,6,3)
DIMENSION DAWA(3,3),AWA(3,3),AWG(3,3)
DIMENSION TSDF(20,6,3),TSA(20,6,3)
DO 1 I=1,3
DO 1 J=1,3
DAWA(I,J)=0.0
AWA(I,J)=0.0
1 AWG(I,J)=0.0
DO 2 I=1,20
DO 2 J=1,6
DO 2 K=1,3
TSDA(I,J,K)=0.0
2 TSA(I,J,K)=0.0
CK=-0.5*ROH*CL*CHOD*R**4
CA=CD/CL

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AER00001
 AER00002
 AER00003
 AER00004
 AER00005
 AER00006
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 AER00008
 AER00009
 AER00010
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 AER00036

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CA1=1.0+CA          AER00037
CA2=1.0-CA          AER00038
ARAMCA=RAMDA        AER00039
RAMCA=ABS(RAMDA)    AER00040
DO 11  JJ=1,NPT     AER00041
XSQ=SGRT(RAMDA**2+XXX(JJ)**2)  AER00042
TAU0=1.0/XSQ        AER00043
TAU1=XXX(JJ)/XSQ    AER00044
TAU2=XXX(JJ)**2/XSQ  AER00045
TAU3=XXX(JJ)**3/XSQ  AER00046
ALPHA=THETAI(JJ)-ATAN( RAMCA/XXX(JJ) )+ATAN( RAMDA*4.0/3.0) AER00047
FTH0=RAMDA**3*ALPHA+TAU0+RAMCA**2 *CA*TAU1+RAMDA*ALPHA*TAU2
/CA*TAU3            AER00048
FTH1=RAMDA**2*CA1*TAU0+RAMCA*ALPHA+TAU1+2.0*CA*TAU2          AER00049
FTH2=2.0*RAMDA**2*ALPHA*TAU0-RAMDA*CA2*TAU1+ALPHA*TAU2        AER00050
FTH3=RAMDA**3*TAU0+RAMCA*TAU2          AER00051
FTHC=-FTH0*SNOPEG          AER00052
FTH1=-FTH1          AER00053
FTH2=-FTH2*SNOPEG          AER00054
FTH3=-FTH3*SNOPEG          AER00055
FZ0=-RAMDA**3*CA*TAU0+RAMDA**2*ALPHA*TAU1 -RAMDA*CA*TAU2        AER00056
/ALPHA*TAU3          AER00057
FZ1=RAMDA**2*ALPHA*TAU0+RAMCA*CA2*TAU1+2.0*ALPHA*TAU2          AER00058
FZ2=-2.0*RAMDA**2*CA*TAU0+RAMCA*ALPHA*TAU1-CA1*TAU2          AER00059
FZ3=RAMDA**2*TAU1+TAU3          AER00060
FZ1=FZ1*SNOPEG          AER00061
DO 200 J=1,4          AER00062
DO 100 I=1,4          AER00063
H(J,I,JJ)=FTH1*VI(J,JJ)*VI(I,JJ)+FZ1*WI(J,JJ)*VI(I,JJ)+FTH2*
  @VI(J,JJ)*WI(I,JJ)+FZ2*WI(J,JJ)*WI(I,JJ)          AER00064
  IF(ITYPE.EQ.0) GO TO 100          AER00065
  CH(J,I,JJ)=FTH1*VICOL(J,JJ)*VICOL(I,JJ)+FZ1*WICOL(J,JJ)*
  @VICOL(I,JJ)+FTH2*VICOL(J,JJ)*WICOL(I,JJ)+FZ2*WICOL
  @ (J,JJ)*WICOL(I,JJ)          AER00066
100  CONTINUE          AER00067
  HI(J,JJ)=FTH1*VI(J,JJ)+FZ1*WI(J,JJ)          AER00068
  @          AER00069
  @          AER00070
  @          AER00071
  @          AER00072

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116

HII (J, JJ) = (FTH2*VI (J, JJ) + FZ2*WI (J, JJ)) * XXX (JJ) AER00073
HRZ (J, JJ) = FTH2*VI (J, JJ) + FZ2*WI (J, JJ) AER00074
HNR (J, JJ) = (FTH1*VI (J, JJ) + FZ1*WI (J, JJ)) * XXX (JJ) AER00075
WD (J, JJ) = AMASSI (JJ) * WI (J, JJ) AER00076
VO (J, JJ) = AMASSI (JJ) * VI (J, JJ) AER00077
WI (J, JJ) = AMASSI (JJ) * WI (J, JJ) * XXX (JJ) AER00078
VI (J, JJ) = AMASSI (JJ) * VI (J, JJ) * XXX (JJ) AER00079
HIII (J, JJ) = FTH1*VI (J, JJ) + FTH2*WI (J, JJ) AFR00080
HIV (J, JJ) = HIII (J, JJ) * XXX (JJ) AER00081
HV (J, JJ) = FZ1*VI (J, JJ) + FZ2*WI (J, JJ) AER00082
HVI (J, JJ) = HV (J, JJ) * XXX (JJ) AER00083
HVII (J, JJ) = FZ0*VI (J, JJ) - FTH0*WI (J, JJ) AER00084
CHIII (J, JJ) = FZ3*WI (J, JJ) + FTH3*VI (J, JJ) AER00085
IF (ITYPE.EQ.0) GO TO 200 AER00086
OWE (J, JJ) = AMASSI (JJ) * WICOL (J, JJ) AER00087
OV1 (J, JJ) = AMASSI (JJ) * VICOL (J, JJ) * XXX (JJ) AFR00088
HRZ (J, JJ) = FTH2*VICOL (J, JJ) + FZ2*WICOL (J, JJ) AER00089
HNR (J, JJ) = (FTH1*VICOL (J, JJ) + FZ1*WICOL (J, JJ)) * XXX (JJ) AFR00090
HHTII (J, JJ) = FZ3*WICOL (J, JJ) + FTH3*VICOL (J, JJ) AER00091
OHV (J, JJ) = FZ1*VICOL (J, JJ) + FZ2*WICOL (J, JJ) AER00092
CHIV (J, JJ) = (FTH1*VICOL (J, JJ) + FTH2*VICOL (J, JJ)) * XXX (JJ) AER00093
200 CONTINUE AER00094
C AER0 FOR WING DUE TO BLADES AER00095
FT0P1 (JJ) = FTH0*XXX (JJ) AER00096
FT1P0 (JJ) = FTH1 AER00097
FT1P2 (JJ) = FTH1*XXX (JJ)**2 AER00098
FT2P1 (JJ) = FTH2*XXX (JJ) AER00099
FZ0P0 (JJ) = FZ0 AFR00100
FZ1P1 (JJ) = FZ1*XXX (JJ) AER00101
FZ2P0 (JJ) = FZ2 AER00102
FZ2P2 (JJ) = FZ2*XXX (JJ)**2 AER00103
FT3P0 (JJ) = FTH3 AER00104
FT3P1 (JJ) = FTH3*XXX (JJ) AER00105
FZ3P0 (JJ) = FZ3 AER00106
FZ3P1 (JJ) = FZ3*XXX (JJ) AER00107
11 CONTINUE AER00108

C AERO FOR WING DUE TO ITSELF AERO0109
 RAMDA=ARAMDA
 RC=R0H*WC00 AERO0110
 DAWA(1,1)=-0.5*RC*VEL*(WCL+WCD) AERO0111
 DAWA(1,2)=RC*WCL*WTHET*VEL AERO0112
 DAWA(2,1)=-0.5*RC*WCL*WTHET*VEL AERO0113
 DAWA(2,2)=-RC*WCD*VEL AERO0114
 DAWA(3,1)=-0.5*RC*WC00*VEL*(WCL*EDIS+WCMA) AERO0115
 DAWA(3,2)=RC*WC00*(WC00+WCMA*WTHET+WCL*WTHET*EDIS)*VEL AERO0116
 AWA(1,3)=0.5*RC*WCL*VEL**2 AERO0117
 AWA(3,3)=0.5*RC*WC00*VEL**2*(WCMA+WCL*EDIS) AERO0118
 AWG(1,1)=DAWA(1,1)*VEL AERO0119
 AWG(1,3)=DAWA(1,2)*VEL AERO0120
 AWG(2,1)=DAWA(2,1)*VEL AERO0121
 AWG(2,3)=DAWA(2,2)*VEL AERO0122
 AWG(3,1)=DAWA(3,1)*VEL AERO0123
 AWG(3,3)=DAWA(3,2)*VEL AERO0124
 DO 501 II=1,NFT AERO0125
 DO 502 I=1,6 AERO0126
 DO 502 J=1,3 AERO0127
 DO 502 K=1,3 AERO0128
 TSDA(II,I,J)=TSTR(II,I,K)*DAWA(K,J)+TSDA(II,I,J) AERO0129
 TSA(II,I,J)=TSTR(II,I,K)*AWA(K,J)+TSA(II,I,J) AERO0130
 TSAG(II,I,J)=TSTR(II,I,K)*AWG(K,J)+TSAG(II,I,J) AERO0131
 502 CONTINUE AERO0132
 DO 503 I=1,6 AERO0133
 DO 503 J=1,6 AERO0134
 DO 503 K=1,3 AERO0135
 TS0S(II,I,J)=TSDA(II,I,K)*STR(II,K,J)+TS0S(II,I,J) AERO0136
 TSAS(II,I,J)=TSA(II,I,K)*STR(II,K,J)+TSAS(II,I,J) AERO0137
 503 CONTINUE AERO0138
 501 CONTINUE AERO0139
 RETURN AERO0140
 END AERO0141
 AERO0142

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SUBROUTINE CRDINT

C TO DEFINE THE ORDER OF NUMERICAL INTEGRATION

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COMMON /PARMT/  ITYPE ,IFLT          ORDI0001
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG  ORDI0002
COMMON /AREA6/NOBLD,ROH,CHOD,AIB,CK,HMAST ,ALOCK ,ANO,HR  ORDI0003
COMMON/AREA5/AH(4,4),AH1(4),AHII(4),AHRZ(4),AHNR(4),AWC(4),AVD(4)  ORDI0004
@,AW1(4),AV1(4),DAH(4,4),DAW0(4),DAV1(4),DAHIII(4),CAHIII(4)  ORDI0005
@,DAHV(4),DAHIV(4)  ORDI0006
COMMON/AERO/AFTOP1,AFT1P0,AFT1P2,AFT2P1,AFZ0P0,AFZ1P1,AFZ2P0,  ORDI0007
@AFZ2P2,AHIII(4),AHIV(4),AHV(4),AHVI(4),AHVII(4)  ORDI0008
@,AFT3P0,AFT3P1,AFZ3P0,AFZ3P1  ORDI0009
COMMON/WICH/WL,WCD0,WCL,WCD,WCMQ,WCMR,EDIS,WTHET,VV  ORDI0010
COMMON/ARWNG/DARWA(6,6),ARWA(6,6),ARWG(6,3)  ORDI0011
IDEBUG=0  ORDI0012
NN=1  ORDI0013
DO 100 JQ=1,4  ORDI0014
DO 100 IQ=1,4  ORDI0015
CALL INTEG(FSUM,NN,JQ,IQ)  ORDI0016
AH(JQ,IQ)=CK*FSUM/R**2  ORDI0017
100  CONTINUE  ORDI0018
NK=NN  ORDI0019
1000 NN=NN+1  ORDI0020
DO 200 JQ=1,4  ORDI0021
CALL INTEG(FSUM,NN,JQ,IQ)  ORDI0022
FSUM=FSUM*CK/R  ORDI0023
NM=NN-NK  ORDI0024
GO TO (2,3,4,5),NM  ORDI0025
2  AH1(JQ)=FSUM  ORDI0026
GO TO 200  ORDI0027
3  AHII(JQ)=FSUM  ORDI0028
GO TO 200  ORDI0029
4  AHRZ(JQ)=FSUM  ORDI0030
GO TO 200  ORDI0031
5  AHNR(JQ)=FSUM  ORDI0032
GO TO 200  ORDI0033

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ORDI0034
ORDI0035
ORDI0036
ORDI0037
ORDI0038
ORDI0039
ORDI0040
ORDI0041
ORDI0042
ORDI0043
ORDI0044
ORDI0045
ORDI0046
ORDI0047
ORDI0048
ORDI0049
ORDI0050
ORDI0051
ORDI0052
ORDI0053
ORDI0054
ORDI0055
ORDI0056
ORDI0057
ORDI0058
ORDI0059
ORDI0060
ORDI0061
ORDI0062
ORDI0063
ORDI0064
ORDI0065
ORDI0066
ORDI0067
ORDI0068
ORDI0069
ORDI0070
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ORDI0072
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ORDI0074
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ORDI0115
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ORDI0135
ORDI0136

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200 CONTINUE ORDI0037
IF(NN.LT.5) GO TO 1000 ORDI0038
NK=NN ORDI0039
2000 NN=NN+1 ORDI0040
DO 300 JQ=1,4 ORDI0041
CALL INTEG(FSUM,NN,JQ,1Q) ORDI0042
FSUM=FSUM*R**2 ORDI0043
NM=NN-NK ORDI0044
GO TO (6,7,8,9),NM ORDI0045
6 AWQ(JQ)=FSUM ORDI0046
GO TO 300 ORDI0047
7 AVD(JQ)=FSUM ORDI0048
GO TO 300 ORDI0049
8 AW1(JQ)=FSUM ORDI0050
GO TO 300 ORDI0051
9 AV1(JQ)=FSUM ORDI0052
300 CONTINUE ORDI0053
IF(NN.LT.9) GO TO 2000 ORDI0054
NK=NN ORDI0055
3000 NN=NN+1 ORDI0056
CALL INTEG(FSUM,NN,JQ,1Q) ORDI0057
FSUM=FSUM*CK*ANO ORDI0058
NM=NN-NK ORDI0059
GO TO (10,11,12,13,14,15,16,17),NM ORDI0060
10 AFTOP1=FSUM ORDI0061
GO TO 400 ORDI0062
11 AFT1P1=FSUM ORDI0063
GO TO 400 ORDI0064
12 AFT1P2=FSUM ORDI0065
GO TO 400 ORDI0066
13 AFT2P1=FSUM ORDI0067
GO TO 400 ORDI0068
14 AFZOP0=FSUM ORDI0069
GO TO 400 ORDI0070
15 AFZ1P1=FSUM ORDI0071
GO TO 400 ORDI0072

16 AFZ2P0=FSUM ORDI0073
GO TO 400 ORDI0074
17 AFZ2P2=FSUM ORDI0075
400 IF(NN.LT.17) GO TO 3000 ORDI0076
NK=NN ORDI0077
4000 NN=NN+1 ORDI0078
DO 500 JQ=1,4 ORDI0079
CALL INTEG(FSUM,NN,JQ,IQ) ORDI0080
FSUM=FSUM/R*CK*ANO ORDI0081
NM=NN-NK ORDI0082
GO TO (18,19,20,21,22),NM ORDI0083
18 AHIII(JQ)=FSUM ORDI0084
GO TO 500 ORDI0085
19 AHIV(JQ)=FSUM ORDI0086
GO TO 500 ORDI0087
20 AHV(JQ)=FSUM ORDI0088
GO TO 500 ORDI0089
21 AHVI(JQ)=FSUM ORDI0090
GO TO 500 ORDI0091
120 22 AHVII(JQ)=FSUM ORDI0092
500 CONTINUE ORDI0093
IF(NN.LT.22) GO TO 4000 ORDI0094
NK=NN ORDI0095
5000 NN=NN+1 ORDI0096
DO 600 JQ=1,6 ORDI0097
DO 600 IQ=1,6 ORDI0098
CALL INTEG(FSUM,NN,JQ,IQ) ORDI0099
NM=NN-NK ORDI0100
GO TO (23,24),NM ORDI0101
23 FSUM=FSUM*WL/ABS(DMEGA) ORDI0102
CARWA(JQ, IQ)=FSUM ORDI0103
GO TO 600 ORDI0104
24 FSUM=FSUM*WL/DMEGA**2 ORDI0105
ARWA(JQ, IQ)=FSUM ORDI0106
600 CONTINUE ORDI0107
IF(NN.LT.24) GO TO 5000 ORDI0108

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NN=25          ORD10109
DO 700 JQ=1,6  ORD10110
DO 700 IQ=1,3  ORD10111
CALL INTEG(FSUM,NN,JQ,IC)  ORD10112
FSUM=FSUM*WL/OMEGA**2  ORD10113
ARWG(IQ,IQ)=FSUM  ORD10114
700 CONTINUE  ORD10115
NN=26          ORD10116
DO 801 JQ=1,4  ORD10117
CALL INTEG(FSUM,NN,JQ,IC)  ORD10118
FSUM=FSUM*CK/R  ORD10119
CAHIII(JQ)=FSUM  ORD10120
801 CONTINUE  ORD10121
NK=NN          ORD10122
2003 NN=NN+1  ORD10123
CALL INTEG(FSUM,NN,JQ,IQ)  ORD10124
FSUM=FSUM*CK*AND  ORD10125
NM=NN-NK  ORD10126
GOTO (27,28,29,30),NM  ORD10127
27 AFT3P0=FSUM  ORD10128
GO TO 2003  ORD10129
28 AFT3P1=FSUM  ORD10130
GO TO 2003  ORD10131
29 AFZ3P0=FSUM  ORD10132
GO TO 2003  ORD10133
30 AFZ3P1=FSUM  ORD10134
IF(IDEBUG.EQ.0) GO TO 450  ORD10135
WRITE(6,50)((AH(I,J),J=1,4),I=1,4)  ORD10136
50 FORMAT(///1X,2X, 'AH',4(T10.4(E15.7,2X)/1X ))  ORD10137
WRITE(6,51)AH1,AHII,AHRZ,AHNR,AHIII,AHIV,AHV,AHVI,AHVII,CAHIII  ORD10138
51 FORMAT(2X,'AH1',T10.4(E15.7,2X)
%      /2X,'AHII',      T10.4(E15.7,2X)  ORD10140
%      /2X,'AHRZ',      T10.4(E15.7,2X)  ORD10141
%      /2X,'AHNR',      T10.4(E15.7,2X)  ORD10142
*      /2X,'AHIII',      T10.4(E15.7,2X)  ORD10143
%      /2X,'AHIV',      T10.4(E15.7,2X)  ORD10144

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      *      /2X,'AHV',      T10,4(E15.7,2X)      ORDI0145
      *      /2X,'AHVI',      T10,4(E15.7,2X)      ORDI0146
      *      /2X,'AHVII',     T10,4(E15.7,2X)      ORDI0147
      *      /2X,'CAHIII',    T10,4(E15.7,2X)      ORDI0148
      *      WRITE(6,82) AFT3P0,AFT3P1,AFZ3P0,AFZ3P1  ORDI0149
82      *      FORMAT(2X,'AFT3P0'      ,T10,E15.7      ORDI0150
      *      /2X,'AFT3P1'      ,T10,E15.7      ORDI0151
      *      /2X,'AFZ3P0'      ,T10,E15.7      ORDI0152
      *      /2X,'AFZ3P1'      ,T10,E15.7      ORDI0153
450     CONTINUE
      IF(ITYPE.EQ.0) GO TO 851
      NN=NN+1
      DO 101 JQ=1,4
      DO 101 IQ=1,4
      CALL INTEG(FSUM,NN,JQ,IQ)
      OAH(JQ,IQ)=CK*FSUM/R**2
101     CONTINUE
      NK=NN
2001     NN=NN+1
      DO 301 JQ=1,4
      CALL INTEG(FSUM,NN,JQ,IQ)
      FSUM=FSUM*R**2
      NM=NN-NK
      GO TO (32,33),NM
32      OAW0(JQ)=FSUM
      GO TO 301
33      OAV1(JQ)=FSUM
301     CONTINUE
      IF(NN.LT.33) GO TO 2001
      NN=NN+1
      DO 302 JQ=1,4
      CALL INTEG(FSUM,NN,JQ,IQ)
      FSUM=FSUM*CK/R
      OAHIII(JQ)=FSUM
302     CONTINUE
      NN=NN+1
      ORDI0154
      ORDI0155
      ORDI0156
      ORDI0157
      ORDI0158
      ORDI0159
      ORDI0160
      ORDI0161
      ORDI0162
      ORDI0163
      ORDI0164
      ORDI0165
      ORDI0166
      ORDI0167
      ORDI0168
      ORDI0169
      ORDI0170
      ORDI0171
      ORDI0172
      ORDI0173
      ORDI0174
      ORDI0175
      ORDI0176
      ORDI0177
      ORDI0178
      ORDI0179
      ORDI0180

```

```

DO 780 JQ=1,4
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM*CK/R*AND
DAHV(JQ)=FSUM
780 CONTINUE
NN=NN+1
DO 781 JQ=1,4
CALL INTEG(FSUM,NN,JQ,IQ)
FSUM=FSUM*CK/P*AND
DAHIV(JQ)=FSUM
781 CONTINUE
IF (ICDEBUG.EQ.0) GO TO 851
WRITE(6,80) ((DAH(I,J),J=1,4),I=1,4)
80 FORMAT(2X,'DAH',4(T10.4(E15.7,2X)/1X))
WRITE(6,81) DAW0,DAV1,DAHII,DAHV,DAHIV
81 FORMAT(2X,'DAW0',T10.4(E15.7,2X)
*      /2X,'DAV1',T10.4(E15.7,2X)
*      /2X,'DAHII',T10.4(E15.7,2X)
*      /2X,'DAHV',T10.4(E15.7,2X)
*      /2X,'DAHIV',T10.4(E15.7,2X)      )
851 RETURN
END

```

```
SUBROUTINE INTEG(FSUM,NN,JQ,IQ)           INTE0001
C                                         INTE0002
C NUMERICAL INTEGRATION---GALSSIAN QUADRATURE INTE0003
C                                         INTE0004
C
COMMON /AREA2/NPT,XXX(20),A(20)           INTE0005
SUM=0.0                                     INTE0006
DO 40 JJJ=1,NPT                           INTEJ007
X=XXX(JJJ)                                 INTE0008
SUM=SUM+A(JJJ)*F(X,NN,JJJ,JQ,IQ)          INTE0009
40 CONTINUE                                 INTE0010
FSUM=0.5*SUM                               INTE0011
RETURN                                     INTEJ012
END                                         INTE0013
```

FUNCTION FIX,NN,JJJ,JQ,IC1
 C
 C TO DEFINE THE INTEGRAND FUNCTIONS
 C
 COMMON/AREA4/H(4,4,20),HI(4,20),HII(4,20),HRZ(4,20),HNR(4,20),
 %W0(4,20),V0(4,20),W1(4,20),V1(4,20)
 @ ,OH(4,4,20),OW0(4,20),OV1(4,20),OHIII(4,20),CHIII(4,20)
 @ ,OHV(4,20),OHIV(4,20)
 COMMON/AKKH/FTOP1(20),FT1P0(20),FT1P2(20),FT2P1(20), FZ2P0(20),
 /FZDP0(20),FZ1P1(20),FZ2P2(20)
 @ ,FT3P0(20),FT3P1(20),FZ3P0(20),FZ3P1(20)
 COMMON/ADFB/HIII(4,20),FIV(4,20),HV(4,20),HVII(4,20),HVIII(4,20)
 COMMON/WINGAR/TS0S(20,6,6),TSAS(20,6,6),TSAG(20,6,3)
 GC TO(1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,
 @21,22,23,24,25,26,27,28,29,30,31,32,33,34,35,36),NN
 1 F=H(JQ,IC,JJJ)
 RETURN
 2 F=HI(JQ,JJJ)
 RETURN
 3 F=HII(JQ,JJJ)
 RETURN
 4 F=HRZ(JQ,JJJ)
 RETURN
 5 F=HNR(JQ,JJJ)
 RETURN
 6 F= W0(JQ,JJJ)
 RETURN
 7 F= V0(JQ,JJJ)
 RETURN
 8 F= W1(JQ,JJJ)
 RETURN
 9 F= V1(JQ,JJJ)
 RETURN
 10 F=FTOP1(JJJ)
 RETURN
 11 F=FT1P0(JJJ)
 F 0001
 F 0002
 F 0003
 F 0004
 F 0005
 F 0006
 F 0007
 F 0008
 F 0009
 F 0010
 F 0011
 F 0012
 F 0013
 F 0014
 F 0015
 F 0016
 F 0017
 F 0018
 F 0019
 F 0020
 F 0021
 F 0022
 F 0023
 F 0024
 F 0025
 F 0026
 F 0027
 F 0028
 F 0029
 F 0030
 F 0031
 F 0032
 F 0033
 F 0034
 F 0035
 F 0036

12	RETURN	F	0037
	F=FT1P2(JJJ)	F	0038
13	RETURN	F	0039
	F=FT2P1(JJJ)	F	0040
14	RETURN	F	0041
	F=FZDP0(JJJ)	F	0042
15	RETURN	F	0043
	F=FZ1P1(JJJ)	F	0044
16	RETURN	F	0045
	F=FZ2P0(JJJ)	F	0046
17	RETURN	F	0047
	F=FZ2P2(JJJ)	F	0048
18	RETURN	F	0049
	F=HIII(JQ, JJJ)	F	0050
19	RETURN	F	0051
	F=HIV(JQ, JJJ)	F	0052
20	RETURN	F	0053
	F=HV(JQ, JJJ)	F	0054
21	RETURN	F	0055
	F=HVI(JQ, JJJ)	F	0056
22	RETURN	F	0057
	F=HVII(JQ, JJJ)	F	0058
23	RETURN	F	0059
	F=TS0S(JJJ, JQ, IQ)	F	0060
24	RETURN	F	0061
	F=TSAS(JJJ, JQ, IQ)	F	0062
25	RETURN	F	0063
	F=TSAG(JJJ, JQ, IQ)	F	0064
26	RETURN	F	0065
	F=CHIII(JQ, JJJ)	F	0066
27	RETURN	F	0067
	F=FT3P0(JJJ)	F	0068
28	RETURN	F	0069
	F=FT3P1(JJJ)	F	0070
29	RETURN	F	0071
	F=FZ3P0(JJJ)	F	0072

	RETURN	F 0073
30	F=FZ3P1(JJJ)	F 0074
	RETURN	F 0075
31	F=OH(JQ,IG,JKJ)	F 0076
	RETURN	F 0077
32	F=OWD(JQ,JKJ)	F 0078
	RETURN	F 0079
33	F=OV1(JQ,JKJ)	F 0080
	RETURN	F 0081
34	F=OHIII(JQ,JKJ)	F 0082
	RETURN	F 0083
35	F=OHV(JQ,JKJ)	F 0084
	RETURN	F 0085
36	F=OHIV(JQ,JKJ)	F 0086
	RETURN	F 0087
	END	F 0088

SUBROUTINE AINER

C

TO DEFINE THE EQUATION'S COEFFICIENTS IN MATRIX FORM RELATING TO
INERTIA TERMS

C

```

COMMON /PARMT/  ITYPE ,IFLT
COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /AREA6/NOBLD,ROH,CHOD,AIB,CK,HMAST ,ALOCK ,ANO,HR
COMMON/AREA5/AH(4,4),AH(4),AHII(4),AHRZ(4),AHNR(4),AW0(4),AV0(4)
a,AW1(4),AV1(4),OAH(4,4),OAW0(4),OAV1(4),OAHIII(4),CAHIII(4)
a,OAHV(4),OAHIV(4)
COMMON/INERTI/TTMT(4,6,3),TTCTJ(4,6,3),AMJT(4,3,6),CJT(4,3,6)
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
DIMENSION AMT(4,5,3),CJ(4,3,5),AM(4,3,5),TCJ(4,5,3)
DO 50 I=1,4
DO 50 J=1,5
DO 50 K=1,3
AMT(I,J,K)=0.0
50 CJ(I,K,J)=0.0
DO 210 NM=1,4
AMT(NM,1,3)=-AV0(NM)/R
AMT(NM,2,1)=AW0(NM)/R
AMT(NM,3,2)=-AVC(NM)*HR
AMT(NM,3,3)=AW1(NM)
AMT(NM,4,2)=-AW1(NM)
AMT(NM,4,3)=-AV0(NM)*HR
AMT(NM,5,1)=AV1(NM)
IF(ITYPE.EQ.0) GO TO 300
AMT(NM,2,1)=OAW0(NM)/R
AMT(NM,5,1)=OAV1(NM)
300 CONTINUE
DO 2 I=1,6
DO 2 J=1,3
DO 2 K=1,5
2 TTMT(NM,I,J)=TT(I,K)*AMT(NM,K,J)+TTMT(NM,I,J)
DO 3 I=1,6

```

128

50

300

2

AINE001
AINE002
AINE003
AINE004
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AINE014
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AINE016
AINE017
AINE018
AINE019
AINE020
AINE021
AINE022
AINE023
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AINE026
AINE027
AINE028
AINE029
AINE030
AINE031
AINE032
AINE033
AINE034
AINE035
AINE036

	DO 3 J=2,3	AINE0037
3	TTMT(NM,I,J)=0.5*TTMT(NM,I,J)	AINE0038
	CJ(NM,2,3)=2.0*AW1(NM)	AINE0039
	CJ(NM,3,4)=2.0*AW1(NM)	AINE0040
	DO 5 I=1,5	AINE0041
	DO 5 J=1,3	AINE0042
5	TCJ(NM,I,J)=CJ(NM,J,I)	AINE0043
	CC 6 I=1,6	AINE0044
	DO 6 J=1,3	AINE0045
	DC 6 K=1,5	AINE0046
6	TTCTJ(NM,I,J)=TT(I,K)*TCJ(NM,K,J)+TTCTJ(NM,I,J)	AINE0047
	DO 100 I=1,6	AINE0048
	DC 100 J=2,3	AINE0049
100	TTCTJ(NM,I,J)=0.5*TTCTJ(NM,I,J)	AINE0050
	DC 7 I=1,5	AINE0051
	CC 7 J=1,6	AINE0052
7	T(I,J)=T(J,I)	AINE0053
	DO 8 I=1,3	AINE0054
	DC 8 J=1,5	AINE0055
8	AM(NM,I,J)=AMT(NM,J,I)	AINE0056
	DO 9 I=1,3	AINE0057
	DC 9 J=1,6	AINE0058
	DC 9 K=1,5	AINE0059
9	AMJT(NM,I,J)=AM(NM,I,K)*T(K,J)+AMJT(NM,I,J)	AINE0060
	DO 10 I=1,3	AINE0061
	DO 10 J=1,6	AINE0062
	DC 10 K=1,5	AINE0063
10	CJT(NM,I,J)=CJ(NM,I,K)*T(K,J)+CJT(NM,I,J)	AINE0064
210	CONTINUE	AINE0065
	RETURN	AINE0066
	END	AINE0067

SUBROUTINE AEROMT
 C
 C TO DEFINE THE EQUATION'S COEFFICIENTS IN MATRIX FORM RELATING TO
 C AERODYNAMIC TERMS
 C

```

  COMMON /PARMT/  ITYPE ,IFLT
  COMMON /AREA6/NOBLD,RCH,CHOD,AIB,CK,HMAST ,ALOCK ,ANO,HR
  COMMON/AREA5/AH(4,4),AH1(4),AH11(4),AHRZ(4),AHNR(4),AW0(4),AV0(4)
  @,AW1(4),AV1(4),OAH(4,4),CAWD(4),DAV1(4),OAHIII(4),CAHIII(4)
  @,CAHV(4),OAHIV(4)
  COMMON /AREA1/OMEGA,R,VEL,CL,CD,RAMDA,SNOMEA
  COMMON/AERO/AFT0P1,AFT1P0,AFT1P2,AFT2P1,AFZ0P0,AFZ1P1,AFZ2P0,
  @AFZ2P2,AHIII(4),AHIV(4),AHV(4),AHVI(4),AHVII(4)
  @,AFT3P0,AFT3P1,AFZ3P0,AFZ3P1
  COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
  COMMON /ARR/WGUST(6,6),CAMX(6,6),DQ(4,6,3),Q(4,6,3)
  @ ,DHMAX(4,3,6),HMAX(4,3,6)
  COMMON /COUPL/  AKPC(4),AKPD(4)
  DIMENSION          CDHMX(4,3,5),CHMX(4,3,5)
  DIMENSION GUST(5,6),CCANX(5,5),CCDAMX(6,5),CAMX(5,5),CCAMX(6,5)
  @,CDQ(4,5,3),CQ(4,5,3)
  DC 100 I=1,4
  DC 100 J=1,3
  DC 100 K=1,5
  CDHMX(I,J,K)=0.0
  CHMX(I,J,K)=0.0
  CDQ(I,K,J)=0.0
  100  CQ(I,K,J)=0.0
  DO 101 I=1,5
  DO 102 J=1,5
  CAMX(I,J)=0.0
  102  CCAMX(I,J)=0.0
  DC 103 K=1,6
  GUST(I,K)=0.0
  CCDAMX(K,I)=0.0
  103  CCAMX(K,I)=0.0
  
```

```

101  CONTINUE
      DO 1 I=1,2
      DO 1 J=1,6
1      T(I,J)=T(I,J)/R
      DO 2 I=1,6
      DO 2 J=1,2
2      TT(I,J)=TT(I,J)/R
      GUST(1,1)=0.5*AFT1P0
      GUST(2,3)=AFZ2P0
      GUST(3,1)=-0.5*AFZ1P1
      GUST(3,2)=-HR*AFT1P0 *0.5
      GUST(4,1)=0.5*HR*AFT1P0
      GUST(4,2)=-AFZ1P1 *0.5
      GUST(5,3)=AFT2P1
      GUST(1,6)=0.5*AFT3P0
      GUST(2,4)=AFZ3P0
      GUST(3,5)=-0.5*HR*AFT3P0
      GUST(3,6)=0.5*AFZ3P1
      GUST(4,5)=-0.5*AFZ3P1
      GUST(4,6)=-0.5*HR*AFT3P0
      GUST(5,4)=AFT3P1
      DO 5 I=1,6
      DO 5 J=1,6
      DO 5 K=1,5
5      WGUST(I,J)=TT(I,K)*GUST(K,J)+WGUST(I,J)
      DO 6 I=1,6
      DO 6 J=1,3
6      WGUST(I,J)=WGUST(I,J)*ABS(RAMDA)
      CDAMX(1,1)=0.5*AFT1P0
      CDAMX(1,3)=-0.5*AFZ2P1
      CDAMX(1,4)=0.5*HR*AFT1P0
      CDAMX(2,2)=AFZ2P0
      CDAMX(2,5)=AFZ1P1
      CDAMX(3,1)=-0.5*AFZ1P1
      CDAMX(3,3)=0.5*(HR**2*AFT1P0+AFZ2P2)
      CDAMX(3,4)=0.5*HR*(AFT2P1-AFZ1P1)

```

```

CDAMX(4,1)=0.5*HR*AFT1P0          AER00073
CDAMX(4,3)=HR*(-AFT2P1+AFZ1P1)    *0.5  AER00074
CDAMX(4,4)=0.5*(HR**2*AFT1P0+AFZ2P2) AER00075
CDAMX(5,2)=AFT2P1                AER00076
CDAMX(5,5)=AFT1P2                AER00077
      DO 9 I=1,6                  AER00078
      DO 9 J=1,5                  AER00079
      DO 9 K=1,5                  AER00080
9   CCDAMX(I,J)=TT(I,K)*CDAMX(K,J)+CCDAMX(I,J) AER00081
      DO 11 I=1,6                AER00082
      DO 11 J=1,6                AER00083
      DO 11 K=1,5                AER00084
11  DAMX(I,J)=CCDAMX(I,K)*T(K,J)+DAMX(I,J) AER00085
      AMDA=ABS(RAMDA)            AER00086
      CAMX(1,4)=-0.5* AMDA*AFT1P0+AFZ0P0 AER00087
      CAMX(3,3)=HR*(AFZ0P0-0.5* AMDA*AFT1P0) AER00088
      CAMX(3,4)=0.5* AMDA*AFZ1P1+AFT0P1 AER00089
      CAMX(4,3)=-0.5* AMDA*AFZ1P1 AER00090
      CAMX(4,4)=HR*(-0.5* AMDA*AFT1P0+AFZ0P0) AER00091
      DO 12 I=1,6                AER00092
      DO 12 J=1,5                AER00093
      DO 12 K=1,5                AER00094
12  CCAMX(I,J)=TT(I,K)*CAMX(K,J)+CCAMX(I,J) AER00095
      DO 13 I=1,6                AER00096
      DO 13 J=1,6                AER00097
      DO 13 K=1,5                AER00098
13  AMX(I,J)=CCAMX(I,K)*T(K,J)+AMX(I,J) AER00099
      DO 40 NM=1,4                AER00100
      CDO(NM,1,3)=-0.5*AHIII(NM) AER00101
      CDO(NM,2,1)=AHV(NM)        AER00102
      CDO(NM,3,2)=-0.5*HR*AHIII(NM) AER00103
      CDO(NM,3,3)=0.5*AHVI(NM)   AER00104
      CDO(NM,4,2)=-0.5*AHVI(NM)  AER00105
      CDO(NM,4,3)=-0.5*HR*AHIII(NM) AER00106
      CDO(NM,5,1)=AHIV(NM)       AER00107
      CQ(NM,1,2)=0.5*AHIII(NM) *SRCMEG AER00108

```

CQ(NM,3,2)=0.5*(AHVII(NM)-AHVI(NM)*SNOMEGL
 CQ(NM,3,3)=-0.5*HR*AHIII(NM)*SNOMEGL
 CQ(NM,4,2)=0.5*HR*AHIII(NM) *SNOMEGL
 CQ(NM,4,3)=0.5*(AHVIT(NM)- AHVI(NM) *SNOMEGL)
 IF (ITYPE.EQ.0) GO TO 110
 CDQ(NM,2,1)=DAHV(NM)
 CDQ(NM,5,1)=DAHIV(NM)
 CQ(NM,1,3)=0.5*AKPC(NM)*AFT3P0
 CQ(NM,2,1)=AKPD(NM)*AFZ3P0
 CQ(NM,3,2)=CQ(NM,3,2)-0.5*HR*AKPC(NM)*AFT3P0
 CQ(NM,3,3)=CQ(NM,3,3)+0.5*AKPC(NM)*AFZ3P1
 CQ(NM,4,2)=CQ(NM,4,2)-0.5*AKPC(NM)*AFZ3P1
 CQ(NM,4,3)=CQ(NM,4,3)-0.5*HR*AKPC(NM)*AFT3P0
 CQ(NM,5,1)=AKPD(NM)*AFT3P1
 110 CONTINUE
 DO 16 I=1,6
 DO 16 J=1,3
 DO 16 K=1,5
 Q(NM,I,J)=TT(I,K)*CQ(NM,K,J)+Q(NM,I,J)
 16 DQ(NM,I,J)=TT(I,K)*CDQ(NM,K,J)+DQ(NM,I,J)
 C AERO FOR BLADES DUE TO WING MOTION
 CDHMX(NM,1,2)=AHRZ(NM)
 CDHMX(NM,1,5)=AHNR(NM)
 CDHMX(NM,2,3)=-HR*AHII(NM)
 CDHMX(NM,2,4)=-AHII(NM)
 CDHMX(NM,3,1)=-AHII(NM)
 CDHMX(NM,3,3)=AHII(NM)
 CDHMX(NM,3,4)=-HR*AHII(NM)
 CHMX(NM,2,3)= AMDA*AHII(NM)
 CHMX(NM,3,4)= AMDA*AHII(NM)
 DO 20 I=1,3
 DO 20 J=1,6
 DO 20 K=1,5
 DHMAX(NM,I,J)=CDHMX(NM,I,K)*T(K,J)+DHMAX(NM,I,J)
 20 HMAX(NM,I,J)=CHMX(NM,I,K)*T(K,J)+HMAX(NM,I,J)
 40 CONTINUE

AERO0109
 AERO0110
 AERO0111
 AERO0112
 AERO0113
 AERO0114
 AERO0115
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 AERO0118
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 AERO0120
 AERO0121
 AERO0122
 AERO0123
 AERO0124
 AERO0125
 AERO0126
 AERO0127
 AERO0128
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 AERO0132
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 AERO0134
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 AERO0136
 AERO0137
 AERO0138
 AERO0139
 AERO0140
 AERO0141
 AERO0142
 AERO0143
 AERO0144

RE TURN
END

AERO145
AERO146

SUBROUTINE EQMTX(1DOF)

EQMTJ001

EQMT0002

EQMTU003

EQMTU004

EQMTJ005

EQMTUJ06

EQMTU007

EQMTU008

EQMTJ009

EQMT0010

EQMTU011

EQMTJ012

EQMTU013

EQMTU014

EQMT0015

EQMTU016

EQMTU017

EQMT0018

EQMTJ019

EQMTU020

EQMTU021

EQMTJ022

EQMTU023

EQMTU024

EQMTU025

EQMT0026

EQMTUJ27

EQMTU028

EQMTU029

EQMTU030

EQMT0031

EQMT0032

EQMTU033

EQMTU034

EQMTUJ35

EQMTJ036

C TO DEFINE THE COEFFICIENT MATRICES A,B,C AND D IN EQ. 2.3

COMMON /PARMT/ ITYPE ,IFLT
COMMON/AREA8/BLAM(4),WLAM(6),BRAM(4),WRAM(6),BLAM0(4),BRAM0(4)
COMMON /AREA1/DMEGA,R,VEL,CL,CD,RAMDA,SNOMEG
COMMON /APEA6/NOBLD,PCD,CHOD,AIB,CK,FMAST ,ALOCK ,ANO,HR
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
COMMON/AREA5/AH(4,4),AHI(4),AHII(4),AHRZ(4),AHNR(4),AWD(4),AVD(4)
a,AWI(4),AVI(4),CAH(4,4),DAWD(4),DAV1(4),DAHII(4),CAHII(4)
a,CAHV(4),DAHV(4)
COMMON/INERTI/TTMT(4,6,3),TTCTJ(4,6,3),AMJT(4,3,6),CJT(4,3,6)
COMMON /ARR/WGUST(6,6),AMX(6,6),AMX(6,6),DQ(4,6,3),Q(4,6,3)
a ,DHMAX(4,3,6),FMAX(4,3,6)
COMMON/ARWNG/DARWA(6,6),ARWA(6,6),ARWG(6,3)
COMMON/DOF18/AY(19,19),BY(19,19),CY(19,19),DY(19,6)
COMMON /COUPL/ AKPC(4),AKPD(4)
WRITE(6,450)
450 FORMAT(//1X,75(1H-)//15X,44HEQUATIONS OF MOTION ; A*X" + B*X' + C
E*X=D*E ,//1X,75(1H-)////)
DO 801 I=1,18
801 AAY(I,I)=1.0
DC 802 NM=1,4
DO 802 I=1,3
DC 802 J=1,6
AAY(3*(NM-1)+I,J+12)=AMJT(NM,I,J)
802 AAY(J+12,3*(NM-1)+I)=ANC*TTMT(NM,J,I)
DC 804 I=1,4
BY(3*I-1,3*I)=2.0*SNCMEG
804 BY(3*I,3*I-1)=-2.0*SNCMEG
DC 805 J=1,4
DC 805 I=1,4
DO 805 K=1,3
805 BY(3*(J-1)+K,3*(I-1)+K)=AH(J,I)
DC 806 NM=1,4

135

96
 806 DO 806 I=1,3 EQMT0037
 DO 806 J=1,6 EQMTJ038
 BBY(3*(NM-1)+I,J+12)=DHMAX(NM,I,J)+CJT(NM,I,J)*SNOMEG EQMT0039
 806 BBY(J+12,3*(NM-1)+I)=DC(NM,J,I)-AND*TTCTJ(NM,J,I)*SNOMEG EQMT0040
 DO 808 I=1,6 EQMT0041
 DO 808 J=1,6 EQMT0042
 808 BBY(I+12,J+12)=DAMX(I,J)+C(I,J)*SNOMEG-DARWA(I,J) EQMT0043
 DC 809 I=1,4 EQMT0044
 CCY(3*(I-1)+1,3*(I-1)+1)=BLAM(I) EQMT0045
 CCY(3*(I-1)+2,3*(I-1)+2)=BLAM(I)-1.0 EQMT0046
 809 CCY(3*I,3*I)=BLAM(I)-1.0 EQMT0047
 DO 810 J=1,4 EQMT0048
 DO 810 I=1,4 EQMT0049
 CCY(3*j-1,3*I)=AH(J,I)*SNOMEG EQMT0050
 810 CCY(3*j,3*I-1)=-AH(J,I)*SNOMEG EQMTJ051
 DC 811 NM=1,4 EQMT0052
 DO 811 I=1,3 EQMT0053
 DO 811 J=1,6 EQMT0054
 CCY(3*(NM-1)+I,J+12)=HMAX(NM,I,J) EQMT0055
 811 CCY(J+12,3*(NM-1)+I)= Q(NM,J,I) EQMT0056
 DO 812 I=1,6 EQMT0057
 DO 812 J=1,6 EQMT0058
 812 CCY(I+12,J+12)=AMX(I,J) -ARWA(I,J) EQMT0059
 DC 813 I=1,6 EQMTJ060
 813 CCY(I+12,I+12)=CCY(I+12,I+12)+WLAM(I) EQMT0061
 DC 814 NM=1,4 EQMTJ062
 DDY(3*(NM-1)+1,4)=-CAHIII(NM) EQMT0063
 DDY(3*(NM-1)+2,5)=-CAHIII(NM) EQMTJ064
 CCY(3*(NM-1)+3,6)=-CAHIII(NM) EQMT0065
 DDY(3*NM-1,2)=AHI(NM) *ABS(RAMCA) *(-1.0) EQMT0066
 DDY(3*NM-2,3)=AHRZ(NM)*ABS(RAMDA) *(-1.0) EQMT0067
 814 CCY(3*NM,1)=-AHI(NM) *ABS(RAMDA) *(-1.0) EQMT0068
 DC 815 I=1,6 EQMT0069
 DO 816 J=1,3 EQMT0070
 816 CCY(I+12,J)=WGUST(I,J) +ARWG(I,J) EQMT0071
 DC 817 J=4,6 EQMT0072

817 DEY(I+12,J)=-WGUST(I,J) EQMT0073
 815 CCNTINUE EQMT0074
 IF(I TYPE, EQ, 0) GO TO 300 EQMT0075
 DO 500 J=1,4 EQMT0076
 DO 500 I=1,4 EQMT0077
 500 BBY(3*(J-1)+1,3*(I-1)+1)=DAH(J,I) EQMT0078
 DO 550 I=1,4 EQMT0079
 CCY(3*(I-1)+1,3*(I-1)+1)=BLAM0(I) EQMT0080
 CCY(3*(I-1)+2,3*(I-1)+2)=BLAM(I)-1.0 EQMT0081
 550 CCY(3*I,3*I)=BLAM(I)-1.0 EQMT0082
 DO 502 J=1,4 EQMT0083
 DO 502 I=1,4 EQMT0084
 CCY(3*j-2,3*I-2)=CCY(3*j-2,3*I-2)+AKPD(I)*DAHII(J) EQMT0085
 CCY(3*j-1,3*I-1)=CCY(3*j-1,3*I-1)+AKPC(I)*CAHII(J) EQMT0086
 5j2 CCY(3*j ,3*I)=CCY(3*j ,3*I)+AKPC(I)*CAHII(J) EQMT0087
 DO 501 NM=1,4 EQMT0088
 501 CDY(3*(NM-1)+1,4)=-DAHII(NM) EQMT0089
 300 CCNTINUE EQMT0090
 IF(I DOF, EQ, 9) GO TO 100 EQMT0091
 IF(IFLT, NE, 0) GO TO 205 EQMT0092
 WRITE(6,451) EQMT0093
 WRITE(6,6) ((AAY(I,J),J=1,9),I=1,18) EQMT0094
 WRITE(6,6) ((AAY(I,J),J=10,18),I=1,18) EQMT0095
 WRITE(6,5) EQMT0096
 WRITE(6,452) EQMT0097
 WRITE(6,6) ((BBY(I,J),J=1,9),I=1,18) EQMT0098
 WRITE(6,6) ((BBY(I,J),J=10,18),I=1,18) EQMT0099
 WRITE(6,5) EQMT0100
 WRITE(6,453) EQMT0101
 WRITE(6,6) ((CCY(I,J),J=1,9),I=1,18) EQMT0102
 WRITE(6,6) ((CCY(I,J),J=10,18),I=1,18) EQMT0103
 WRITE(6,5) EQMT0104
 WRITE(6,454) EQMT0105
 WRITE(6,7) ((CDY(I,J),J=1,6),I=1,18) EQMT0106
 5 FORMAT(1H1) EQMT0107
 6 FORMAT(//1X,18{/1X,9(E12.5,1X)}) EQMT0108

```

7   FORMAT(//1X,18(/1X,6(E12.5,1X)))
451  FORMAT(2CX,'A MATRIX=')
452    FORMAT(//20X,'B MATRIX=')
453    FORMAT(//20X,'C MATRIX=')
454    FORMAT(//20X,'D MATRIX=')
      RETURN
100  CCNTINUE
      DO 201 I=1,6
      DC 201 J=7,9
      AAY(I,J)=AAY(I,J+6)
      BBY(I,J)=BBY(I,J+6)
      CCY(I,J)=CCY(I,J+6)
      AAY(J,I)=AAY(J+6,I)
      BBY(J,I)=BBY(J+6,I)
201  CCY(J,I)=CCY(J+6,I)
      DO 202 I=7,9
      DO 202 J=7,9
      AAY(I,J)=AAY(I+6,J+6)
      BBY(I,J)=BBY(I+6,J+6)
      CCY(I,J)=CCY(I+6,J+6)
202  DO 204 I=7,9
      DC 204 J=1,6
      DCY(I,J)=DCY(I+6,J)
      IF(IFLT.NE.0) GO TO 205
      WRITE(6,451)
      WRITE(6,850)((AAY(I,J),J=1,9),I=1,9)
      WRITE(6,452)
      WRITE(6,850)((BBY(I,J),J=1,9),I=1,9)
      WRITE(6,453)
      WRITE(6,850)((CCY(I,J),J=1,9),I=1,9)
      WRITE(6,454)
      WRITE(6,850)((DDY(I,J),J=1,6),I=1,9)
      FORMAT(//1X,9(/1X,9(E12.5,1X)))
      FORMAT(//1X,9(/1X,6(E12.5,1X)))
      CCNTINUE
      RETURN
      EQMT0109
      EQMT0110
      EQMT0111
      EQMT0112
      EQMT0113
      EQMT0114
      EQMT0115
      EQMT0116
      EQMT0117
      EQMT0118
      EQMT0119
      EQMT0120
      EQMT0121
      EQMT0122
      EQMT0123
      EQMT0124
      EQMT0125
      EQMT0126
      EQMT0127
      EQMT0128
      EQMT0129
      EQMT0130
      EQMT0131
      ECMT0132
      FQMT0133
      EQMT0134
      EQMT0135
      EQMT0136
      EQMT0137
      EQMT0138
      EQMT0139
      EQMT0140
      EQMT0141
      EQMT0142
      EQMT0143
      EQMT0144

```

END

EQMTO145

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SUBROUTINE AUTO(1DOF)

```

C
C      IN AUTOROTATION FLIGHT ANOTHER DEGREE OF FREEDOM IS ADDED
C
COMMON /PARMT/  ITYPE ,IFLT
COMMON/AMATIC/TT(6,5),C(6,6) ,T(5,6)
COMMON /AREA6/NOBLD,ROH,CHOD,AIB,CK,HMAST ,ALOCK ,ANG,HR
COMMON/AREA5/AH(4,4),AH1(4),AHII(4),AHRZ(4),AHNR(4),AW0(4),AV0(4)
@,AW1(4),AV1(+),OAH(4,4),CAWC(4),CAV1(4),CAHIII(4),CAHIII(4)
@ ,CAHV(4),OAHIV(4)
COMMON/DOF18/AAY(19,19),BBY(19,19),CCY(19,19),DDY(19,6)
COMMON /COUPL/  AKPC(4),AKPD(4)
COMMON/AERO/AFTOP1,AFT1P0,AFT1P2,AFT2P1,AFZOP0,AFZ1P1,AFZ2P0,
@AFZ2P2,AHIII(4),AHIV(4),AHV(4),AHVI(4),AHVII(4)
@ ,AFT3P0,AFT3P1,AFZ3P0,AFZ3P1
NB=4
Nh=6
NR=19
DO 11 I=1,NB
AAY(3*I-2, NR)=AV1(I)
AAY(NR, 3*I-2)=AV1(I)*ANG
BBY(3*I-2, NR)=AHNR(I)
BBY(NR, 3*I-2)=AHIV(I)
11  CONTINUE
DO 12 I=1,Nh
BBY(NR, 3*NB+I)=AFT2P1*T(2,I)
BBY(3*NR+I, NR)=AFZ1P1*T(2,I)
12  CONTINUE
AAY(NR, NR)=AIB*ANG
BBY(NR, NR)=AFT1P2
CCY(NR, 3)=-AFT2P1
DDY(NR, 4)=-AFT3P1
IF(ITYPE.EQ.0) GO TO 13
DO 14 I=1,NB
AAY(3*I-2, NR)=OAV1(I)
AAY(NR, 3*I-2)=OAV1(I)*ANG

```

AUTOJ001
AUT00002
AUT00003
AUT00014
AUT00005
AUT00006
AUT00007
AUT00008
AUT00009
AUT00010
AUT00011
AUT00012
AUT00013
AUT00014
AUT00015
AUT00016
AUT00017
AUT00018
AUT00019
AUT00020
AUT00021
AUT00022
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AUT00029
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AUT00033
AUT00034
AUT00035
AUT00036

```

      BBY(NR,3*I-2)=DAHIV(I)
      CCY(NR,3*I-2)=AKPO(I)*AFT3P1
14    CONTINUE
13    CONTINUE
      IF(IDOF.EC.9) GO TO 100
      WRITE(6,451)
      WRITE(6,6)(( AAY(I,J),J=1,9),I=1,19)
      WRITE(6,8)(( AAY(I,J),J=10,19),I=1,19)
      WRITE(6,5)
      WRITE(6,452)
      WRITE(6,6)(( BBY(I,J),J=1,9),I=1,19)
      WRITE(6,8)(( BBY(I,J),J=10,19),I=1,19)
      WRITE(6,5)
      WRITE(6,453)
      WRITE(6,6)(( CCY(I,J),J=1,9),I=1,19)
      WRITE(6,8)(( CCY(I,J),J=10,19),I=1,19)
      WRITE(6,5)
      WRITE(6,454)
      WRITE(6,7)(( DDY(I,J),J=1,6),I=1,19)
5     FFORMAT(1H1)
6     FFORMAT(//1X,19(/1X,9(E12.5,1X)))
7     FFORMAT(//1X,19(/1X,6(E12.5,1X)))
8     FFORMAT(//1X,19(/1X,10(E12.5,1X)))
      RETURN
100   CONTINUE
      DC 15 I=1,6
      AAY(1,10)=AAY(1,19)
      BBY(1,10)=BBY(1,19)
      CCY(1,10)=CCY(1,19)
      AAY(10,1)=AAY(19,1)
      BBY(10,1)=BBY(19,1)
      CCY(10,1)=CCY(19,1)
      CCY(10,1)=DDY(19,1)
15    CONTINUE
      DO 16 I=1,3
      AAY(I+6,10)=AAY(I+12,19)

```

	BBY(I+6,10)=BBY(I+12,19)	AUT00073
	CCY(I+6,10)=CCY(I+12,19)	AUT00074
	AAY(10,I+6)=AAY(19,I+12)	AUT00075
	BBY(10,I+6)=BBY(19,I+12)	AUT00076
	CCY(10,I+6)=CCY(19,I+12)	AUT00077
16	CONTINUE	AUT00078
	AAY(10,10)=AAY(19,19)	AUT00079
	BBY(10,10)=BBY(19,19)	AUT00080
	CCY(10,10)=CCY(19,19)	AUT00081
	WRITE(6,451)	AUT00082
	WRITE(6,850)((AAY(I,J),J=1,10),I=1,10)	AUT00083
	WRITE(6,452)	AUT00084
	WRITE(6,850)((BBY(I,J),J=1,10),I=1,10)	AUT00085
	WRITE(6,453)	AUT00086
	WRITE(6,850)((CCY(I,J),J=1,10),I=1,10)	AUT00087
	WRITE(6,454)	AUT00088
	WRITE(6,950)((DDY(I,J),J=1,6),I=1,10)	AUT00089
451	FORMAT(20X,'A MATRIX=')	AUT00090
452	FORMAT(//20X,'B MATRIX=')	AUT00091
453	FORMAT(//20X,'C MATRIX=')	AUT00092
454	FORMAT(//20X,'D MATRIX=')	AUT00093
850	FORMAT(//1X,10(/1X,10(E12.5,1X)))	AUT00094
950	FORMAT(//1X,10(/1X,6(E12.5,1X)))	AUT00095
	RETURN	AUT00096
	END	AUT00097

```
      SUBROUTINE GUSTCC(GUST,L,DDY,DDZ)
C
C      TO DEFINE GUST AND BLADE PITCH CONTROL COMPONENTS
C
      DIMENSION CCUST(6),ECDY(19,6),DDZ(19)
      DO 1 I=1,L
      DDZ(I)=0.0
      DO 2 I=1,L
      DO 2 J=1,6
      2 DDZ(I)=ECDY(I,J)*GUST(J)+DDZ(I)
      RETURN
      END
```

GUST001
GUST002
GUST003
GUST004
GUST005
GUST006
GUST007
GUST008
GUST009
GUST010
GUST011
GUST012

```

SUBROUTINE FRQRES(L,AAA,BBB,CCC,DDD,IFLT,ICDF)
C
C      T) CALCULATE THE FREQUENCY RESPONSE
C
      DIMENSION AAA(19,19),BBB(19,19),CCC(19,19),DDD(19)
      DOUBLE PRECISION  FREQ,DPA(19,19),DPR(19,19),DPC(19,19),DPD(19)
      COMPLEX*16 CCMA(19,19),CCNE(19),  DCMPLX
      WRITE(6,1001)
1000  FORMAT(//10X,4G(1E-),//20X,'FREQUENCY RESPONSE',//10X,4G(1E-)
      *      //10X,'--FREQUENCY/OMEGA--')
      IF(1DLF.EQ.1B) GE TC 1001
      WRITE(6,1002)
1002  FORMAT(//10X,'Q1C',T22,'Q1C',T34,'Q1S',T46,'Q2C',T58,'Q2C',T70,
      *      'Q2S',T82,'WING 1', T94,'WING 2',T106,'WING 3')
      GE T) 1003
1003  WRITE(6,1004)
1004  FORMAT(//10X,'Q1C',T22,'Q1C',T34,'Q1S',T46,'Q2C',T58,'Q2C',T70,
      *      'Q2S',T82,'Q3C',T94,'Q3C', T106,'Q3S' //10X,'Q4C',T22,
      *      'Q4C',T34,'Q4S',T46,'WING 1',T58,'WING 2', T70,'WING 3',
      *      T82,'WING 4', T94,'WING 5',T106,'WING 6')
      1005  CONTINUE
      IF(IFLT.EQ.0) GE TC 1007
      WRITE(6,1005)
1005  FORMAT(//10X,'C(MU R)/DT')
1007  CONTINUE
      DO 180 I=1,L
      DO 180 J=1,L
      DPA(I,J)=AAA(I,J)
      DPE(I,J)=BBB(I,J)
      DPC(I,J)=CCC(I,J)
180   CONTINUE
      DO 181 I=1,L
      DPD(I) = DCC(I)
181   CONTINUE
      IK=L
      F=EC=L*CDJ

```

FRQR0001
FRQR0002
FRQR0003
FRQR0004
FRQR0005
FRQR0006
FRQR0007
FRQR0008
FRQR0009
FRQR0010
FRQR0011
FRQR0012
FRQR0013
FRQR0014
FRQR0015
FRQR0016
FRQR0017
FRQR0018
FRQR0019
FRQR0020
FRQR0021
FRQR0022
FRQR0023
FRQR0024
FRQR0025
FRQR0026
FRQR0027
FRQR0028
FRQR0029
FRQR0030
FRQR0031
FRQR0032
FRQR0033
FRQR0034
FRQR0035
FRQR0036

1 THE ORIGINAL PAGE IS FLOOR.

211 FREQ=FREQ+L.0100 FRQR0037
IK=IK+1 FRQR0038
GO TO 511 FRQR0039
311 FREQ=FREQ+L.0200 FRQR0040
IK=IK+1 FRQR0041
GO TO 511 FRQR0042
611 FREQ=FREQ+L.0500 FRQR0043
IK=IK+1 FRQR0044
GO TO 511 FRQR0045
711 FREQ=FREQ+L.100 FRQR0046
IK=IK+1 FRQR0047
GO TO 511 FRQR0048
811 FREQ=FREQ+L.500 FRQR0049
IK=IK+1 FRQR0050
GO TO 511 FRQR0051
511 DO 100 I=1,L FRQR0052
DO 100 J=1,L FRQR0053
100 CCMA(I,J)=DCMPLX(DPC(I,J)-FREQ*+2* DPA(I,J),FREQ*DPA(I,J)) FRQR0054
DO 301 I=1,L FRQR0055
301 CCMD(I)=DCMPLX(DPC(I),L.CCC) FRQR0056
CALL GAEI I(CCMA,CCMD,L ,FREQ,IDDF,IFLT) FRQR0057
IF(IK.LT.10) GO TO 211 FRQR0058
IF(IK.LT.25) GO TO 311 FRQR0059
IF(IK.LT.37) GO TO 611 FRQR0060
IF(IK.LT.57) GO TO 711 FRQR0061
IF(IK.LT.71) GO TO 811 FRQR0062
PICTURE FRQR0063
END FRQR0064

SUBROUTINE GAEL1(A,Y,N,FREQ,ICDF,IFLT)

C THE GAUSS-JORDAN REDUCTION

COMPLEX*16 A(19,19),Y(19),X(19)
DOUBLE PRECISION FREQ,CCABS
DIMENSION ABX(19)
COMMON/FPMAG/...,FRB(4),FRBC(4),FRW(6),IFRMAG
N=N-1
DO 10 I=1,M
L=I+1
DO 10 J=L,N
IF((CCABS(A(I,J)).EQ.0.0D0)) GO TO 10
DO 8 K=L,N
A(J,K)=A(J,K)-A(I,K)+A(J,I)/A(I,I)
CONTINUE
Y(J)=Y(J)-Y(I)*A(J,I)/A(I,I)
10 CONTINUE
X(N)=Y(N)/A(N,N)
DO 20 I=1,N
K=N-I
L=K+1
DO 20 J=L,N
Y(K)=Y(K)-X(J)*A(K,J)
30 X(K)=Y(K)/A(K,K)
DO 40 I=1,N
ABX(I)=CCABS(X(I))
IF((IFRMAG.EQ.1)) GO TO 50
IF((IDCF.EQ.9)) GO TO 51
LT=4
LT=6
GO TO 54
51 LT=2
LT=3
54 DO 52 I=1,LT
DO 52 J=1,3

GAEL001
GAEL002
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GAEL029
GAEL030
GAEL031
GAEL032
GAEL033
GAEL034
GAEL035
GAEL036

52	ABX(3*(I-1)+J)=ABX(3*(I-1)+J)*FRB(I)	GAELO037
	DC 55 I=1,LT	GAELO038
55	ABX(3*(I-1)+1)=ABX(3*(I-1)+1)*FRBO(I)/FRB(I)	GAELO039
	DO 53 I=1,LT	GAELO040
53	ABX(I+3*LT)=ABX(I+3*LT)*FRW(I)	GAELO041
50	CONTINUE	GAELO042
	IF (IFLT.EQ.0) GO TO 56	GAELO043
	ABX(N)=FREQ*ABX(N)	GAELO044
56	CONTINUE	GAELO045
	WRITE(6,100) FREQ	GAELO046
100	FORMAT(//3X,'--',F 6.2,'--')	GAELO047
	WRITE(6,200)(ABX(I),I=1,N)	GAELO048
200	FORMAT(//8X,9(E10.3,2X)//)	GAELO049
	RETURN	GAELO050
	END	GAELO051

SUBROUTINE EIGEN(N,AAA,BBB,CCC,DDD,IDEF)

ROUTINE TO FORM AN EIGENVALUE PROBLEM AND TO CALL EIPACK SUBROUTINE

DIMENSION AAA(19,19), BBB(19,19), CCC(19,19), DDD(19,6)

DIMENSION A(361), L(19), M(19), AINV(19,19)

DIMENSION AAN(19,19), BBN(19,19), CCN(19,19), DDN(19,6)

REAL*8 AFIG(38,38), WR(38), WI(38), ZP(38,38)

REAL*8 SCALE(38)

INTEGER INT(38)

DIMENSION RTG(25), ARMOD(25,25), DAMP(38)

COMPLEX AMOD(25,25), RTGCOM(25)

COMMON/FRMAG/ FPR(4), FPRD(4), FRW(6), TFRMAG

IDEBUG=0

WRITF(6,153)

DO 3003 I=1,N

DO 3004 J=1,N

AAN(I,J)=0.0

BBN(I,J)=0.0

3004 CCN(I,J)=0.0

DO 3005 K=1,6

3005 DDN(I,K)=0.0

3003 CONTINUE

LL=0

DO 1000 J=1,N

DO 1000 I=1,N

LL=LL+1

1000 A(LL)=AAA(I,J)

CALL MINV(A,N,D,L,M)

LL=0

DO 2000 J=1,N

DO 2000 I=1,N

LL=LL+1

2000 AINV(I,J)=A(LL)

DO 3000 I=1,N

DO 3001 J=1,N

ETGF0001

ETGF0002

EIGE0003

EIGE0004

EIGF0005

EIGF0006

EIGF0007

EIGF0008

EIGE0009

EIGE0010

EIGF0011

EIGE0012

EIGE0013

EIGE0014

ETGF0015

EIGE0016

ETGE0017

EIGE0018

ETGF0019

ETGF0020

EIGF0021

EIGE0022

ETGF0023

EIGE0024

ETGF0025

EIGF0026

ETGF0027

EIGE0028

ETGF0029

EIGE0030

EIGE0031

EIGE0032

ETGF0033

EIGF0034

EIGE0035

ETGF0036

DO 3001 K=1,N
 AAN(I,J)=AINV(I,K)*AAA(K,J)+AAN(I,J)
 RBN(I,J)=AINV(I,K)*BBB(K,J)+RBN(I,J)
 3001 CCN(I,J)=AINV(I,K)*CCC(K,J)+CCN(I,J)
 DO 3002 J=1,6
 DO 3002 K=1,N
 3002 DDN(I,J)=AINV(I,K)*DDD(K,J)+DDN(I,J)
 3000 CONTINUE
 6000 N2=2*N
 DO 300 I=1,N
 DO 300 J=1,N
 AEIG(I,J)=-RBN(I,J)
 300 AFIG(I,J+N)=-CCN(I,J)
 DO 301 I=1,N
 DO 301 J=1,N2
 301 AFIG(I+N,J)=0.0D0
 DO 302 I=1,N
 302 AFIG(I+N,I)=1.0D0
 CALL ETPACK(38,N2,AEIG,WR, WI, ZP, TERROR , SCALE , INT)
 IF(TERROR.EQ.0) GO TO 152
 WRITE(6,150)TERROR
 150 FORMAT(15X,'TERROR=',I5)
 152 CONTINUE
 IF(TDEBUG.EQ.0) GO TO 61
 WRITE(6,671)(WR(I),WI(I),I=1,N2)
 671 FORMAT(//10X,D15.7,2X,D15.7)
 N3=N/3
 DO 400 IL=1,N3
 TJ=6*(IL-1)+1
 KL=6*(IL-1)+6
 400 WRITE(6,251)(ZP(I,J),J=TJ,KL),I=1,N2)
 251 FORMAT(//1X,(/1X,(2D15.7,4X,2D15.7,4X,2D15.7))
 IF(3*N3.EQ.0) GO TO 61
 K=2*(N-3*N3)
 TJ=KL+1
 KL=KL+K

EIGE0037
 EIGE0038
 EIGE0039
 EIGE0040
 EIGE0041
 EIGE0042
 EIGE0043
 EIGE0044
 EIGE0045
 EIGE0046
 EIGE0047
 EIGE0048
 EIGE0049
 EIGE0050
 EIGE0051
 EIGE0052
 EIGE0053
 EIGE0054
 EIGE0055
 EIGE0056
 EIGE0057
 EIGE0058
 EIGE0059
 EIGE0060
 EIGE0061
 EIGE0062
 EIGE0063
 EIGE0064
 EIGE0065
 EIGE0066
 EIGE0067
 EIGE0068
 EIGE0069
 EIGE0070
 EIGE0071
 EIGE0072

```

      WRITE(6,751)((ZP(I,J),J=IJ,KL),I=1,N2)          EIGE0073
751  FORMAT(//1X,(/1X,(2D15.7)))
61   CONTINUE
      DO 140 I=1,N2
      XX=SNGL(WR(I)*#2+WI(I)*#2)
      IF(XX.EQ.0.0) GO TO 141
      DAMP(I)=-SNGL(WR(I))/SQRT(XX)
      GO TO 140
141  DAMP(I)=0.0
140  CONTINUE
      N1=N+1
      LK=0
      LKK=0
      NTOT=0
      I=1
64   CONTINUE
      IF(I.GE.N2+1) GO TO 63
      NTOT=NTOT+1
      K=NTOT
      IF(WI(I).EQ.0.000) GO TO 65
      INT(I)=K
      INT(I+1)=K
      LK=LKK+1
      LKK=LK+1
      IF(1DEBUG.EQ.0) GO TO 68
      WRITE(6,69) I,LK,LKK,K
69   FORMAT(1X,4I5)
68   CONTINUE
      DO 50 J=N1,N2
      IF(1DEBUG.EQ.0) GO TO 71
      WRITE(6,72) ZP(J,LK),ZP(J,LKK)
72   FORMAT(1X,2D15.7)
71   CONTINUE
      AMDO(K,J-N1+1)=CMPLX(SNGL(ZP(J,LK)),SNGL(ZP(J,LKK)))
50   CONTINUE
      I=I+2

```

65	GO TO 64	EIGE0109
	CONTINUE	EIGE0110
	INT(I)=K	EIGE0111
	LK=LKK+1	EIGE0112
	LKK=LK	EIGE0113
	IF (IDFRUG.EQ.0) GO TO 73	EIGE0114
	WRITE(6,69)I,LK,LKK,K	EIGE0115
73	CONTINUE	EIGE0116
	DO 66 J=N1,N2	EIGE0117
	IF (IDFRUG.EQ.0) GO TO 74	EIGE0118
	WRITE(6,72)ZP(J,LK),ZP(J,LKK)	EIGE0119
74	CONTINUE	EIGE0120
	AMOD(K,I-N1+1)=CMPLX(SNGL(ZP(J,LK)),0.0)	EIGE0121
66	CONTINUE	EIGE0122
	I=I+1	EIGE0123
	GO TO 64	EIGE0124
63	CONTINUE	EIGE0125
tst	IF (IFRMAG.EQ.1) GO TO 130	EIGE0126
	IF (IDOF.EQ.9) GO TO 131	EIGE0127
	LT=4	EIGE0128
	LTT=6	EIGE0129
	GO TO 134	EIGE0130
131	LT=2	EIGE0131
	LTT=3	EIGE0132
134	CONTINUE	EIGE0133
	DO 136 TJ=1,NTOT	EIGE0134
	DO 132 I=1,LT	EIGE0135
	DO 132 J=1,3	EIGE0136
132	AMOD(IJ,3*(I-1)+J)= AMOD(IJ,3*(I-1)+J)*FRB(I)	EIGE0137
	DO 135 I=1,LT	EIGE0138
135	AMOD(TJ,3*(I-1)+1)= AMOD(TJ,3*(I-1)+1)*FRBD(I)/FRB(I)	EIGE0139
	DO 133 I=1,LTT	EIGE0140
133	AMOD(IJ,I+3*LT)=AMOD(IJ,I+3*LT)*FRW(I)	EIGE0141
136	CONTINUE	EIGE0142
130	CONTINUE	EIGE0143
	DO 51 I=1,NTOT	EIGE0144

```

51    DO 51 J=1,N
      ABMOD(I,J)=CABS(AMOD(I,J))
      DO 52 I=1,NTOT
      BIG(I)=0.0
      DO 53 J=1,N
      IF(ABMOD(I,J) -  BIG(I)) 53,53,54
54      BIG(I)=ABMOD(I,J)
      BIGCOM(I)=AMOD(I,J)
53      CONTINUE
52      CONTINUE
      DO 60 I=1,NTOT
      DO 60 J=1,N
      ABMOD(I,J)=ABMOD(I,J)/BIG(I)
      AMOD(I,J)=AMOD(I,J)/BIGCOM(I)
60      CONTINUE
153      FORMAT(//15X,20(1H*)//20X,'EIGENVALUES',//15X, 20(1H*),
      &      //20X,'** REAL PART **', 3X,'** IMAGINARY PART **'
      &      ,10X,'** DAMPING RATIO **')
      WRITE(6,151)(INT(I),WR(I),WI(I),DAMP(I),I=1,N2)
151      FORMAT( 9X,'NO.',I2,5X,D15.7,5X,D15.7,15X,F15.7)
      WRITE(6,59)
59      FORMAT(1H1,//5X, 20 (1H*),//10X,  'EIGENVECTORS',//5X, 20(1H*))
      IP=0
      DO 55 I=1,NTOT
      IP=IP+1
      WRITE(6,154)I      ,WR(IP),WI(IP)
154      FORMAT(//2X,'-- CORRESPONDING TO NO.',I2,1X,'EIGENVALUE --',
      &      5X,'(',D10.3,')'+IMAG('D10.3,''),
      &      //8X,'** ABSOLUTE VALUE **',20X,'** REAL PART **',2X,
      &      '** IMAGINARY PART **',//)
      IF((IP+1).GT.N2) GO TO 752
      IF(INT(IP).EQ.INT(IP+1)) IP=IP+1
752      CONTINUE
      DO 56 J=1,N
      WRITE(6,57)ABMOD(I,J), AMOD(I,J)
57      FORMAT(10X,F15.7,22X,E15.7,3X,E15.7)

```

56 CONTINUE
58 WRITE(6,58)
59 FORMAT(//1X)
55 CONTINUE
RETURN
END

EIGE0181
EIGE0182
EIGE0183
EIGE0184
EIGE0185
EIGE0186

153

SUBROUTINE EIPACK(NM, N, A, WR, WI, Z , IERR,SCALE,INT)
C
C AN EIGENSYSTEM PROBLEM SOLVER FOR THE GENERAL MATRIX
C
REAL*8 A(NM,N),Z(NM,N), WR(N), WI(N) ,SCALE(N)
INTEGER INT(N)
CALL BALANC(NM,N,A,LOW,IGH,SCALE)
CALL ELMHES(NM,N,LOW,IGH,A,INT)
CALL ELTRAN(NM,N,LOW,IGH,A,INT,Z)
CALL HQR2(NM,N,LOW,IGH,A,WR,WI,Z,IERR)
CALL BAIRAK(NM,N,LOW,IGH,SCALE,N,Z)
RETURN
END

EIPA0001
EIPA0002
EIPA0003
EIPA0004
EIPA0005
EIPA0006
EIPA0007
EIPA0008
EIPA0009
EIPA0010
EIPA0011
EIPA0012
EIPA0013

C 69210001
C ----- 69210002
C 69210003
C SUBROUTINE BALANC(NM,N,A,LOW,IGH,SCALE) 69210004
C 69210005
C INTEGER I,J,K,L,M,N,JI,NM,IGH,LOW,IEXC 69210006
C REAL*8 A(NM,N),SCALE(N) 69210007
C REAL*8 C,F,G,R,S,B2,RADIX 69210008
C REAL*8 DABS 69210009
C LOGICAL NOCONV 69210010
C 69210011
C THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE BALANCE. 69210012
C NUM. MATH. 13, 293-304(1969) BY PARLETT AND REINSCH. 69210013
C HANDBOOK FOR AUTO. COMP., VOL.II-LINEAR ALGEBRA, 315-326(1971). 69210014
C 69210015
C THIS SUBROUTINE BALANCES A REAL MATRIX AND ISOLATES 69210016
C EIGENVALUES WHENEVER POSSIBLE. 69210017
C 69210018
C ON INPUT: 69210019
C 69210020
C NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL 69210021
C ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM 69210022
C DIMENSION STATEMENT; 69210023
C 69210024
C N IS THE ORDER OF THE MATRIX; 69210025
C 69210026
C A CONTAINS THE INPUT MATRIX TO BE BALANCED. 69210027
C 69210028
C ON OUTPUT: 69210029
C 69210030
C A CONTAINS THE BALANCED MATRIX; 69210031
C 69210032
C LOW AND IGH ARE TWO INTEGERS SUCH THAT A(I,J) 69210033
C IS EQUAL TO ZERO IF
C (1) I IS GREATER THAN J AND 69210034
C (2) J=1,...,LOW-1 OR I=IGH+1,...,N; 69210035
C 69210036

C SCALE CONTAINS INFORMATION DETERMINING THE 69210037
 C PERMUTATIONS AND SCALING FACTORS USED. 69210038
 C 69210039
 C 69210040
 C SUPPOSE THAT THE PRINCIPAL SUBMATRIX IN ROWS LCW THROUGH IGH 69210041
 C HAS BEEN BALANCED, THAT P(J) DENOTES THE INDEX INTERCHANGED 69210042
 C WITH J DURING THE PERMUTATION STEP, AND THAT THE ELEMENTS 69210043
 C OF THE DIAGONAL MATRIX USED ARE DENOTED BY E(I,J). THEN 69210044
 C SCALE(J) = P(J), FOR J = 1, ..., LOW-1 69210045
 C = E(J,J), J = LCW, ..., IGH 69210046
 C = P(J) J = IGH+1, ..., N. 69210047
 C THE ORDER IN WHICH THE INTERCHANGES ARE MADE IS N TO IGH+1, 69210048
 C THEN 1 TO LCW-1. 69210049
 C 69210050
 C NOTE THAT I IS RETURNED FOR IGH IF IGH IS ZERO FORMALLY. 69210051
 C 69210052
 C THE ALGOL PROCEDURE EXC CONTAINED IN BALANCE APPEARS IN 69210053
 C BALANC IN LINE. (NOTE THAT THE ALGOL RULES OF IDENTIFIERS 69210054
 C K,L HAVE BEEN REVERSED.) 69210055
 C 69210056
 C QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW, 69210057
 C APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY 69210058
 C 69210059
 C ----- 69210060
 C :::::::::: RADIX IS A MACHINE DEPENDENT PARAMETER SPECIFYING 69210061
 C THE BASE OF THE MACHINE FLOATING POINT REPRESENTATION. 69210062
 C RADIX = 16.000 FOR LONG FORM ARITHMETIC 69210063
 C ON S360 :::::::::::: 69210064
 C DATA RADIX/2421CCCCCCCCCCCC/ 69210065
 C 69210066
 C B2 = RADIX * RADIX 69210067
 C K = 1 69210068
 C L = N 69210069
 C GO TO 100 69210070
 C :::::::::::: IN-LINE PROCEDURE FOR ROW AND 69210071
 C 69210072

C	COLLUMN EXCHANGE ::::::::::::	69210073
20	SCALE(M) = J	69210074
	IF (J .EQ. M) GC TC 50	69210075
C	DC 30 I = 1, L	69210076
	F = A(I,J)	69210077
	A(I,J) = A(I,M)	69210078
	A(I,M) = F	69210079
30	CENTINLE	69210080
C	DC 40 I = K, N	69210081
	F = A(J,I)	69210082
	A(J,I) = A(M,I)	69210083
	A(M,I) = F	69210084
40	CONTINUE	69210085
C	50 GC TC 180, 130), IEXC	69210086
C	::::::::::: SEARCH FOR ROWS ISOLATING AN EIGENVALUE	69210089
C	AND PUSH THEM DOWN ::::::::::::	69210090
50	IF (L .EQ. 1) GC TC 280	69210091
	L = L - 1	69210092
C	::::::::::: FOR J=L STEP -1 UNTIL 1 DO -- ::::::::::::	69210093
100	DC 120 JJ = 1, L	69210094
	J = L + 1 - JJ	69210095
C	DC 110 I = 1, L	69210096
	IF (I .EQ. J) GC TC 110	69210097
	IF (A(J,I) .NE. 0.0DC) GC TC 120	69210098
110	CONTINUE	69210099
C	M = L	69210100
	IEXC = 1	69210101
	GC TC 20	69210102
120	CENTINLE	69210103
C	GC TC 140	69210104
		69210105
		69210106
		69210107
		69210108

```

C      :::::::::::: SEARCH FOR COLUMNS ISOLATING AN EIGENVALUE      69210109
C      AND PUSH THEM LEFT ::::::::::::
130 K = K + 1                                         69210110
C
140 DO 170 J = K, L                                 69210111
C
      EC 150 I = K, L                               69210112
      IF (I .EQ. J) GC TO 150                      69210113
      IF (A(I,J) .NE. 0.000) GC TO 170            69210114
150  CONTINUE                                         69210115
C
      N = K                                         69210116
      IEXC = 2                                       69210117
      GC TO 20                                     69210118
170  CONTINUE                                         69210119
C      :::::::::::: NOW BALANCE THE SUBMATRIX IN ROWS K TO L :::::::::::: 69210120
      DO 180 I = K, L                               69210121
180  SCALE(I) = 1.000                            69210122
C      :::::::::::: ITERATIVE LCCP FOR NORM REDUCTION :::::::::::: 69210123
190  NOCONV = .FALSE.                            69210124
C
      EC 270 I = K, L                               69210125
      C = C.CDC                                     69210126
      R = C.CDC                                     69210127
C
      EC 200 J = K, L                               69210128
      IF (J .EQ. I) GC TO 200                      69210129
      C = C + CABS(A(J,I))                         69210130
      R = R + CABS(A(I,J))                         69210131
200  CONTINUE                                         69210132
C
      G = R / RADIX                                69210133
      F = 1.000                                     69210134
      S = C + R                                     69210135
210  IF (C .GE. G) GC TO 220                      69210136
      F = F * RADIX                                69210137

```

	C = C * R2	69210145
	GC TC 210	69210146
220	G = R * RADIX	69210147
230	IF (C .LT. G) GC TC 240	69210148
	F = F / RADIX	69210149
	C = C / R2	69210150
	GC TO 230	69210151
C	::::::: NOW BALANCE ::::::::::::	69210152
240	IF ((C + R) / F .GE. 0.9500 * S) GC TC 270	69210153
	G = 1.000 / F	69210154
	SCALE(I) = SCALE(I) * F	69210155
	NOCCNV = .TRUE.	69210156
C	CC 250 J = K, N	69210157
250	A(I,J) = A(I,J) * G	69210158
C	CC 260 J = 1, L	69210159
260	A(J,I) = A(J,I) * F	69210160
C	270 CONTINUE	69210161
C	IF (NOCCNV) GC TC 190	69210162
C	280 LOW = K	69210163
	HIGH = L	69210164
	RETURN	69210165
C	::::::: LAST CARD OF BALANC ::::::::::::	69210166
	END	69210167
		69210168
		69210169
		69210170
		69210171
		69210172

```

C                               73210001
C----- 73210002
C                               73210003
C----- 73210004
C----- 73210005
C----- 73210006
C----- 73210007
C----- 73210008
C----- 73210009
C----- 73210010
C----- 73210011
C----- 73210012
C----- 73210013
C----- 73210014
C----- 73210015
C----- 73210016
C----- 73210017
C----- 73210018
C----- 73210019
C----- 73210020
C----- 73210021
C----- 73210022
C----- 73210023
C----- 73210024
C----- 73210025
C----- 73210026
C----- 73210027
C----- 73210028
C----- 73210029
C----- 73210030
C----- 73210031
C----- 73210032
C----- 73210033
C----- 73210034
C----- 73210035
C----- 73210036

SUBROUTINE ELMHES(N,LCW,IGH,A,INT)
  INTEGER I,J,M,N,LA,NM,IGH,KP1,LOW,MPI1,MPI
  REAL*8 A(NM,N)
  REAL*8 X,Y
  REAL*8 DABS
  INTEGER INT(IGH)

THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE ELMHES,
NUM. MATH. 12, 349-368(1968) BY MARTIN AND WILKINSON.
HANDBOOK FOR AUTO. COMP., VOL.II-LINEAR ALGEBRA, 339-358(1971).

GIVEN A REAL GENERAL MATRIX, THIS SUBROUTINE
REDUCES A SUBMATRIX SITUATED IN ROWS AND COLUMNS
LOW THROUGH IGH TO UPPER HESSENBERG FORM BY
STABILIZED ELEMENTARY SIMILARITY TRANSFORMATIONS.

ON INPUT:
  NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL
  ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM
  DIMENSION STATEMENT:
  N IS THE ORDER OF THE MATRIX:
  LOW AND IGH ARE INTEGERS DETERMINED BY THE BALANCING
  SUBROUTINE BALANC. IF BALANC HAS NOT BEEN USED,
  SET LCW=1, IGH=N;
  A CONTAINS THE INPUT MATRIX.

ON OUTPUT:

```

C A CONTAINS THE HESSENBERG MATRIX. THE MULTIPLIERS 73210037
 C WHICH WERE USED IN THE REDUCTION ARE STORED IN THE 73210038
 C REMAINING TRIANGLE UNDER THE HESSENBERG MATRIX; 73210039
 C
 C INT CONTAINS INFORMATION ON THE ROWS AND COLUMNS 73210040
 C INTERCHANGED IN THE REDUCTION. 73210042
 C ONLY ELEMENTS LOW THROUGH IGH ARE USED. 73210043
 C
 C QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW, 73210044
 C APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY 73210045
 C
 C ----- 73210048
 C
 C LA = IGH - 1 73210049
 C KPI = LOW + 1 73210050
 C IF (LA .LT. KPI) GO TO 200 73210051
 C
 C DO 180 M = KPI, LA 73210052
 C M1 = M - 1 73210053
 C X = 0.000 73210054
 C I = M 73210055
 C
 C 100 CC 100 J = M, 1CH 73210056
 C IF (DABS(A(J,M1)) .LE. DABS(X)) GO TO 100 73210057
 C X = A(J,M1) 73210058
 C I = J 73210059
 C 100 CCNTINUE 73210060
 C
 C INT(M) = I 73210061
 C IF (I .EQ. M) GO TO 130 73210062
 C ::::::::::: INTERCHANGE ROWS AND COLUMNS OF A ::::::::::: 73210063
 C DO 110 J = M1, N 73210064
 C Y = A(I,J) 73210065
 C A(I,J) = A(M,J) 73210066
 C A(M,J) = Y 73210067
 C 110 CCNTINUE 73210068

C	DC 120 J = 1, IGF	7321C073
	Y = A(J,I)	7321C074
	A(J,I) = A(J,M)	73210075
	A(J,M) = Y	7321C076
120	CONTINUE	7321C077
C	:::::::::: END INTERCHANGE ::::::::::::	7321C078
130	IF (X .EQ. C.0DC) GO TO 180	73210079
	MPI = M + 1	73210080
C	DC 160 I = MPI, IGF	73210081
	Y = A(I,MPI)	73210082
	IF (Y .EQ. C.0DC) GO TO 160	73210083
	Y = Y / X	73210084
	A(I,MPI) = Y	73210085
C	DC 140 J = M, N	73210086
140	A(I,J) = A(I,J) - Y * A(M,J)	73210087
C	DC 150 J = 1, IGF	73210088
150	A(J,M) = A(J,M) + Y * A(J,I)	73210089
C	160 CONTINUE	73210090
C	180 CONTINUE	73210091
C	200 RETURN	73210092
C	:::::::::: LAST CARD OF ELMSES ::::::::::::	73210093
	END	73210094
		73210095
		73210096
		73210097
		73210098
		73210099
		73210100
		73210101

```

C-----20210001
C-----20210002
C-----20210003
C-----20210004
C-----20210005
C-----20210006
C-----20210007
C-----20210008
C-----20210009
C-----20210010
C-----20210011
C-----20210012
C-----20210013
C-----20210014
C-----20210015
C-----20210016
C-----20210017
C-----20210018
C-----20210019
C-----20210020
C-----20210021
C-----20210022
C-----20210023
C-----20210024
C-----20210025
C-----20210026
C-----20210027
C-----20210028
C-----20210029
C-----20210030
C-----20210031
C-----20210032
C-----20210033
C-----20210034
C-----20210035
C-----20210036

SUBROUTINE ELTRAN(NM,N,LCW,IGH,A,INT,Z)          20210001
-----20210002
-----20210003
-----20210004
-----20210005
-----20210006
-----20210007
-----20210008
-----20210009
-----20210010
-----20210011
-----20210012
-----20210013
-----20210014
-----20210015
-----20210016
-----20210017
-----20210018
-----20210019
-----20210020
-----20210021
-----20210022
-----20210023
-----20210024
-----20210025
-----20210026
-----20210027
-----20210028
-----20210029
-----20210030
-----20210031
-----20210032
-----20210033
-----20210034
-----20210035
-----20210036

INTEGER I,J,N,KL,NM,MP,NM,IGH,LOW,MP1          20210001
REAL*8 A(NM,IGH),Z(NM,N)                        20210002
INTEGER INT(IGH)                                20210003

THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE ELMTRANS, 20210004
NUM. MATH. 16, 181-204(1970) BY PETERS AND WILKINSON. 20210005
HANDBOOK FOR AUTO. COMP., VOL.II-LINEAR ALGEBRA, 372-395(1971). 20210006

THIS SUBROUTINE ACCUMULATES THE STABILIZED ELEMENTARY 20210007
SIMILARITY TRANSFORMATIONS USED IN THE REDUCTION OF A 20210008
REAL GENERAL MATRIX TO UPPER HESSENBERG FORM BY ELMHES. 20210009

ON INPUT:                                         20210010
-----20210011
-----20210012
-----20210013
-----20210014
-----20210015
-----20210016
-----20210017
-----20210018
-----20210019
-----20210020
-----20210021
-----20210022
-----20210023
-----20210024
-----20210025
-----20210026
-----20210027
-----20210028
-----20210029
-----20210030
-----20210031
-----20210032
-----20210033
-----20210034
-----20210035
-----20210036

NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL 20210020
ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM 20210021
DIMENSION STATEMENT;                            20210022
-----20210023
-----20210024
-----20210025
-----20210026
-----20210027
-----20210028
-----20210029
-----20210030
-----20210031
-----20210032
-----20210033
-----20210034
-----20210035
-----20210036

N IS THE ORDER OF THE MATRIX;                  20210024
-----20210025
-----20210026
-----20210027
-----20210028
-----20210029
-----20210030
-----20210031
-----20210032
-----20210033
-----20210034
-----20210035
-----20210036

LCW AND IGH ARE INTEGERS DETERMINED BY THE BALANCING 20210026
SUBROUTINE BALANC. IF BALANC HAS NOT BEEN USED, 20210027
SET LOW=1, IGH=N;                            20210028
-----20210029
-----20210030
-----20210031
-----20210032
-----20210033
-----20210034
-----20210035
-----20210036

A CONTAINS THE MULTIPLIERS WHICH WERE USED IN THE 20210030
REDUCTION BY ELMHES IN ITS LOWER TRIANGLE 20210031
BELOW THE SUBDIAGONAL;                      20210032
-----20210033
-----20210034
-----20210035
-----20210036

INT CONTAINS INFORMATION ON THE ROWS AND COLUMNS 20210034
INTERCHANGED IN THE REDUCTION BY ELMHES. 20210035
ONLY ELEMENTS LCW THROUGH IGH ARE USED. 20210036

```

C 20210037
 C ON CLTPUT:
 C 20210038
 C Z CONTAINS THE TRANSFORMATION MATRIX PRODUCED IN THE
 C 20210039
 C REDUCTION BY ELMHES.
 C 20210040
 C QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW,
 C 20210041
 C APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY
 C 20210042
 C 20210043
 C 20210044
 C 20210045
 C 20210046
 C 20210047
 C ::::::: INITIALIZE Z TO IDENTITY MATRIX :::::::
 C 20210048
 C DO 80 I = 1, N
 C 20210049
 C 20210050
 C 20210051
 C 60 Z(I,J) = 0.000
 C 20210052
 C 20210053
 C 20210054
 C 20210055
 C 20210056
 C 20210057
 C 20210058
 C 20210059
 C ::::::: FOR MP=IGH-1 STEP -1 UNTIL LCH+1 DO -- :::::::
 C 20210060
 C 140 MM = 1, KL
 C 20210061
 C MP = IGH - MM
 C 20210062
 C MP1 = MP + 1
 C 20210063
 C 20210064
 C 100 Z(I,MP) = A(I,MP-1)
 C 20210065
 C 20210066
 C 20210067
 C I = INT(MP)
 C 20210068
 C IF (I .EQ. MP) GO TO 140
 C 20210069
 C 20210070
 C 130 J = MP, IGH
 C 20210071
 C Z(MP,J) = Z(I,J)
 C 20210072
 C Z(I,J) = C.CEC

130	CONTINUE	20210073
C		20210074
	Z(I,MP) = 1.000	20210075
140	CONTINUE	20210076
C		20210077
200	RETURN	20210078
C	::::::: LAST CARD OF ELTRAN ::::::	20210079
	END	20210080

```

SUBROUTINE FQR2(NM,N,LCH,IGH,H,WR,WI,Z,IERR)
  INTEGER I,J,K,L,N,N,EN,IT,JJ,LL,NR,NA,NN,NN,
  X      IGH,ITS,LCH,MP2,ENM2,IERR
  REAL*8 H(NM,N),VR(N),WI(N),Z(NM,N)
  REAL*8 P,Q,R,S,T,W,X,Y,RA,SA,VI,VR,ZZ,NCRM,MACHEP
  REAL*8 CSGRT,CAES,CSIGN
  INTEGER MINC
  LOGICAL ACTLAS
  COMPLEX*16 Z3
  COMPLEX*16 ECMFLX
  REAL*8 T3(2)
  EQUIVALENCE (Z3,T3(1))

  THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE HQR2,
  NUM. MATH. 16, 181-204(1970) BY PETERS AND WILKINSON.
  HANDBOOK FOR ALG. COMP., VOL.II-LINEAR ALGEBRA, 372-395(1971).

  THIS SUBROUTINE FINDS THE EIGENVALUES AND EIGENVECTORS
  OF A REAL UPPER HESSENBERG MATRIX BY THE QR METHOD. THE
  EIGENVECTORS OF A REAL GENERAL MATRIX CAN ALSO BE FOUND
  IF ELMHES AND ELTRAN OR CRTHES AND CRTRAN HAVE
  BEEN USED TO REDUCE THIS GENERAL MATRIX TO HESSENBERG FORM
  AND TO ACCUMULATE THE SIMILARITY TRANSFORMATIONS.

  ON INPUT:
    NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL
    ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM
    DIMENSION STATEMENT;
    N IS THE ORDER OF THE MATRIX;

```

C LCW AND IGH ARE INTEGERS DETERMINED BY THE BALANCING
 C SUBCUTINE BALANC. IF BALANC HAS NOT BEEN USED,
 C SET LCW=1, IGH=N; 87210037
 C 87210038
 C 87210039
 C 87210040
 C 87210041
 C 87210042
 C F CONTAINS THE UPPER HESSENBERG MATRIX; 87210043
 C 87210044
 C Z CONTAINS THE TRANSFORMATION MATRIX PRECUCED BY ELTRAN
 C AFTER THE REDUCTION BY ELMHES, OR BY CRTRAN AFTER THE
 C REDUCTION BY CRTHES, IF PERFORMED. IF THE EIGENVECTRS
 C OF THE HESSENBERG MATRIX ARE DESIRED, Z MUST CCONTAIN THE
 C IDENTITY MATRIX. 87210045
 C 87210046
 C 87210047
 C 87210048
 C ON CLPUT:
 C 87210049
 C 87210050
 C F HAS BEEN DESTROYED; 87210051
 C 87210052
 C WR AND WI CCONTAIN THE REAL AND IMAGINARY PARTS,
 C RESPECTIVELY, OF THE EIGENVALUES. THE EIGENVALUES
 C ARE UNORDERED EXCEPT THAT COMPLEX CONJUGATE PAIRS
 C OF VALUES APPEAR CONSECUTIVELY WITH THE EIGENVALUE
 C HAVING THE POSITIVE IMAGINARY PART FIRST. IF AN
 C ERROR EXIT IS MADE, THE EIGENVALLES SHOULD BE CORRECT
 C FOR INDICES IERR+1,...,N; 87210053
 C 87210054
 C 87210055
 C 87210056
 C 87210057
 C 87210058
 C 87210059
 C 87210060
 C Z CONTAINS THE REAL AND IMAGINARY PARTS OF THE EIGENVECTRS. 87210061
 C IF THE I-TH EIGENVALUE IS REAL, THE I-TH COLUMN OF Z 87210062
 C CCONTAINS ITS EIGENVECTOR. IF THE I-TH EIGENVALUE IS COMPLEX 87210063
 C WITH POSITIVE IMAGINARY PART, THE I-TH AND (I+1)-TH
 C COLUMNS OF Z CCONTAIN THE REAL AND IMAGINARY PARTS OF ITS 87210064
 C EIGENVECTOR. THE EIGENVECTRS ARE LANCRALIZED. IF AN 87210065
 C ERROR EXIT IS MADE, NONE OF THE EIGENVECTRS HAS BEEN FCUNE; 87210066
 C 87210067
 C 87210068
 C IERR IS SET TO
 C ZERO FOR NORMAL RETURN, 87210069
 C J IF THE J-TH EIGENVALUE HAS NOT BEEN
 C DETERMINED AFTER 30 ITERATIONS. 87210070
 C 87210071
 C 87210072

```

C ARITHMETIC IS REAL EXCEPT FOR THE REPLACEMENT OF THE ALGOL      87210073
C PROCEDURE CCIV BY COMPLEX DIVISION.                                87210074
C                                                               87210075
C                                                               87210076
C QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARECK,      87210077
C APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY      87210078
C                                                               87210079
C -----
C ::::::::::: MACHEP IS A MACHINE DEPENDENT PARAMETER SPECIFYING      87210080
C THE RELATIVE PRECISION OF FLOATING POINT ARITHMETIC.            87210081
C MACHEP = 1E.0DC**(-13) FOR LONG FORM ARITHMETIC                 87210082
C CN S360 :::::::                                                 87210083
C DATA MACHEP/Z341CC0000000000/                                      87210084
C                                                               87210085
C IEPR = C                                                       87210086
C ::::::::::: STORE ROOTS ISOLATED BY BALANC :::::::                87210087
C DO 50 I = 1, N
C     IF (I .GE. LCH .AND. I .LE. IGH) GO TO 50
C     WR(I) = R(I,I)
C     WI(I) = C.0DC
C 50 CONTINUE
C
C EN = ICH
C T = C.0DC
C ::::::::::: SEARCH FOR NEXT EIGENVALUES :::::::                  87210096
C 60 IF 1EN .LT. LCH) GO TO 340
C ITS = C
C NA = EN - 1
C ENN2 = NA - 1
C ::::::::::: LOOK FOR SINGLE SMALL SUB-DIAGONAL ELEMENT          87210097
C             FOR L=EN STEP -1 UNTIL LCH DO -- :::::::                87210098
C 70 DO 80 LL = LCH, EN
C     L = EN + LCH - LL
C     IF (L .EQ. LCH) GO TO 100
C     IF (DABS(H(L,L-1)) .LE. MACHEP * (DABS(H(L-1,L-1)))      87210099
C

```

```

      X      + CABS(F(L,L))) GO TC 100          87210109
      F0 CONTINLF                                87210110
C      :::::::::::: FORM SHIFT ::::::::::::      87210111
100 X = F(EN,EN)                                87210112
      IF (L .EQ. EN) CC TC 270                  87210113
      Y = H(NA,NA)                                87210114
      W = F(EN,NA) * F(NA,EN)                  87210115
      IF (L .EQ. NA) CC TO 280                  87210116
      IF (ITS .EQ. 3C) GC TC 1000                87210117
      IF (ITS .NE. 1C .AND. ITS .NE. 2C) GO TC 130 87210118
C      :::::::::::: FORM EXCEPTIONAL SHIFT :::::::::::: 87210119
      T = T + X                                87210120
C
      DO 120 I = LOW, EN                      87210121
120 H(I,I) = F(I,I) - X                      87210122
C
      S = DABS(H(EN,NA)) + DABS(F(NA,ENM2)) 87210123
      X = C.75DC * S                          87210124
      Y = X                                    87210125
      W = -0.4375DC * S * S                  87210126
130 ITS = ITS + 1                            87210127
C      :::::::::::: LOOK FOR TWO CONSECUTIVE SMALL 87210128
C          SUB-DIAGONAL ELEMENTS.                87210129
C          FOR M=EN-2 STEP -1 UNTIL L DO -- :::::::::::: 87210130
C
      DO 140 MM = L, ENM2                      87210131
      M = ENM2 + L - MM                      87210132
      ZZ = H(M,M)                                87210133
      R = X - ZZ                                87210134
      S = Y - ZZ                                87210135
      P = (R + S - W) / F(M+1,M) + F(M,M+1) 87210136
      G = H(M+1,M+1) - ZZ - R - S            87210137
      R = H(M+2,M+1)                            87210138
      S = CABS(P) + CABS(G) + CABS(R)          87210139
      F = P / S                                87210140
      G = Q / S                                87210141
      R = R / S                                87210142
      Q = R / S                                87210143
      P = P / S                                87210144

```

IF (N .EQ. L) GO TO 150 87210145
 IF (DABS(H(N,N-1)) * (DABS(G) + DABS(R)) .LE. MACHEP * DABS(P)) 87210146
 X * (DABS(H(N-1,N-1)) + DABS(ZZ) + DABS(H(N+1,N+1))) GO TO 150 87210147
 140 CONTINUE 87210148
 C 87210149
 150 MP2 = N + 2 87210150
 C 87210151
 CC 160 T = MP2, EN 87210152
 H(I,I-2) = C.CCC 87210153
 IF (I .EQ. MP2) GO TO 160 87210154
 H(I,I-3) = C.CCC 87210155
 160 CONTINUE 87210156
 C ::::::::::: DOUBLE GR STEP INVOLVING ROWS L TO EN AND 87210157
 C COLUMNS M TO EN ::::::::::: 87210158
 CC 260 K = N, NA 87210159
 NCLAS = K .NE. NA 87210160
 IF (K .EQ. N) GO TO 170 87210161
 P = H(K,K-1) 87210162
 G = H(K+1,K-1) 87210163
 R = C.CCC 87210164
 IF (NCLAS) R = H(K+2,K-1) 87210165
 X = DABS(P) + DABS(G) + DABS(R) 87210166
 IF (X .EQ. C.CCC) GO TO 260 87210167
 P = P / X 87210168
 G = G / X 87210169
 R = R / X 87210170
 170 S = DSIGN(DSQR(P*P+Q*Q+R*R),P) 87210171
 IF (K .EQ. N) GO TO 180 87210172
 H(K,K-1) = -S * X 87210173
 GO TO 190 87210174
 180 IF (L .NE. N) H(K,K-1) = -H(K,K-1) 87210175
 190 P = P + S 87210176
 X = P / S 87210177
 Y = G / S 87210178
 ZZ = R / S 87210179
 G = G / P 87210180

	R = R / P	87210181
C	:::::::::: ROW MODIFICATION ::::::::::::	87210182
	DC 210 J = K, N	87210183
	P = H(K,J) + C * H(K+1,J)	87210184
	IF (.NOT. NOTLAS) GO TO 200	87210185
	F = P + R * F(K+2,J)	87210186
	F(K+2,J) = H(K+2,J) - P * ZZ	87210187
200	F(K+1,J) = H(K+1,J) - P * Y	87210188
	F(K,J) = F(K,J) - P * X	87210189
210	CONTINUE	87210190
C	J = MIN0(EN,K+3)	87210191
C	:::::::::: COLUMN MODIFICATION ::::::::::::	87210192
	DC 220 I = 1, J	87210193
	P = X * F(I,K) + Y * F(I,K+1)	87210194
	IF (.NOT. NCLAS) GO TO 220	87210195
	P = P + ZZ * H(I,K+2)	87210196
	F(I,K+2) = H(I,K+2) - P * R	87210197
220	F(I,K+1) = F(I,K+1) - P * Q	87210198
	F(I,K) = F(I,K) - P	87210199
230	CONTINUE	87210200
C	:::::::::: ACCUMULATE TRANSFORMATIONS ::::::::::::	87210201
	DC 250 I = LCH, ICH	87210202
	P = X * Z(I,K) + Y * Z(I,K+1)	87210203
	IF (.NOT. NCLAS) GO TO 240	87210204
	P = P + ZZ * Z(I,K+2)	87210205
	Z(I,K+2) = Z(I,K+2) - P * R	87210206
240	Z(I,K+1) = Z(I,K+1) - P * C	87210207
	Z(I,K) = Z(I,K) - P	87210208
250	CONTINUE	87210209
C	260 CONTINUE	87210210
C	GC TC 70	87210211
C	:::::::::: ONE ROW FOUND ::::::::::::	87210212
270	H(EN,EN) = X + T	87210213
		87210214
		87210215
		87210216

WR(EN) = H(EN,EN) 87210217
 WI(EN) = C.CDC 87210218
 EN = NA 87210219
 GC TC 60 87210220
 C :::::::::: TWC RECTS FOUND :::::::::::: 87210221
 280 P = (Y - X) / 2.0DC 87210222
 G = P * P + W 87210223
 ZZ = DSQRT(DAPS(G)) 87210224
 H(EN,EN) = X + T 87210225
 X = H(EN,EN) 87210226
 H(NA,NA) = Y + T 87210227
 IF (G .LT. C.CCC) GC TC 320 87210228
 C :::::::::: REAL PAIR :::::::::::: 87210229
 ZZ = P + ESIGN(ZZ,P) 87210230
 WR(NA) = X + ZZ 87210231
 WR(EN) = WR(NA) 87210232
 IF (ZZ .NE. 0.CEO) WR(EN) = X - W / ZZ 87210233
 WI(NA) = C.CDC 87210234
 WI(EN) = C.CDC 87210235
 X = H(EN,NA) 87210236
 R = CSCRT(X*X+ZZ*ZZ) 87210237
 P = X / R 87210238
 Q = ZZ / R 87210239
 C :::::::::: ROW MODIFICATION :::::::::::: 87210240
 CC 290 J = NA, N 87210241
 ZZ = H(NA,J) 87210242
 H(NA,J) = Q * ZZ + P * H(EN,J) 87210243
 H(EN,J) = Q * H(EN,J) - P * ZZ 87210244
 290 CONTINUE 87210245
 C :::::::::: COLUMN MODIFICATION :::::::::::: 87210246
 DO 300 I = 1, EN 87210247
 ZZ = H(I,NA) 87210248
 H(I,NA) = C * ZZ + P * H(I,EN) 87210249
 H(I,EN) = C * H(I,EN) - P * ZZ 87210250
 300 CONTINUE 87210251
 C :::::::::: ACCUMULATE TRANSFORMATIONS :::::::::::: 87210252

DC 310 I = LCH, IGF 87210253
 ZZ = Z(I,NA) 87210254
 Z(I,NA) = C * ZZ + P * Z(I,EN) 87210255
 Z(I,EN) = C * Z(I,EN) - P * ZZ 87210256
 310 CONTINUE 87210257
 C 87210258
 GC TO 330 87210259
 C ::::::: COMPLEX PAIR :::::::
 320 WR(NA) = X + P 87210260
 WR(EN) = X + P 87210261
 WI(NA) = ZZ 87210262
 WI(EN) = -ZZ 87210263
 330 EN = ENM2 87210264
 GC TO 60 87210265
 C ::::::: ALL RCCTS FCUND. BACKSUBSTITUTE TO FIND 87210266
 C VECTCRS OF UPPER TRIANGULAR FCRM :::::::
 340 NORM = 0.000 87210267
 K = 1 87210268
 C 87210269
 CC 360 I = 1, N 87210270
 C 87210271
 C CC 350 J = K, N 87210272
 350 NORM = NORM + DARS(H(I,J)) 87210273
 C 87210274
 K = I 87210275
 360 CONTINUE 87210276
 C 87210277
 IF (NORM .EQ. C.CCC) GC TO 1001 87210278
 C ::::::: FOR EN=N STEP -1 UNTIL 1 CC -- :::::::
 DC 800 NN = 1, N 87210279
 EN = N + 1 - NN 87210280
 P = WR(EN) 87210281
 C = WI(EN) 87210282
 NA = EN - 1 87210283
 IF (I) 710, 600, 800 87210284
 C ::::::: REAL VECTCR ::::::: 87210285
 87210286
 87210287
 87210288

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600      N = EN                               87210289
        F(EN,EN) = 1.000                         87210290
        IF (NA .EQ. 0) GO TO 800                 87210291
C      ::::::::::::: FOR I=EN-1 STEP -1 UNTIL 1 DO -- ::::::::::::
        GO TO 700  II = 1, NA                   87210292
        I = EN - II                            87210293
        W = H(I,I) - P                         87210294
        R = H(I,EN)                            87210295
        IF (N .GT. NA) GO TO 620                 87210296
C
        DO 610  J = N, NA                   87210298
        R = R + F(I,J) * H(J,EN)                 87210299
C
        620      IF (WI(I) .GE. C.000) GO TO 630     87210300
        ZZ = W                               87210301
        S = R                               87210302
        GO TO 700
        630      N = I                           87210303
        IF (WI(I) .NE. C.000) GO TO 640     87210304
        T = W                               87210305
        IF (W .GE. C.000) T = MACHEP * NORM     87210306
        F(I,EN) = -R / T                     87210307
        GO TO 700
C      ::::::::::::: SOLVE REAL EQUATIONS ::::::::::::
        640      X = H(I,I+1)                   87210308
        Y = F(I+1,I)                         87210309
        G = (WR(I) - P) * (WP(I) - P) + WI(I) * WI(I) 87210310
        T = (X * S - ZZ * R) / G             87210311
        F(I,EN) = T                         87210312
        IF (DARS(X) .LE. DAPS(ZZ)) GO TO 650     87210313
        F(I+1,EN) = (-R - W * T) / X           87210314
        GO TO 700
        650      F(I+1,EN) = (-S - Y * T) / ZZ     87210315
        700      CONTINUE                         87210316
C      ::::::::::::: END REAL VECTOR ::::::::::::
        GO TO 800                               87210317

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C	::::::: COMPLEX VECTOR :::::::	87210325
710	N = NA	87210326
C	::::::: LAST VECTOR COMPONENT OF CSEN IMAGINARY SO THAT	87210327
C	EIGENVECTOR MATRIX IS TRIANGULAR :::::::	87210328
	IF (DAPS(H(EN,NA)) .LE. DAPS(H(NA,EN))) GO TO 720	87210329
	H(NA,NA) = C / H(EN,NA)	87210330
	H(NA,EN) = -(H(EN,EN) - P) / H(EN,NA)	87210331
	GO TO 730	87210332
720	Z3 = COMPLEX(C,CDC,-H(NA,EN)) / COMPLEX(H(NA,NA)-P,C)	87210333
	H(NA,NA) = T3(1)	87210334
	H(NA,EN) = T3(2)	87210335
730	H(EN,NA) = C.CDC	87210336
	H(EN,EN) = 1.CDC	87210337
	ENM2 = NA - 1	87210338
	IF (ENM2 .EQ. 0) GO TO 800	87210339
C		87210340
	GO 790 II = 1, ENM2	87210341
174	I = NA - II	87210342
	W = H(I,I) - P	87210343
	RA = C.CDC	87210344
	SA = H(I,EN)	87210345
C		87210346
	GO 760 J = N, NA	87210347
	RA = RA + H(I,J) * H(J,NA)	87210348
	SA = SA + H(I,J) * H(J,EN)	87210349
760	CONTINUE	87210350
C		87210351
	IF (WI(I) .GE. C.CDC) GO TO 770	87210352
	Z2 = W	87210353
	R = RA	87210354
	S = SA	87210355
	GO TO 790	87210356
770	N = I	87210357
	IF (WI(I) .NE. C.000) GO TO 780	87210358
	Z3 = COMPLEX(-RA,-SA) / COMPLEX(W,C)	87210359
	H(I,NA) = T3(1)	87210360

```

F(I,EN) = T3(2)
GO TO 790
C      :::::::::::: SOLVE COMPLEX EQUATIONS ::::::::::::
780      X = H(I,I+1)
      Y = H(I+1,I)
      VR = (WR(I) - P) * (WR(I) - P) + WI(I) * WI(I) - C * C
      VT = (WR(I) - P) * 2.000 * C
      IF (VR .GE. C.000 .AND. VI .GE. 0.000) VR = PACHEP * NORM
      X   * (DABS(W) + DABS(Q) + DABS(X) + DABS(Y) + DABS(Z))
      Z3 = DCMPLX(X*R-ZZ*RA+Q*SA,X*S-ZZ*SA-C*RA) / DCMPLX(VR,VI)
      H(I,NA) = T3(1)
      H(I,EN) = T3(2)
      IF (DABS(X) .LE. DABSIZE) + DABS(Q)) GO TO 785
      H(I+1,NA) = (-RA - W * H(I,NA) + C * H(I,EN)) / X
      H(I+1,EN) = (-SA - W * H(I,EN) - C * H(I,NA)) / X
      GO TO 790
785      Z3 = DCMPLX(-R-Y*H(I,NA),-S-Y*H(I,EN)) / DCMPLX(ZZ,Q)
      H(I+1,NA) = T3(1)
      H(I+1,EN) = T3(2)
790      CCNTINUE
C      :::::::::::: END COMPLEX VECTOR ::::::::::::
800      CONTINUE
C      :::::::::::: END BACK SUBSTITUTION.
C      :::::::::::: VECTORS OF ISOLATED ROOTS ::::::::::::
C      DO 840 I = 1, N
C          IF (I .GE. LCH .AND. I .LE. IGH) GO TO 840
C
C          DO 820 J = I, N
820      Z(I,J) = H(I,J)
C
C      840 CCNTINUE
C      :::::::::::: MULTIPLY BY TRANSFORMATION MATRIX TO GIVE
C      :::::::::::: VECTORS OF ORIGINAL FULL MATRIX.
C          FOR J=N STEP -1 UNTIL LCH DO -- ::::::::::::
C      DO 880 JJ = LCH, N
C          J = N + LCH - JJ

```

N = MIN(IJ,IEH)	87210397
C	87210398
DO EPC I = LCH, 16H	87210399
ZZ = 0.000	87210400
C	87210401
DO 860 K = LCH, N	87210402
860 ZZ = ZZ + Z(I,K) * H(K,J)	87210403
C	87210404
Z(I,J) = ZZ	87210405
880 CONTINUE	87210406
C	87210407
GC TO 1001	87210408
C ::::::::::: SET ERROR -- NO CONVERGENCE TO AN	87210409
C EIGENVALUE AFTER 30 ITERATIONS ::::::::::::	87210410
1000 IEPR = FN	87210411
1001 RETRN	87210412
C :::::::::::: LAST CARD OF HQR2 ::::::::::::	87210413
END	87210414

C 70210001
 C 70210002
 C 70210003
 C 70210004
 C 70210005
 C 70210006
 C 70210007
 C 70210008
 C 70210009
 C 70210010
 C 70210011
 C 70210012
 C 70210013
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 C 70210020
 C 70210021
 C 70210022
 C 70210023
 C 70210024
 C 70210025
 C 70210026
 C 70210027
 C 70210028
 C 70210029
 C 70210030
 C 70210031
 C 70210032
 C 70210033
 C 70210034
 C 70210035
 C 70210036

SUBROUTINE BALPAK(NM,N,LCW,IGH,SCALE,M,Z)
 INTEGER I,J,K,M,N,II,NM,IGH,LOW
 REAL*8 SCALE(N),Z(NM,N)
 REAL*8 S
 THIS SUBROUTINE IS A TRANSLATION OF THE ALGOL PROCEDURE BALBAK,
 NUM. MATH. 13, 293-304(1969) BY PARLETT AND REINSCH.
 HANDBOOK FOR ALGOL. COMP., VOL.II-LINEAR ALGEBRA, 315-326(1971).
 THIS SUBROUTINE FORMS THE EIGENVECTORS OF A REAL GENERAL
 MATRIX BY BACK TRANSFORMING THOSE OF THE CORRESPONDING
 BALANCED MATRIX DETERMINED BY BALANC.
 ON INPUT:
 NM MUST BE SET TO THE ROW DIMENSION OF TWO-DIMENSIONAL
 ARRAY PARAMETERS AS DECLARED IN THE CALLING PROGRAM
 DIMENSION STATEMENT;
 N IS THE ORDER OF THE MATRIX;
 LCW AND IGH ARE INTEGERS DETERMINED BY BALANC;
 SCALE CONTAINS INFORMATION DETERMINING THE PERMUTATIONS
 AND SCALING FACTORS USED BY BALANC;
 M IS THE NUMBER OF COLUMNS OF Z TO BE BACK TRANSFORMED;
 Z CONTAINS THE REAL AND IMAGINARY PARTS OF THE EIGEN-
 VECTORS TO BE BACK TRANSFORMED IN ITS FIRST M COLUMNS.
 ON OUTPUT:

```

C          Z CONTAINS THE REAL AND IMAGINARY PARTS OF THE          7C210037
C          TRANSFORMED EIGENVECTORS IN ITS FIRST N COLUMNS.          7C210038
C          QUESTIONS AND COMMENTS SHOULD BE DIRECTED TO B. S. GARBOW, 7C210039
C          APPLIED MATHEMATICS DIVISION, ARGONNE NATIONAL LABORATORY 7C210040
C          -----
C          IF (IGH .EQ. LCH) GO TO 120 7C210041
C          DO 110 I = LOW, IGH 7C210042
C          S = SCALE(I) 7C210043
C          :::::::::::: LEFT HAND EIGENVECTORS ARE BACK TRANSFORMED 7C210044
C          :::::::::::: IF THE FOLLOWING STATEMENT IS REPLACED BY 7C210045
C          :::::::::::: S=1.0DC/SCALE(I). :::::::::::: 7C210046
C          DO 100 J = 1, N 7C210047
C          100    Z(I,J) = Z(I,J) * S 7C210048
C          110 CONTINUE 7C210049
C          :::::::::::: FOR I=LOW-1 STEP -1 UNTIL 1, 7C210050
C          :::::::::::: IGH+1 STEP 1 UNTIL N DO -- :::::::::::: 7C210051
C          120 DO 140 II = 1, N 7C210052
C          I = II 7C210053
C          IF (I .GE. LCH .AND. I .LE. IGH) GO TO 140 7C210054
C          IF (I .LT. LCH) I = LCH - II 7C210055
C          K = SCALE(I) 7C210056
C          IF (K .EQ. 1) GO TO 140 7C210057
C
C          DO 130 J = 1, N 7C210058
C          S = Z(I,J) 7C210059
C          Z(I,J) = Z(K,J) 7C210060
C          Z(K,J) = S 7C210061
C          130 CONTINUE 7C210062
C          140 CONTINUE 7C210063

```

C

RETURN

C

::::::: LAST CARE OF BALBAK :::::::

END

7021C073

7021C074

7021C075

7021C076

179

SUBROUTINE MINV

FURFCSE
INVERT A MATRIX

USAGE
CALL MINV(A,N,D,L,M)

DESCRIPTION OF PARAMETERS
A - INPUT MATRIX, DESTROYED IN COMPUTATION AND REPLACED BY
RESULTANT INVERSE.
N - CFDER OF MATRIX A
D - RESULTANT DETERMINANT
L - WORK VECTOR OF LENGTH N
M - WORK VECTOR OF LENGTH N

REMARKS
MATRIX A MUST BE A GENERAL MATRIX

SUBROUTINES AND FUNCTION SUBPROGRAMS REQUIRED
NONE

METHOD
THE STANDARD GAUSS-JORDAN METHOD IS USED. THE DETERMINANT
IS ALSO CALCULATED. A DETERMINANT OF ZERO INDICATES THAT
THE MATRIX IS SINGULAR.

ROUTINE MINV(A,N,D,L,M)

MENSION A(1),L(1),M(1)

MINV 30
MINV 40
MINV 50
MINV 60
MINV 70
MINV 80
MINV 90
MINV 100
MINV 110
MINV 120
MINV 130
MINV 140
MINV 150
MINV 160
MINV 170
MINV 180
MINV 190
MINV 200
MINV 210
MINV 220
MINV 230
MINV 240
MINV 250
MINV 260
MINV 270
MINV 280
MINV 290
MINV 300
MINV 310
MINV 320
MINV 330
MINV 340
MINV 350
MINV 360

C
C IF A DOUBLE PRECISION VERSION OF THIS ROUTINE IS DESIRED, THE
C IN COLUMN 1 SHOULD BE REMOVED FROM THE DOUBLE PRECISION
C STATEMENT WHICH FOLLOWS.
C

C DOUBLE PRECISION A,D,BIGA,HOLD
C

C THE C MUST ALSO BE REMOVED FROM DOUBLE PRECISION STATEMENTS
C APPEARING IN OTHER ROUTINES USED IN CONJUNCTION WITH THIS
C ROUTINE.
C

C THE DOUBLE PRECISION VERSION OF THIS SUBROUTINE MUST ALSO
C CONTAIN DOUBLE PRECISION FORTRAN FUNCTIONS. ABS IN STATEMENT
C 10 MUST BE CHANGED TO DABS.
C

C SEARCH FOR LARGEST ELEMENT
C

D=1.0
NK=-N
DO 80 K=1,N
NK=NK+N
L(K)=K
M(K)=K
KK=NK+K
BIGA=A(KK)
DO 20 J=K,N
IZ=N*(J-1)
DO 20 I=K,N
IJ=IZ+I
10 IF(ABS(BIGA)- ABS(A(IJ))) 15,20,20
15 BIGA=A(IJ)
L(K)=I
M(K)=J
20 CONTINUE
C
C MINV 370
C MINV 380
C MINV 390
C MINV 400
C MINV 410
C MINV 420
C MINV 430
C MINV 440
C MINV 450
C MINV 460
C MINV 470
C MINV 480
C MINV 490
C MINV 500
C MINV 510
C MINV 520
C MINV 530
C MINV 540
C MINV 550
C MINV 560
C MINV 570
C MINV 580
C MINV 590
C MINV 600
C MINV 610
C MINV 620
C MINV 630
C MINV 640
C MINV 650
C MINV 660
C MINV 670
C MINV 680
C MINV 690
C MINV 700
C MINV 710
C MINV 720

```

C
C           INTERCHANGE ROWS
C
J=L(K)
IF(J-K) 35,35,25
25 KI=K-N
DO 30 I=1,N
KI=KI+N
HOLD=-A(KI)
JI=KI-K+J
A(KI)=A(JI)
30 A(JI)=HOLD

C
C           INTERCHANGE COLUMNS
C
35 I=M(K)
IF(I-K) 45,45,38
38 JP=N*(I-1)
DO 40 J=1,N
JK=NK+J
JI=JP+J
HOLD=-A(JK)
A(JK)=A(JI)
40 A(JI)=HOLD

C
C           DIVIDE COLUMN BY MINUS PIVOT (VALUE OF PIVOT ELEMENT IS
C           CONTAINED IN BIGA)
C
45 IF(BIGA) 48,46,48
46 D=0.0
RETURN
48 DO 55 I=1,N
IF(I-K) 50,55,50
50 IK=NK+I
A(IK)=A(IK)/(-BIGA)
55 CONTINUE

```

MINV 730
MINV 740
MINV 750
MINV 760
MINV 770
MINV 780
MINV 790
MINV 800
MINV 810
MINV 820
MINV 830
MINV 840
MINV 850
MINV 860
MINV 870
MINV 880
MINV 890
MINV 900
MINV 910
MINV 920
MINV 930
MINV 940
MINV 950
MINV 960
MINV 970
MINV 980
MINV 990
MINV1000
MINV1010
MINV1020
MINV1030
MINV1040
MINV1050
MINV1060
MINV1070
MINV1080

```

C
C          REDUCE MATRIX
C
C      DO 65 I=1,N
C      IK=NK+I
C      HCDE=A(IK)
C      IJ=I-N
C      DO 65 J=1,N
C      IJ=IJ+N
C      IF(I-K) 60,65,60
C 60  IF(J-K) 62,65,62
C 62  KJ=IJ-I+K
C      A(IJ)=HCDE+A(KJ)+A(IJ)
C 65  CONTINUE
C
C          DIVIDE ROW BY PIVOT
C
C      KJ=K-N
C      DC 75 J=1,N
C      KJ=KJ+N
C      IF(J-K) 70,75,70
C 70  A(KJ)=A(KJ)/BIGA
C 75  CONTINUE
C
C          PRODUCT OF PIVOTS
C
C      D=D*BIGA
C
C          REPLACE PIVOT BY RECIPROCAL
C
C      A(KK)=1.0/BIGA
C 30  CONTINUE
C
C          FINAL ROW AND COLUMN INTERCHANGE
C
C      K=N
C
C          MINV1090
C          MINV1100
C          MINV1110
C          MINV1120
C          MINV1130
C          MINV1140
C          MINV1150
C          MINV1160
C          MINV1170
C          MINV1180
C          MINV1190
C          MINV1200
C          MINV1210
C          MINV1220
C          MINV1230
C          MINV1240
C          MINV1250
C          MINV1260
C          MINV1270
C          MINV1280
C          MINV1290
C          MINV1300
C          MINV1310
C          MINV1320
C          MINV1330
C          MINV1340
C          MINV1350
C          MINV1360
C          MINV1370
C          MINV1380
C          MINV1390
C          MINV1400
C          MINV1410
C          MINV1420
C          MINV1430
C          MINV1440

```

100 K=(Y-1)	MINV1450
IF(K) 150,150,105	MINV1460
105 I=L(K)	MINV1470
IF(I-K) 120,120,108	MINV1480
108 JQ=N*(K-1)	MINV1490
JR=N*(I-L)	MINV1500
DO 110 J=1,N	MINV1510
JK=JQ+J	MINV1520
HOLD=A(JK)	MINV1530
JI=JR+J	MINV1540
A(JK)=-A(JI)	MINV1550
110 A(JI) =HOLD	MINV1560
120 J=N(K)	MINV1570
IF(J-K) 100,100,125	MINV1580
125 KI=K-N	MINV1590
DO 130 I=1,N	MINV1600
KI=KI+N	MINV1610
HOLD=A(KI)	MINV1620
JI=KI-K+J	MINV1630
A(KI)=-A(JI)	MINV1640
130 A(JI) =HOLD	MINV1650
GC TO 100	MINV1660
150 RETURN	MINV1670
END	MINV1680

APPENDIX B

INPUT DATA AND OUTPUT LISTING OF THE SAMPLE PROBLEMS

B.1 Application of the FREEVI Program to the Wing

B.1.1 Input Data Listing for the Bell Wing

The FREEVI program input data for the wing are illustrated in this section. The structural data are shown in Fig. 6 and in Table 3.

RELL WING

1							8/17/74	DATA0001
2							TCASE	DATA0012
0							TPUNCH	DATA0003
9	20	6					IGUEST	DATA0004
0.001							NET,NTTP,M	DATA0005
0.0							ERR	DATA0006
0.5							DMFG	DATA0007
0.0							RAMDA	DATA0008
0.0	0.0						COL	DATA0009
0.0							SPKB,SPKC	DATA0010
9202.9	E62653.0	E62653.0	E62653.0	E62653.0	E62653.0	E6	ALPHAH	DATA0011
2653.0	E62653.0	E62653.0	E62653.0	E62653.0	E6			DATA0012
18794.0	E610410.0	E610410.0	E610410.0	E610410.0	E610410.0	E6		DATA0013
10410.0	E610410.0	E610410.0	E610410.0	E610410.0	E6			DATA0014
0.0	0.0	0.0	0.0	0.0	0.0			DATA0015
0.0								DATA0016
0.0								DATA0017
0.00705	0.00705	0.00488	0.00488	0.00488	0.00488	0.00508	0.03248	DATA0018
0.00001								DATA0019
41.0	21.0	21.0	21.0	21.0	21.0	21.0	18.4	DATA0020
14.6								DATA0021
4.71	4288.8	6591.6	6570.0	53.076				DATA0022
16868.0	E62696.0	E62696.0	E62696.0	E62696.0	E62696.0	E6		DATA0023
2696.0	E62696.0	E62696.0	E62696.0	E62696.0	E6			DATA0024
0.389	E00.389	E00.389	E00.389	E00.389	E00.389	E0		DATA0025
0.389	E00.389	E00.389	E00.389	E00.389	E0			DATA0026
0.0	E00.0	E00.0	E00.0	E00.0	E00.0	E0		DATA0027
0.0	E00.0	E00.0	E00.0	E00.0	E00.0	E0		DATA0028

B.1.2 The FEEVI program output data for the Bell Wing. The example output of the Bell wing is shown in this subsection.

WING

BELL WING

8/17/74

* * *
INPUT DATA

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

IPUNCH=0 IGMEST=0
 NO OF DEGRE PER NODE= 6
 NO OF ELEMENTS= 9
 NO OF MAX ITER ALLOEWD= 20
 NO OF MODES= 6
 ERR= 0.00100
 OMEG= 0.0
 LAMRDA= 0.0
 COLLECTIVE PITCH= 0.0
 SPRING= 0.0 0.0
 ALPHAH= 0.0

--FLAPPING BENDING STIFFNESS--

0.9202901E+10	0.2653000E+10	0.2653000E+10	0.2653000E+10	0.2653000E+10	0.2653000E+10	0.2653000E+10
0.2653000E+10	0.2653000E+10					

--CHORDWISE BENDING STIFFNESS--

0.1879400E+11	0.1041000E+11	0.1041000E+11	0.1041000E+11	0.1041000E+11	0.1041000E+11	0.1041000E+11
0.1041000E+11	0.1041000E+11					

--ANGLE OF TWIST--

0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0						

--MASS DISTRIBUTION--

0.00705	0.00705	0.00488	0.00488	0.00488	0.00488	0.00488
0.00E+1						

--ELEMENT SIZE--

41.60000	21.00000	21.00000	21.00000	21.00000	21.00000	21.00000
14.60000						

TIP MASS	ROLL INERTIA	YAW INERTIA	PITCH INERTIA	MASS COUPLING
4.71000	4288.80078	6591.60156	6570.00000	53.07600

--TORSIONAL RIGIDITY--

0.1696800E+11	0.2696000E+10	0.2696000E+10	0.2696000E+10	0.2696000E+10	0.2696000E+10	0.2696000E+10
0.2696000E+10	0.2696000E+10					

--MOMENT OF INERTIA--

0.3890000E+00	0.3890000E+00	0.3891000E+00	0.3891100E+00	0.3891110E+00	0.3892000E+00	0.3892100E+00
0.3890000E+00	0.3890000E+00					

--MASS COUPLING ALONG SPAN--

1.0	0.7	0.0	0.0	0.0	0.0	0.0
0.5	0.0					

TENSION DUE TO CENTRIF FORCE

0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0						

MASS = 0.62615E+01

MOMENT OF INERTIA AT ROOT= 0.21483E+06

TOTAL LENGTH OF THE BEAM= 0.20000E+03

MAX. SIZE OF STF IS 484 SPECTIFIED SIZE IS 654

NO. OF NEGATIVE DIAGS.= 0 FACT. COMPLETED

EIGENVALUES=

0.28091D+03 0.89998D+03 0.16245D+05 0.34651D+05 0.26504D+06 0.53303D+06

EIGENVALUES=

0.27768D+03 0.89084D+03 0.27303D+04 0.12970D+05 0.37610D+05 0.27656D+06

EIGENVALUES=

0.27768D+03 0.89084D+03 0.27300D+04 0.12968D+05 0.32494D+05 0.26217D+06

EIGENVALUES=

0.27768D+03 0.89084D+03 0.27300D+04 0.12968D+05 0.32494D+05 0.26097D+06

EIGENVALUES=

0.27768D+03 0.89084D+03 0.27300D+04 0.12968D+05 0.32494D+05 0.26086D+06

RADIAN/SFC

0.16664D+02 0.29847D+02 0.52250D+02 0.11388D+03 0.18026D+03 0.51074D+03

HERTZ

0.26521D+01 0.47503D+01 0.83158D+01 0.18124D+02 0.28689D+02 0.81287D+02

NO. OF ITERATION= 5 CONVERGED WITHIN 0.10000D-02

REDUCED MASS MATRIX

0.10000D+01							
0.11699D-22	0.10000D+01						
-0.51511D-20	-0.33025D-21	0.10000D+01					
-0.11609D-19	-0.13470D-17	-0.92236D-19	0.10000D+01				
0.88490D-24	-0.13376D-20	0.12102D-18	0.10999D-19	0.10000D+01			
-0.51707D-20	0.76081D-20	0.13915D-17	0.86677D-18	-0.20838D-19	0.10000D+01		

REDUCED STIF MATRIX

0.27768D+03							
0.12056D-18	0.89084D+03						
-0.59669D-13	0.38420D-17	0.27300D+04					
-0.36503D-17	-0.11888D-16	0.93751D-16	0.12968D+05				
-0.27794D-16	0.63537D-13	-0.98995D-18	-0.58898D-14	0.32494D+05			
-0.44715D-16	-0.12874D-12	-0.11159D-15	-0.89091D-14	0.16965D-15	0.26086D+06		

**** WING MODE SHAPES ****

I= 1

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PH(I,J)	DPH(I,J)
1	0.0	0.0	0.0	0.0	0.0	0.4732115E-16
2	0.1096412E-01	-0.4118297E-09	0.5154577E-03	-0.1607661E-10	0.1781619E-14	0.5296245E-15
3	0.2995049E-01	-0.7596179E-09	0.1275148E-02	-0.1562293E-10	0.6824774E-14	0.225357E-15
4	0.5378090E-01	-0.1020656E-08	0.1929206E-02	-0.8398275E-11	0.1221887E-13	0.2528330E-15
5	0.1102392E+00	-0.1089811E-08	0.2477859E-02	0.2030671E-11	0.1765127E-13	0.2587192E-15
6	0.1671160E+00	-0.9396308E-09	0.2921520E-02	0.1186243E-10	0.2311340E-13	0.2595412E-05
7	0.2322127E+00	-0.6202676E-09	0.3260845E-02	0.1763036E-10	0.2855684E-13	0.2566636E-15
8	0.3033477E+00	-0.2455758E-09	0.3496786E-02	0.1680664E-10	0.3421046E-13	0.259617E-15
9	0.3689417E+00	0.5387467E-11	0.3620509E-02	0.9286009E-11	0.3978768E-13	0.2596392E-15
10	0.4221950E+00	0.6504591E-10	0.3666978E-02	-0.1889718E-11	0.4257825E-13	0.2526161E-05

I= 2

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PH(I,J)	DPH(I,J)
1	0.0	0.0	0.0	0.0	0.0	0.1334282E-13
2	-0.1165887E-08	0.1734024E-01	-0.4099619E-10	0.8156588E-03	0.4967241E-12	0.1503261E-13
3	-0.1780436E-08	0.4120878E-01	-0.1078385E-10	0.1443248E-02	0.1793459E-11	0.5271469E-13
4	-0.1508654E-08	0.7735723E-01	0.3577688E-10	0.1985208E-02	0.2899238E-11	0.4211952E-13
5	-0.4287495E-09	0.1239857E+00	0.6140244E-10	0.2441776E-02	0.3564264E-11	0.1911476E-13
6	0.7976879E-09	0.1793168E+00	0.4901710E-10	0.2813344E-02	0.3702648E-11	0.54942711E-14
7	0.1419738E-08	0.2415592E+00	0.7250959E-11	0.3100497E-02	0.3337820E-11	0.2797991E-13
8	0.1085335E-08	0.3089125E+00	-0.3688012E-10	0.3304057E-02	0.2568991E-11	0.4423885E-13
9	0.2516420E-09	0.3708636E+00	-0.4400065E-10	0.3415339E-02	0.1653754E-11	0.5336117E-13
10	-0.1154645E-09	0.4211117E+00	0.2109291E-11	0.3461931E-02	0.8527415E-12	0.5725261E-13

I= 3

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PH(I,J)	DPH(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.1626321E-14
2	0.3132011E-02	0.1067552E-05	0.1493440E-03	0.4164287E-07	-0.5369098E-03	-0.1776540E-14
3	0.8682542E-02	0.1967319E-05	0.3762855E-03	0.4036162E-07	-0.2056599E-02	-0.4788566E-14
4	0.1876992E-01	0.2640408E-05	0.5815080E-03	0.2158016E-07	-0.3678715E-12	-0.7646311E-14
5	0.3290243E-01	0.2815990E-05	0.7615838E-03	-0.5406847E-08	-0.5317826E-12	-0.7790148E-14
6	0.5060757E-01	0.2425011E-05	0.9210168E-03	-0.3075634E-07	-0.6959036E-12	-0.7810385E-14
7	0.7144558E-01	0.1548726E-05	0.1060446E-02	-0.4554926E-07	-0.8599557E-12	-0.7903290E-14
8	0.9502667E-01	0.6317913E-06	0.1182823E-02	-0.4332351E-07	-0.1023867E-11	-0.7911231E-14
9	0.1177033E+00	-0.1453627E-07	0.1282109E-02	-0.2388719E-17	-0.1167341E-11	-0.7793421E-14
10	0.1370279E+00	-0.1678002E-06	0.1366351E-02	0.4879347E-08	-0.1281075E-01	-0.7786400E-04

I = 4

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.8124932E-16
2	0.5561896E-01	0.1292796E-04	0.2441053E-02	0.5067096E-06	-0.3020681E-14	-0.5993528E-06
3	0.1320716E+00	0.2396124E-04	0.4596125E-02	0.4992368E-06	-0.1156774E-13	-0.3716693E-15
4	0.2385222E+00	0.3238695E-04	0.5303770E-02	0.2753594E-06	-0.2068353E-13	-0.4294215E-15
5	0.3449906E+00	0.3479325E-04	0.4606590E-02	-0.5469537E-07	-0.2988146E-13	-0.4367310E-15
6	0.4226109E+00	0.3018290E-04	0.2568961E-02	-0.3721357E-06	-0.3907180E-13	-0.436317E-15
7	0.4440947E+00	0.2005251E-04	-0.7243240E-03	-0.5633744E-06	-0.4823287E-13	-0.4353352E-15
8	0.3840748E+00	0.8010285E-05	-0.5176779E-02	-0.5431261E-06	-0.5735478E-13	-0.433373E-05
9	0.2462974E+00	-0.1363861E-06	-0.9906098E-02	-0.3031313E-06	-0.6537981E-13	-0.431248E-05
10	0.7180148E-01	-0.2095530E-05	-0.1494954E-01	0.6366438E-07	-0.7159102E-13	-0.4293397E-05

I = 5

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.1459670E-17
2	0.2360992E-05	0.6912452E-01	0.8368607E-07	0.2999669E-02	-0.5442764E-09	-0.1754413E-16
3	0.3658430E-05	0.1467586E+00	0.2591068E-07	0.4220549E-02	-0.1985294E-08	-0.5971562E-17
4	0.3202141E-05	0.2391851E+00	-0.6824558E-07	0.4412588E-02	-0.3275932E-08	-0.5190257E-10
5	0.1072496E-05	0.3250826E+00	-0.1235147E-06	0.3604392E-02	-0.4168427E-08	-0.3156966E-10
6	-0.1439231E-05	0.3838446E+01	-0.1026097E-06	0.18335852E-02	-0.4545821E-08	-0.4846510E-11
7	-0.2793039E-05	0.3958154E+01	-0.1964723E-07	-0.8429433E-03	-0.4376279E-08	0.2069658E-10
8	-0.2200011E-05	0.3424572E+00	0.7231574E-07	-0.4376560E-02	-0.3722741E-08	0.4262971E-11
9	-0.5198935E-06	0.2284233E+00	0.9011211E-07	-0.8104231E-02	-0.2779422E-08	0.5684496E-10
10	0.2345656E-06	0.8644497E-01	-0.4498673E-08	-0.1138999E-01	-0.1892494E-08	0.6401313E-11

I = 6

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)	PHI(I,J)	DPHI(I,J)
1	0.0	0.0	0.0	0.0	0.0	-0.149331E-16
2	0.4376729E+00	-0.2575393E-02	0.1791070E-01	-0.1012992E-03	0.4125577E-14	0.1326111E-15
3	0.9022505E+00	-0.4794151E-02	0.2376941E-01	-0.1011486E-03	0.1537770E-13	0.4927642E-15
4	0.1344618E+01	-0.6516449E-02	0.1658912E-01	-0.5735150E-04	0.2711348E-13	0.5473314E-15
5	0.1544214E+01	-0.7044562E-02	0.1633530E-02	0.8475477E-05	0.386510E-13	0.525627E-15
6	0.1403761E+01	-0.6153475E-02	-0.1466982E-01	0.7372542E-04	0.4943394E-13	0.4498302E-15
7	0.9648077E+00	-0.4121412E-02	-0.2577179E-01	0.1139852E-03	0.5955135E-13	0.4572572E-15
8	0.3952152E+01	-0.1666956E-02	-0.2635399E-01	0.1115181E-03	0.6863751E-13	0.4292114E-15
9	-0.6146904E-02	0.1676549E-04	-0.1504268E-01	0.6317307E-04	0.7567221E-13	0.3167004E-15
10	-0.2912896E-01	0.4287334E-03	0.3793123E-02	-0.1231682E-14	0.8157512E-13	0.311448E-15

B.2 Application of the FREEVI Program to the Blade

B.2.1 The FREEVI Program Input Data Listing for the Boeing Rotor (Hingeless Rotor)

The input data deck setup is illustrated
in this subsection for the hingeless
rotor. Structural data are shown in Fig. 7.

BOEING BLADE FOR POWERED FLIGHT --- CLAMPED & CLAMPED B.C. 8/18/74 DATA0001
 2 ICASE DATA0002
 1 IPUNCH DATA0003
 0 IQUEST DATA0004
 10 NET,NTTR,M DATA0005
 0.001 ERR DATA0006
 -40.422 OMFG DATA0007
 -0.7 RANDA DATA0008
 0.017453 COL DATA0009
 0.0 SPKR,SPKC DATA0010
 8525.0 ALPHAH DATA0011
 106.0 E619.0 E68.5 E67.5 E65.5 E6 DATA0012
 5.0 E64.5 E64.5 E64.5 E64.0 E6 DATA0013
 110.0 E640.0 E640.0 E6200.0 E6500.0 E6 DATA0014
 520.0 E6510.0 E6515.0 E6530.0 E6535.0 E6 DATA0015
 0.6981 0.4712 0.3403 0.2531 0.1833 0.1222 0.0611 0.0 DATA0016
 -0.0611 -0.1134 DATA0017
 0.016583 0.001036 0.000777 0.000906530.001036 0.001036 0.001036 0.0012303 DATA0018
 0.0012303 0.001036 DATA0019
 15.6 15.6 15.6 15.6 15.6 15.6 15.6 15.6 DATA0020
 15.6 15.6 DATA0021
 0.0106064 DATA0022

**B.2.2 The FREEVI Program Output Data for
the Boeing Blade**

**The example output of the Boeing
blade is shown in this subsection.**

BLADE BEAM*CANTI CHORD*CANTI

ROFING BLADE FOR POWERED FLIGHT --- CLAMPED & CLAMPED B.C.

8/19/74

INPUT DATA

IPUNCH=1 IQUEST=0
 NO OF DEGRE PER NODE= 4
 NO OF ELEMENTS= 10
 NO OF MAX ITER ALLOWED= 20
 NO OF MODES= 4
 ERR= 0.00100
 OMEG= -40.42200

LAMBDA= -0.70000

COLLECTIVE PITCH= 0.01745

SPRING= 0.0 0.0

ALPHAH= 0.85250D+04

--FLAPPING BENDING STIFFNESS--

0.1060000E+09	0.1900000E+03	0.8500000E+07	0.7500000E+17	0.5500000E+07	0.5000000E+07	0.4500000E+17
0.4500000E+07	0.4500000E+07	0.4000000E+07				

--CHORDWISE BENDING STIFFNESS--

0.1100000E+09	0.4000000E+03	0.4000000E+08	0.2000000E+09	0.5000000E+09	0.5200000E+09	0.5100000E+09
0.5150001E+09	0.5304001E+09	0.5350001E+09				

--ANGLE OF TWIST--

0.69810	0.47120	0.34030	0.25310	0.18330	0.12220	0.06110	0.0
-0.06110	-0.11340						

--MASS DISTRIBUTION--

0.01658	0.00104	0.00078	0.00091	0.00104	0.00104	0.00104	0.00104
0.00123	0.00104						

--ELEMENT SIZE--

15.60000	15.60000	15.60000	15.60000	15.60000	15.60000	15.60000	15.60000
15.60000	15.60000						

TIP MASS	ROLL INERTIA	YAW INERTIA	PITCH INERTIA	MASS COUPLING			
0.01061	0.0	0.0	0.0	0.0			

TENSION DUE TO CENTRIF FORCE

27190.4219	2393.4883	23275.5703	22503.1680	21241.5352	19387.7656	17122.0469	14444.1789
10775.3986	6617.02734	2703.50903					

MASS = 0.41476E+00

MOMENT OF INERTIA AT ROOT= 0.16714E+04

TOTAL LENGTH OF THE BEAM= 0.15600E+03

MAX. SIZE OF STF IS 244 SPECIFIED SIZE IS 324

NO. OF NEGATIVE DIAGS.= 0 FACT. COMPLETED

EIGENVALUES=

0.208800+04 0.129500+05 0.273690+05 0.420530+06

EIGENVALUES=

0.111800+04 0.288400+04 0.190050+05 0.972430+15

EIGENVALUES=

0.111720+04 0.285200+04 0.181870+05 0.755500+05

EIGENVALUES=

0.111720+04 0.285190+04 0.181860+05 0.749790+05

EIGENVALUES=

0.111720+04 0.285190+04 0.181860+05 0.749340+05

RADIAN/SEC

0.334240+02 0.534030+02 0.137430+03 0.273740+03

HERTZ

0.531970+01 0.849930+01 0.218720+02 0.435670+02

NO. OF ITERATION= 5 CONVERGED WITHIN 0.100000E-02

REDUCED MASS MATRIX

0.100000+01

0.923460-19 0.100000+01

0.216820-16 0.543580-20 0.100000+01

0.927090-20 -0.196790-21 -0.121490-19 0.100000+01

165

REDUCED STIF MATRIX

0.964220+04

0.591760-14 0.113770+05

-0.773290-15 0.452090-16 0.274110+05

0.999970-15 -0.515870-16 0.302540-14 0.834590+05

**** BLADE MODE SHAPES ****

I= 1

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	-0.3071345E-02	0.3320938E-01	-0.4138651E-03	0.3757305E-02
3	-0.4010361E-02	0.1970022E+00	0.3891176E-04	0.1585099E-01
4	0.1771531E-01	0.5429144E+00	0.2249592E-02	0.2720761E-01
5	0.7252330E-01	0.1007425E+01	0.4471347E-02	0.3180430E-01
6	0.1537749E+00	0.1521890E+01	0.5777858E-02	0.3390279E-01
7	0.2471325E+00	0.2056107E+01	0.6131638E-02	0.3400152E-01
8	0.3411351E+00	0.2593284E+01	0.5890395E-02	0.3432557E-01
9	0.4277322E+00	0.3123945E+01	0.5184587E-02	0.3367477E-01
10	0.5013666E+00	0.3643093E+01	0.4255518E-02	0.3287940E-01
11	0.5611690E+00	0.4150885E+01	0.3513225E-02	0.3230092E-01

t = 2

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	0.4854569E-01	-0.1528439E-01	0.5902052E-02	-0.1984358E-02
3	0.2357861E+00	-0.7704520E-01	0.1740308E-01	-0.6000815E-02
4	0.5839912E+00	-0.1807868E+00	0.2659480E-01	-0.7669512E-02
5	0.1021941E+01	-0.2842678E+00	0.2921298E-01	-0.6042498E-02
6	0.1496003E+01	-0.3587406E+00	0.3124226E-01	-0.3021565E-02
7	0.199373E+01	-0.4039884E+00	0.3303983E-01	-0.2163647E-02
8	0.2529638E+01	-0.4239655E+00	0.3474081E-01	-0.5953177E-03
9	0.3083344E+01	-0.4232069E+00	0.3608362E-01	0.5515825E-03
10	0.3653433E+01	-0.4189971E+00	0.3684258E-01	0.1142329E-12
11	0.4229228E+01	-0.3904818E+00	0.3681487E-01	0.1111808E-02

t = 3

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	-0.7415771E-01	-0.6834286E-01	-0.8815017E-02	-0.7958513E-02
3	-0.3768928E+00	-0.4091305E+00	-0.2786428E-01	-0.3210701E-01
4	-0.9542273E+00	-0.1096154E+01	-0.4312693E-01	-0.5081352E-01
5	-0.1634645E+01	-0.1890661E+01	-0.4194136E-01	-0.4759142E-01
6	-0.2171334E+01	-0.2465169E+01	-0.2497231E-01	-0.2328279E-01
7	-0.2331151E+01	-0.2544001E+01	0.5753405E-02	0.1486159E-01
8	-0.1917689E+01	-0.1956378E+01	0.4791136E-01	0.6118271E-01
9	-0.8257181E+00	-0.6669863E+00	0.7105462E-01	0.1031131E+00
10	0.8585268E+00	0.1168359E+01	0.1214661E+00	0.1292541E+00
11	0.2855342E+01	0.3263458E+01	0.1307493E+00	0.1361399E+12

t = 4

K	W(I,J)	V(I,J)	DW(I,J)	DV(I,J)
1	0.0	0.0	0.0	0.0
2	0.5017383E-01	0.2488598E+01	0.6019762E-12	0.2334812E-11
3	0.3397898E+00	0.1251101E+01	0.2845969E-01	0.8702511E-01
4	0.9262698E+00	0.2709785E+01	0.4080152E-01	0.8272529E-01
5	0.1313488E+01	0.3515694E+01	0.4193374E-02	0.1249554E-01
6	0.9240110E+00	0.2393393E+01	-0.6620163E-01	-0.9232397E-11
7	-0.5951878E+00	0.9211577E+01	-0.1073177E+00	-0.1433128E+01
8	-0.2063768E+01	-0.1215673E+01	-0.6792390E-01	-0.1107412E+10
9	-0.2215355E+01	-0.2093110E+01	0.5533581E-01	0.513751E-02
10	-0.7487896E+00	-0.1783831E+01	0.1872610E+00	0.1108711E+01
11	0.3242649E+01	0.1165699E+01	0.2390831E+00	0.1555464E+00

B.3 The TILDYN Program Examples

B.3.1 Input Data Listing for the TILDYN Program

In this subsection, the sample problem data deck setup is illustrated. The flight condition is powered flight for the Boeing model and autorotation flight for the Bell model. The data for the computation is shown in Table 3 in detail.

BOEING ROTOR --POWERED FLT-- SDF, U-GUST,FREQ RES & EIGEN ANALYSIS

8/20/74 DATA0001

ITYPE DATA0002

IFLT DATA0003

DOF DATA0004

FREQRE DATA0005

IFRMAG DATA0006

IEIGEN DATA0007

DATA0008

DATA0009

DATA0010

DATA0011

DATA0012

DATA0013

DATA0014

DATA0015

DATA0016

DATA0017

DATA0018

DATA0019

DATA0020

DATA0021

DATA0022

DATA0023

DATA0024

DATA0025

DATA0026

DATA0027

DATA0028

DATA0029

DATA0030

DATA0031

DATA0032

DATA0033

DATA0034

DATA0035

DATA0036

1	2	3	4	5	6	7	8	9
1.1468	E-7-40.422	-0.7	4414.082					
156.0	1800.0	18.0496	5.7	0.0065	55.224			
200.5	62.18	5.7	0.004	-0.05	0.0	0.01	0.031	
1.0	0.0	0.0	0.0	0.0	0.0			U GUST
1117.2	2851.9	1EEE6.0	74927.0					
217.68	656.97	2002.2	5988.4	25466.0	253710.0			
9								
0.205	0.105	0.105	0.105	0.105	0.105	0.105	0.092	
0.073								
0.0	0.968E4E-02	0.264E0E-01	0.56422E-01	0.97570E-01	0.14798E+00			
0.20573E+00	0.268E5E+00	0.32718E+00	0.37453E+00					
0.0	-0.19216E-05	-0.35535E-09	-0.47546E-09	-0.51490E-09	-0.44798E-09			
-0.30091E-09	-0.12576E-09	-0.61370E-11	0.24547E-10					
0.0	0.455E1E-03	0.11282E-02	0.17080E-02	0.21954E-02	0.25905E-02			
0.28939E-02	0.21061E-02	0.32185E-02	0.32613E-02					
0.0	-0.75167E-11	-0.73673E-11	-0.40539E-11	0.78800E-12	0.54042E-11			
0.081805E-11	0.19227E-11	0.45167E-11	0.68893E-12					
0.0	0.12465E-04	0.41748E-04	0.85418E-04	0.12350E-03	0.16164E-03			
0.19980E-03	0.23795E-03	0.27138E-03	0.29790E-03					
0.33113E-06	0.41245E-06	0.15762E-05	0.17759E-05	0.18101E-05	0.18159E-05			
0.18168E-05	0.18168E-05	0.18167E-05	0.18166E-05					
0.0	-0.69305E-05	-0.10621E-08	-0.50808E-09	-0.27148E-09	0.46049E-09			
0.04255E-09	0.65E58E-09	0.16E50E-09	-0.52234E-10					
0.0	0.15288E-01	0.36346E-01	0.68257E-01	0.10945E+00	0.15835E+00			
0.21341E+00	0.27306E+00	0.32790E+01	0.37243E+00					
0.0	-0.24413E-10	-0.67135E-11	0.20905E-10	0.36406E-10	0.29522E-10			
0.50409E-11	-0.21349E-10	-0.26157E-10	0.56106E-12					
0.0	0.71933E-03	0.12737E-02	0.17530E-02	0.21576E-02	0.24876E-02			

-0.40395E+00	-0.42391E+00	-0.42317E+00	-0.40902E+00	-0.39059E+00		DATA0073
0.0	0.58995E-02	0.17399E-01	0.26594E-01	0.29213E-01	0.31244E-01	DATA0074
0.33043E-01	0.34745E-01	0.36086E-01	0.36842E-01	0.38814E-01		DATA0075
0.0	-0.18829E-02	-0.60045E-02	-0.76701E-02	-0.60446E-02	-0.39221E-02	DATA0076
-0.21631E-02	-0.59548E-03	0.54903E-03	0.11376E-02	0.11063E-02		DATA0077

BELL Rotor ALTOROTATICA FLIGHT S-CCF L-GUST FREQ ANALYSIS & EIGEN

8/18/74 DATA0001

1							ITYPE	DATA0002
1							IFLT	DATA0003
S							DNF	DATA0004
1							FREORE	DATA0005
0							IFRMAG	DATA0006
1							EIGEN	DATA0007
3								DATA0008
1.1468	E-748.0	0.7	5040.0					DATA0009
150.0	1260.0	14.0	5.7	6.66E5	51.3	-0.2618		DATA0010
200.5	62.18	5.7	0.004	-0.05	0.0	0.01	0.031	DATA0011
1.0	0.0	0.0	0.0	0.0	0.0		U GUST	DATA0012
2380.1	4143.4	43503.0	236090.0					DATA0013
277.68	890.84	2730.0	12968.0	32494.0	260860.0			DATA0014
9								DATA0015
0.205	0.105	0.105	0.105	0.105	0.105	0.105	0.092	DATA0016
0.073								DATA0017
0.0	0.10964E-01	0.29950E-01	0.63781E-01	0.11024E+00	0.16712E+00			DATA0018
0.23221E+00	0.30335E+00	0.36894E+00	0.42219E+00					DATA0019
0.0	-0.41183E-09	-0.75962E-09	-0.10207E-08	-0.10898E-08	-0.93963E-09			DATA0020
-0.62027E-09	-0.24555E-09	0.53875E-11	0.65046E-10					DATA0021
0.0	0.51546E-03	0.12751E-02	0.19292E-02	0.24779E-02	0.29215E-02			DATA0022
0.32608E-02	0.34966E-02	0.36205E-02	0.36670E-02					DATA0023
0.0	-0.16077E-10	-0.15623E-10	-0.83983E-11	0.20307E-11	0.11862E-10			DATA0024
0.17630E-10	0.16077E-10	0.92860E-11	-0.10057E-11					DATA0025
0.0	0.17816E-04	0.68248E-04	0.12209E-03	0.17651E-03	0.23103E-03			DATA0026
0.28557E-03	0.34010E-03	0.38788E-03	0.42578E-03					DATA0027
0.47329E-06	0.58952E-06	0.22530E-05	0.25383E-05	0.25872E-05	0.25954E-05			DATA0028
0.25966E-05	0.25966E-05	0.25964E-05	0.25962E-05					DATA0029
0.0	-0.11659E-08	-0.17804E-08	-0.15087E-08	-0.42875E-09	0.79769E-09			DATA0030
0.14197E-08	0.10853E-08	0.25164E-09	-0.11546E-09					DATA0031
0.0	0.17340E-01	0.41209E-01	0.77357E-01	0.12399E+00	0.17932E+00			DATA0032
0.24156E+00	0.30895E+00	0.37066E+00	0.42111E+00					DATA0033
0.0	-0.40996E-10	-0.10784E-10	0.35777E-10	0.61402E-10	0.49017E-10			DATA0034
0.72510E-11	-0.36880E-10	-0.44000E-10	0.21093E-11					DATA0035
0.0	0.81566E-03	0.14432E-02	0.19852E-02	0.24418E-02	0.28133E-02			DATA0036

203	0.31005E-02	0.33041E-02	0.34153E-02	0.34619E-02	0.35643E-11	0.37026E-11	0.37026E-11	DATA0037	
	0.0	0.49672E-12	0.17935E-11	0.28992E-11	0.35643E-11	0.37026E-11	0.37026E-11	DATA0038	
	0.33378E-11	0.25690E-11	0.16638E-11	0.89274E-12				DATA0039	
	0.13343E-13	0.15940E-13	0.52715E-13	0.42119E-13	0.19105E-13	-0.59927E-14		DATA0040	
	-0.27980E-13	-0.44239E-13	-0.53361E-13	-0.57253E-13				DATA0041	
	0.0	0.31320E-02	0.86825E-02	0.1E770E-01	0.32902E-01	0.50608E-01		DATA0042	
	0.71446E-01	0.95027E-01	0.11770E+00	0.13703E+00				DATA0043	
	0.0	0.10676E-05	0.19673E-05	0.26404E-05	0.28160E-05	0.24250E-05		DATA0044	
	0.15987E-05	0.63179E-06	-0.14536E-07	-0.16780E-06				DATA0045	
	0.0	0.14634E-03	0.37629E-03	0.5E051E-02	0.76168E-03	0.92102E-03		DATA0046	
	0.10604E-02	0.11828E-02	0.12821E-02	0.13664E-02				DATA0047	
	0.0	0.41643E-07	0.40362E-07	0.21587E-07	-0.54068E-08	-0.30756E-07		DATA0048	
	-0.45549E-07	-0.43324E-07	-0.23887E-07	0.4E793F-08				DATA0049	
	0.0	-0.53691E-03	-0.20566E-02	-0.36787E-02	-0.53178E-02	-0.69590E-02		DATA0050	
	-0.85956E-02	-0.10239E-01	-0.11673E-01	-0.12811E-01				DATA0051	
	-0.14263E-04	-0.17765E-04	-0.67886E-04	-0.76463E-04	-0.77901E-04	-0.78104E-04		DATA0052	
	-0.78083E-04	-0.78012E-04	-0.77934E-04	-0.77864E-04				DATA0053	
	10							DATA0054	
	0.1	0.1	0.1	0.1	0.1	0.1	0.1	DATA0055	
	0.1	0.1						DATA0056	
	0.006993	0.005439	0.003108	0.001295	0.001336	0.001465	0.001165	0.001036	DATA0057
	0.0009712	0.0008417	0.000712						DATA0058
	0.6807	0.5585	0.4363	0.3054	0.2054	0.1222	0.0698	0.0262	DATA0059
	-0.0175	-0.0611	-0.1047						DATA0060
	0.0218								DATA0061
	0.0	0.43406E+00	0.87001E+00	0.13071E+01	0.17459E+01	0.21867E+01		DATA0062	
	0.26295E+01	0.30737E+01	0.35166E+01	0.35633E+01	0.44072E+01			DATA0063	
	0.0	-0.42327E-03	-0.16251E-02	-0.42110E-02	-0.91843E-02	-0.16809E-01		DATA0064	
	-0.26659E-01	-0.37950E-01	-0.49970E-01	-0.61872E-01	-0.73142E-01			DATA0065	
	0.28838E-01	0.29028E-01	0.29055E-01	0.29179E-01	0.29315E-01	0.29452E-01		DATA0066	
	0.29572E-01	0.29644E-01	0.29661E-01	0.29630E-01	0.29554E-01			DATA0067	
	0.0	-0.53766E-04	-0.16352E-03	-0.23308E-03	-0.41699E-03	-0.58510E-03		DATA0068	
	-0.71476E-03	-0.78626E-03	-0.80255E-03	-0.77788E-03	-0.72129E-03			DATA0069	
	0.0	0.13814E+00	0.27332E+00	0.37629E+00	0.40968E+00	0.35495E+00		DATA0070	
	0.21551E+01	0.12193E-01	-0.23614E+00	-0.49140E+00	-0.75705E+00			DATA0071	
	0.0	0.63863E-01	0.22856E+00	0.50534E+00	0.93759E+00	0.15260E+01		DATA0072	

0.22382E+01	0.30330E+01	0.38752E+01	0.47389E+01	0.56075E+01		CATA0073
0.90778E-02	0.93612E-02	0.87107E-02	0.52225E-02	-0.39969E-03	-0.64671E-02	DATA0074
-0.11715E-01	-0.15082E-01	-0.16982E-01	-0.17683E-01	-0.17663E-01		DATA0075
0.0	0.81963E-02	0.13524E-01	0.22872E-01	0.34064E-01	0.43729E-01	CATA0076
0.50693E-01	0.54895E-01	0.57104E-01	0.57871E-01	0.57870E-01		DATA0077
7988.699	37453.0	136740.0	376680.0			DATA0078
0.0	0.94671E-01	0.31163E+00	0.55558E+00	0.97291E+00	0.14786E+01	DATA0079
0.21260E+01	0.28973E+01	0.37551E+01	0.46611E+01	0.55816E+01		DATA0080
0.0	0.22730E+00	0.44648E+00	0.61473E+00	0.67209E+00	0.58087E+00	DATA0081
0.33649E+00	-0.31189E-01	-0.47888E+00	-0.96805E+00	-0.14689E+01		DATA0082
0.0	0.12196E-01	0.16565E-01	0.21075E-01	0.28798E-01	0.38043E-01	DATA0083
0.47582E-01	0.54627E-01	0.55182E-01	0.61171E-01	0.61353E-01		DATA0084
0.15072E-01	0.15215E-01	0.14058E-01	0.86605E-02	-0.47470E-03	-0.11016E-01	DATA0085
-0.20858E-01	-0.27575E-01	-0.31613E-01	-0.33246E-01	-0.33377E-01		DATA0086
0.0	0.20944E+00	0.67206E+00	0.12009E+01	0.16929E+01	0.19969E+01	DATA0087
0.19371E+01	0.14438E+01	0.56583E+00	-0.55484E+00	-0.17710E+01		DATA0088
0.0	-0.66471E+00	-0.12762E+01	-0.17966E+01	-0.21002E+01	-0.20027E+01	DATA0089
-0.13642E+01	-0.18150E+01	0.14329E+01	0.33066E+01	0.52677E+01		DATA0090
0.0	0.26660E-01	0.34476E-01	0.35341E-01	0.29105E-01	0.10407E-01	DATA0091
-0.18427E-01	-0.46323E-01	-0.68326E-01	-0.79558E-01	-0.81443E-01		DATA0092
-0.45442E-01	-0.42335E-01	-0.38601E-01	-0.29705E-01	-0.92970E-02	0.23359E-01	DATA0093
0.61542E-01	0.94766E-01	0.11840E+00	0.12938E+00	0.13108E+00		DATA0094

**B.3.2 The Output Printout for the TILDYN
Program**

**The output printout is illustrated
for autorotation flight of the Bell
model in this subsection.**

***** BELL ROTOR AUTOROTATION FLIGHT 9-DOF U-GUST FREQ ANALYSIS & EIGEN 8/18/74

ITYPE= 1 IFLT= 1 IDOF= 9 IRES= 1 IEIGEN= 1 IFRMAG= 0

NO OF BLADES	ROH	CHORD	IR	HMAST	LOCK NO
3	1.1468001E-07	1.4000000E+01	1.2600000E+03	5.1300003E+01	3.6769247E+00

OMEGA	R	VEL	CL	CD	RANDA
4.800000E+01	1.500000E+02	5.040000E+03	5.6999998E+00	6.4999983E-03	6.9999999E-31

COLLECTIVE PITCH DEL3

2.1800000E-02 -2.6179999E-01

WING L	WING CHOD	WING CL	WING CD	WING CMD	WING CMA
2.0050000E+02	6.2179993E+01	5.6999998E+00	4.0000007E-03	-5.0000001E-02	0.0

DISTANCE AC EA WING ALPHAH

1.000002E-02 3.0999999E-02

EIGENVALUES (NATURAL FREQUENCIES)

--(RAD/SEC)**2--

BLADE COLLECTIVE
7988.699 37453.000

BLADE CYCLIC
2389.100 4143.398

WING

277.680

890.840

2730.000

-- RAD/SEC/OMEGA --

BLADE COLLECTIVE/OMEGA

1.862

4.032

BLADE CYCLIC/OMEGA

1.016

1.341

WING/OMEGA

0.347

0.622

1.089

EXCITING FORCE COMPONENTS

U GUST	V GUST	W GUST	THETA 0	THETA 10	THETA 15
1.0000000E+00	0.0	0.0	0.0	0.0	0.0

***** BLADE MODE SHAPES *****

--- COLLECTIVE MODES ---

I=1

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	0.1507200E-01	0.0	0.0
2	0.1000000E+00	0.2273000E+00	0.1521500E-01	0.9467101E-01	0.1219600E-01
3	0.2000000E+00	0.4464800E+00	0.1405800E-01	0.3116300E+00	0.1656500E-01
4	0.3000001E+00	0.6147300E+00	0.8660499E-02	0.5955800E+00	0.2107500E-01
5	0.4000001E+00	0.6720900E+00	-0.4747000E-03	0.9729100E+00	0.2879800E-01
6	0.5000001E+00	0.5808700E+00	-0.1101600E-01	0.1478600E+01	0.3804300E-01
7	0.6000001E+00	0.3364900E+00	-0.2085800E-01	0.2126000E+01	0.4758200E-01
8	0.7000002E+00	-0.3118900E-01	-0.2757500E-01	0.2897300E+01	0.5462700E-01
9	0.8000002E+00	-0.4788800E+00	-0.3161300E-01	0.3755100E+01	0.5918200E-01
10	0.9000002E+00	-0.9680500E+00	-0.3324600E-01	0.4661100E+01	0.6117100E-01
11	0.1000000E+01	-0.1468900E+01	-0.3337700E-01	0.5581600E+01	0.6135300E-01

I=2

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	-0.4544200E-01	0.0	0.0
2	0.1000000E+00	-0.6647100E+00	-0.4233500E-01	0.2094400E+00	0.2666300E-01
3	0.2000000E+00	-0.1276200E+01	-0.3860100E-01	0.6726600E+00	0.36476100E-01
4	0.3000001E+00	-0.1796600E+01	-0.2970500E-01	0.1200900E+01	0.3534100E-01
5	0.4000001E+00	-0.2100200E+01	-0.9296998E-02	0.1692900E+01	0.2910500E-01
6	0.5000001E+00	-0.2002700E+01	0.2335900E-01	0.1996900E+01	0.1040700E-01
7	0.6000001E+00	-0.1364200E+01	0.6154200E-01	0.1937100E+01	-0.1842700E-01
8	0.7000002E+00	-0.1815000E+00	0.9476602E-01	0.1443800E+01	-0.4632300E-01
9	0.8000002E+00	0.1432900E+01	0.1184000E+00	0.5698300E+00	-0.6932600E-01
10	0.9000002E+00	0.3306600E+01	0.1293800E+00	-0.5548400E+00	-0.7955801E-01
11	0.1000000E+01	0.5267700E+01	0.1310800E+00	-0.1771000E+01	-0.8144321E-01

--- CYCLIC MODES ---

I=1

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	0.2930400E-01	0.0	0.2883800E-01
2	0.1000000E+00	-0.4232700E-03	-0.5376599E-04	0.4340600E+00	0.2902800E-01
3	0.2000000E+00	-0.1625100E-02	-0.1035200E-03	0.8700100E+00	0.2909500E-01
4	0.3000001E+00	-0.4211001E-02	-0.2330800E-03	0.1307100E+01	0.2917900E-01
5	0.4000001E+00	-0.9184301E-02	-0.4169899E-03	0.1745900E+01	0.2931500E-01
6	0.5000001E+00	-0.1680900E-01	-0.5850999E-03	0.2186700E+01	0.2945200E-01
7	0.6000001E+00	-0.2665900E-01	-0.7147600E-03	0.2629500E+01	0.2957200E-01
8	0.7000002E+00	-0.3799000E-01	-0.7862600E-03	0.3073700E+01	0.2964400E-01
9	0.8000002E+00	-0.4997000E-01	-0.8029500E-03	0.3518600E+01	0.2966100E-01
10	0.9000002E+00	-0.6187200E-01	-0.7778800E-03	0.3963300E+01	0.2963000E-01
11	0.1000000E+01	-0.7314199E-01	-0.7212900E-03	0.4407200E+01	0.2955400E-01

I=2

J	XX(J)	V(I,J)	DV(I,J)	W(I,J)	DW(I,J)
1	0.0	0.0	0.1507200E-01	0.0	0.9077799E-02
2	0.1000000E+00	0.6386298E-01	0.8196302E-02	0.1381400E+00	0.9361200E-02
3	0.2000000E+00	0.2285600E+00	0.1352400E-01	0.2733200E+00	0.8710701E-02
4	0.3000001E+00	0.5053400E+00	0.2287200E-01	0.3762900E+00	0.5222499E-02
5	0.4000001E+00	0.9375900E+00	0.3406400E-01	0.4096800E+00	-0.3996899E-03
6	0.5000001E+00	0.1526000E+01	0.4372900E-01	0.3549500E+00	-0.6467100E-02
7	0.6000001E+00	0.2238200E+01	0.5069300E-01	0.2155100E+00	-0.1171500E-01
8	0.7000002E+00	0.3033000E+01	0.5489500E-01	0.1219300E-01	-0.1508200E-01
9	0.8000002E+00	0.3875200E+01	0.5710400E-01	-0.2301400E+00	-0.1698200E-01
10	0.9000002E+00	0.4738900E+01	0.5787100E-01	-0.4914000E+00	-0.1768300E-01
11	0.1000000E+01	0.5607500E+01	0.5787000E-01	-0.7570500E+00	-0.1766300E-01

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J	XX(J)	THE TN(J)	AMASS(J)
1	0.0	0.6807000E+00	0.6992999E-02
2	0.1000000E+00	0.5585000E+00	0.5438998E-02
3	0.2000000E+00	0.4363000E+00	0.3108000E-02
4	0.3000001E+00	0.3054000E+00	0.1295000E-02
5	0.4000001E+00	0.2094000E+00	0.1336000E-02
6	0.5000001E+00	0.1222000E+00	0.1465000E-02
7	0.6000001E+00	0.6980002E-01	0.1165000E-02
8	0.7000002E+00	0.2620000E-01	0.1036000E-02
9	0.8000002E+00	-0.1750000E-01	0.9711999E-03
10	0.9000002E+00	-0.6110000E-01	0.8417000E-03
11	0.1000000E+01	-0.1047000E+00	0.7120001E-03

***** WING MODE SHAPES *****

II=1	J	WX(J)	G(II,J)	DG(II,J)	Z(II,J)	DZ(II,J)	WPHI(II,J)	DWPHI(II,J)
	1	0.0	0.0	0.0	0.0	0.0	0.0	0.4732900E-06
	2	0.2050000E+00	0.1096400E-01	0.5154600E-03	-0.4118299E-09	-0.1607730E-10	0.1781600E-04	0.5895200E-06
	3	0.3100000E+00	0.2995000E-01	0.1275100E-02	-0.7596199E-09	-0.1562300E-10	0.6824800E-04	0.2253000E-05
	4	0.4150000E+00	0.6378102E-01	0.1929200E-02	-0.1020700E-08	-0.8398300E-11	0.1220900E-03	0.2538300E-05
	5	0.5200000E+00	0.1102400E+00	0.2477900E-02	-0.1089800E-08	0.2030700E-11	0.1765100E-03	0.2587200E-05
	6	0.6250001E+00	0.1671200E+00	0.2921500E-02	-0.9396299E-09	0.1186200E-10	0.2310300E-03	0.2595400E-05
	7	0.7300001E+00	0.2322100E+00	0.3260200E-02	-0.6202701E-09	0.1762999E-10	0.2855700E-03	0.2596600E-05
	8	0.8350001E+00	0.3033500E+00	0.3496800E-02	-0.2455800E-09	0.1680700E-10	0.3400999E-03	0.2596600E-05
	9	0.9270001E+00	0.3689400E+00	0.3620500E-02	0.5387500E-11	0.9286000E-11	0.3878800E-03	0.2596400E-05
	10	0.1000000E+01	0.4221900E+00	0.3667900E-02	0.6504600E-10	-0.1889700E-11	0.4257800E-03	0.2596200E-05

II=2	J	WX(J)	G(II,J)	DG(II,J)	Z(II,J)	DZ(II,J)	WPHI(II,J)	DWPHI(II,J)
	1	0.0	0.0	0.0	0.0	0.0	0.0	0.1334300E-13
	2	0.2050000E+00	-0.1165900E-08	-0.4099600E-10	0.1734000E-01	0.8156600E-03	0.4967200E-12	0.1594000E-13
	3	0.3100000E+00	-0.1780400E-08	-0.1078400E-10	0.4120900E-01	0.1443200E-02	0.1793500E-11	0.5271500E-13
	4	0.4150000E+00	-0.1508700E-08	0.3577701E-10	0.7735699E-01	0.1985200E-02	0.2899200E-11	0.4211900E-13
	5	0.5200000E+00	-0.4287499E-09	0.6140199E-10	0.1239900E+00	0.2441800E-02	0.3564300E-11	0.1910500E-13
	6	0.6250001E+00	0.7976899E-09	0.4901700E-10	0.1793200E+00	0.2813300E-02	0.3702600E-11	-0.5992701E-14
	7	0.7300001E+00	0.1419700E-08	0.7251000E-11	0.2415600E+00	0.3100500E-02	0.3337800E-11	-0.2798000E-13
	8	0.8350001E+00	0.1085300E-08	-0.3688000E-10	0.3089500E+00	0.3304100E-02	0.2569000E-11	-0.4423900E-13
	9	0.9270001E+00	0.2516400E-09	-0.4400000E-10	0.3708600E+00	0.3415300E-02	0.1663800E-11	-0.5336100E-13
	10	0.1000000E+01	-0.1154600E-09	0.2109300E-11	0.4211100E+00	0.3461900E-02	0.8527400E-12	-0.5725298E-13

II=3	J	WX(J)	G(II,J)	DG(II,J)	Z(II,J)	DZ(II,J)	WPHI(II,J)	DWPHI(II,J)
	1	0.0	0.0	0.0	0.0	0.0	0.0	-0.1426300E-04
	2	0.2050000E+00	0.3132000E-02	0.1483400E-03	0.1067600E-05	0.4164300E-07	-0.5369100E-03	-0.1776501E-04
	3	0.3100000E+00	0.8682501E-02	0.3762899E-03	0.1967300E-05	0.4036200E-07	-0.2056600E-02	-0.6788599E-04
	4	0.4150000E+00	0.1877000E-01	0.5805099E-03	0.2640400E-05	0.2158000E-07	-0.3678700E-02	-0.7646299E-04
	5	0.5200000E+00	0.3290200E-01	0.7616801E-03	0.2816000E-05	-0.5406800E-08	-0.5317800E-02	-0.7790100E-04
	6	0.6250001E+00	0.5060800E-01	0.9210201E-03	0.2425000E-05	-0.3075600E-07	-0.6958999E-02	-0.7810400E-04
	7	0.7300001E+00	0.7144600E-01	0.1060430E-02	0.1598700E-05	-0.4554900E-07	-0.8599602E-02	-0.7808300E-04
	8	0.8350001E+00	0.9502703E-01	0.1182800E-02	0.6317900E-06	-0.4332400E-07	-0.1023900F-01	-0.7801200E-04
	9	0.9270001E+00	0.1177000E+00	0.1282100E-02	-0.1453600E-07	-0.2388700E-07	-0.1167300E-01	-0.7793400E-04
	10	0.1000000E+01	0.1370300E+00	0.1366400E-02	-0.1678000E-06	0.4879501E-08	-0.1281100E-01	-0.7786400E-04

EQUATIONS OF MOTION : $A*X^3+B*X^2+C*X=D*E$

A MATRIX =

B MATRIX=

0.54017E+00	0.0	0.0	-0.26876E+00	0.0	0.0	0.69574E-11	0.45043E-01	-0.17948E-07	-0.13242E+02
0.0	0.37042E+00	0.20000E+01	0.0	-0.41167E+00	0.0	-0.53078E-02	0.25859E+00	0.15970E+00	0.0
0.0	-0.20000E+01	0.37042E+00	0.0	0.0	-0.41167E+00	0.77536E-01	0.43156E-01	-0.94210E+00	0.0
-0.19099E+00	0.0	0.0	0.43642E+00	0.0	0.0	0.17233E-11	0.11157E-01	-0.44457E-08	-0.23007E+00
0.0	-0.34603E+00	0.0	0.0	0.39483E+00	0.20030E+01	0.49567E-02	-0.14325E-01	-0.14914E+00	0.0
0.0	0.0	-0.34603E+00	0.0	-0.20000E+01	0.39483E+00	-0.45688E-01	-0.40302E-01	0.38752E-01	0.0
0.22544E-10	-0.79814E-02	0.25224E-01	-0.21837E-12	0.88643E-02	-0.66846E-01	0.32997E-01	0.67399E-02	-0.18662E-01	-0.71542E-09
0.14595E+00	-0.33128E+00	0.64894E-01	-0.14137E-02	-0.32659E-01	-0.72073E-01	0.855543E-02	0.28552E-01	0.22520E-02	-0.46317E+01
-0.58157E-07	0.24015E+00	0.12474E+01	0.56333E-09	-0.26671E+00	0.10046E+00	-0.18944E-01	0.21209E-02	0.12854E+00	0.18456E-05
-0.33172E+02	0.0	0.0	-0.33280E+01	0.0	0.0	-0.68859E-09	-0.44580E+01	0.17764E-05	0.11459E+04

C MATRIX=

D MATRIX*

0.0	0.0	-0.11231E+02	0.24135E+02	0.0	0.0
0.0	0.11374E+02	0.0	0.0	0.23678E+02	0.0
-0.11374E+02	0.0	0.0	0.0	0.0	0.23678E+02
0.0	0.0	-0.27819E+01	0.37430E+01	0.0	0.0
0.0	-0.10925E+02	0.0	0.0	-0.23117E+02	0.0
0.10925E+02	0.0	0.0	0.0	0.0	-0.23117E+02
-0.10349E+02	-0.24586E+00	0.38116E+00	0.14824E-08	-0.51082E+00	-0.57982E+01
-0.22047E+01	0.16228E+01	-0.45530E+01	0.95973E+01	0.25721E+01	0.41534E+01
0.29504E+01	0.73975E+01	0.37122E+00	-0.38242E-05	0.15370E+02	-0.11503E+02
0.0	0.0	0.15879E+04	-0.23930E+04	0.0	0.0

FREQUENCY RESPONSE

--FREQUENCY/OMEGA--

Q1C Q1C Q1S Q20 Q2C Q2S WING 1 WING 2 WING 3

D(NU R)/DT

-- 0.01--

0.188E-06 0.772E+00 0.304E+00 0.549E-07 0.476E-01 0.243E-01 0.162E+00 0.518E-03 0.527E-02
0.959E-05

-- 0.02--

0.473E-06 0.771E+00 0.304E+00 0.114E-06 0.486E-01 0.480E-01 0.162E+00 0.531E-03 0.584E-02
0.196E-04

-- 0.03--

0.921E-06 0.769E+00 0.305E+00 0.180E-06 0.505E-01 0.719E-01 0.164E+00 0.553E-03 0.667E-02
0.306E-04

-- 0.04--

0.159E-05 0.766E+00 0.307E+00 0.259E-06 0.534E-01 0.959E-01 0.165E+00 0.584E-03 0.767E-02
0.429E-04

-- 0.05--

0.252E-05 0.762E+00 0.308E+00 0.355E-06 0.576E-01 0.120E+00 0.167E+00 0.623E-03 0.878E-02
0.570E-04

-- 0.06--

0.379E-05 0.758E+00 0.311E+00 0.473E-06 0.633E-01 0.145E+00 0.170E+00 0.670E-03 0.994E-02
0.732E-04

-- 0.07--

0.548E-05	0.753E+00	0.314E+00	0.619E-06	0.708E-01	0.170E+00	0.173E+00	0.726E-03	0.111E-01
0.920E-04								

-- 0.08--

0.766E-05	0.746E+00	0.317E+00	0.798E-06	0.802E-01	0.195E+00	0.177E+00	0.790E-03	0.123E-01
0.114E-03								

-- 0.09--

0.104E-04	0.739E+00	0.321E+00	0.102E-05	0.918E-01	0.220E+00	0.181E+00	0.862E-03	0.135E-01
0.139E-03								

-- 0.10--

0.140E-04	0.731E+00	0.326E+00	0.129E-05	0.106E+00	0.246E+00	0.186E+00	0.944E-03	0.147E-01
0.167E-03								

-- 0.12--

0.237E-04	0.710E+00	0.338E+00	0.203E-05	0.140E+00	0.300E+00	0.198E+00	0.114E-02	0.170E-01
0.237E-03								

-- 0.14--

0.384E-04	0.685E+00	0.354E+00	0.312E-05	0.186E+00	0.356E+00	0.213E+00	0.138E-02	0.192E-01
0.329E-03								

-- 0.16--

0.602E-04	0.652E+00	0.373E+00	0.474E-05	0.243E+00	0.414E+00	0.231E+00	0.169E-02	0.212E-01
0.449E-03								

214

-- 0.18--

0.921E-04	0.610E+00	0.396E+00	0.713E-05	0.312E+00	0.473E+00	0.253E+00	0.208E-02	0.229E-01
	0.608E-03							

-- 0.20--

0.139E-03	0.558E+00	0.420E+00	0.107E-04	0.391E+00	0.530E+00	0.278E+00	0.259E-02	0.242E-01
	0.820E-03							

-- 0.22--

0.206E-03	0.495E+00	0.444E+00	0.158E-04	0.476E+00	0.579E+00	0.309E+00	0.325E-02	0.253E-01
	0.110E-02							

-- 0.24--

0.302E-03	0.425E+00	0.462E+00	0.232E-04	0.562E+00	0.617E+00	0.348E+00	0.407E-02	0.259E-01
	0.146E-02							

-- 0.26--

0.437E-03	0.355E+00	0.475E+00	0.338E-04	0.644E+00	0.642E+00	0.401E+00	0.512E-02	0.263E-01
	0.194E-02							

-- 0.28--

0.633E-03	0.292E+00	0.484E+00	0.494E-04	0.724E+00	0.662E+00	0.486E+00	0.651E-02	0.264E-01
	0.258E-02							

-- 0.30--

0.944E-03	0.239E+00	0.500E+00	0.745E-04	0.822E+00	0.694E+00	0.635E+00	0.861E-02	0.242E-01
	0.355E-02							

-- 0.32--

0.154E-02	0.183E+00	0.540E+00	0.123E-03	0.987E+00	0.784E+00	0.967E+00	0.125E-01	0.242E-01
	0.536E-02							

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— 65 —

0.114E-01 0.268E+00 0.138E+00 0.105E-02 0.242E+00 0.781E-01 0.673E-01 0.262E-01 0.252E-01
0.156E-01

-- 8,70 --

0.707E-02 0.274E+00 0.152E+00 0.658E-03 0.239E+00 0.694E-01 0.566E-01 0.140E-01 0.390E-01
0.865E-02

-- 0.75 --

0.586E-02 0.273E+00 0.155E+00 0.548E-03 0.234E+00 0.687E-01 0.483E-01 0.101E-01 0.466E-01
0.645E-02

— 0.80 —

0.548E-02 0.271E+00 0.158E+00 0.512E-03 0.229E+00 0.704E-01 0.418E-01 0.825E-02 0.536E-01
0.545E-02

— 0.85 —

0.550E-02 0.270E+00 0.161E+00 0.513E-03 0.226E+00 0.736E-01 0.367E-01 0.726E-02 0.613E-01
0.496E-02

--- C.90 ---

0.580E-02 0.271E+00 0.165E+00 0.537E-03 0.225E+00 0.781E-01 0.326E-01 0.670E-02 0.706E-01
0.477E-02

— 0.95 —

0.639E-02 0.275E+00 0.170E+00 0.585E-03 0.226E+00 0.840E-01 0.293E-01 0.649E-02 0.826E-01
0.480E-02

214

	--	2.50--								
		0.501E-02	0.408E-01	0.389E-01	0.105E-02	0.273E+00	0.299E+00	0.496E-02	0.105E-02	0.468E-01
		0.587E-03								
	--	2.60--								
		0.364E-02	0.463E-01	0.644E-01	0.913E-03	0.194E+00	0.225E+00	0.308E-02	0.811E-03	0.305E-01
		0.385E-03								
	--	2.70--								
		0.262E-02	0.470E-01	0.694E-01	0.781E-03	0.139E+00	0.170E+00	0.219E-02	0.617E-03	0.200E-01
		0.249E-03								
	--	2.80--								
		0.196E-02	0.436E-01	0.667E-01	0.694E-03	0.105E+00	0.134E+00	0.182E-02	0.485E-03	0.138E-01
		0.167E-03								
	--	2.90--								
		0.153E-02	0.392E-01	0.619E-01	0.640E-03	0.820E-01	0.110E+00	0.164E-02	0.393E-03	0.992E-02
		0.115E-03								
	--	3.00--								
		0.122E-02	0.350E-01	0.568E-01	0.608E-03	0.662E-01	0.923E-01	0.154E-02	0.326E-03	0.737E-02
		0.796E-04								
	--	3.50--								
		0.539E-03	0.201E-01	0.375E-01	0.674E-03	0.298E-01	0.495E-01	0.123E-02	0.156E-03	0.219E-02
		0.758E-05								

-- 4.00--

0.420E-03 0.125E-01 0.265E-01 0.135E-02 0.169E-01 0.324E-01 0.993E-03 0.999E-06 0.796E-03
0.646E-04

-- 4.50--

0.227E-03 0.840E-02 0.199E-01 0.492E-03 0.107E-01 0.234E-01 0.807E-03 0.745E-04 0.319E-03
0.331E-04

-- 5.00--

0.140E-03 0.592E-02 0.155E-01 0.203E-03 0.733E-02 0.178E-01 0.665E-03 0.503E-04 0.174E-03
0.155E-04

-- 5.50--

220 0.979E-04 0.435E-02 0.125E-01 0.113E-03 0.526E-02 0.141E-01 0.556E-03 0.366E-04 0.156E-03
0.928E-05

-- 6.00--

0.727E-04 0.329E-02 0.103E-01 0.731E-04 0.392E-02 0.115E-01 0.471E-03 0.278E-04 0.159E-03
0.626E-05

-- 6.50--

0.561E-04 0.256E-02 0.861E-02 0.513E-04 0.301E-02 0.959E-02 0.404E-03 0.218E-04 0.159E-03
0.456E-05

-- 7.00--

0.446E-04 0.203E-02 0.734E-02 0.380E-04 0.236E-02 0.812E-02 0.353E-03 0.176E-04 0.152E-03
0.350E-05

-- 7.50--
0.362E-04 0.164E-02 0.633E-02 0.294E-04 0.189E-02 0.698E-02 0.306E-03 0.144E-04 0.144E-03
0.279E-05

-- 8.00--
0.300E-04 0.134E-02 0.552E-02 0.234E-04 0.154E-02 0.606E-02 0.269E-03 0.121E-04 0.135E-03
0.230E-05

-- 8.50--
0.252E-04 0.112E-02 0.485E-02 0.191E-04 0.127E-02 0.532E-02 0.239E-03 0.102E-04 0.125E-03
0.194E-05

-- 9.00--
0.215E-04 0.938E-03 0.431E-02 0.159E-04 0.106E-02 0.471E-02 0.214E-03 0.876E-05 0.116E-03
0.167E-05

-- 9.50--
0.185E-04 0.796E-03 0.385E-02 0.134E-04 0.895E-03 0.420E-02 0.192E-03 0.759E-05 0.107E-03
0.146E-05

-- 10.00--
0.162E-04 0.682E-03 0.346E-02 0.115E-04 0.763E-03 0.377E-02 0.174E-03 0.664E-05 0.992E-04
0.130E-05

EIGENVALUES

	** REAL PART **	** IMAGINARY PART **	** DAMPING RATIO **
NO. 1	0.0	0.0	0.0
NO. 2	-0.2092248D+00	0.4071266D+01	0.5132288E-01
NO. 2	-0.2092248D+00	-0.4071266D+01	0.5132288E-01
NO. 3	-0.1481056D+00	0.2421839D+01	0.6104013E-01
NO. 3	-0.1481056D+00	-0.2421839D+01	0.6104013E-01
NO. 4	-0.2021002D+00	0.1945624D+01	0.1033183E+00
NO. 4	-0.2021002D+00	-0.1945624D+01	0.1033183E+00
NO. 5	-0.2632103D+00	0.1875147D+01	0.1390050E+00
NO. 5	-0.2632103D+00	-0.1875147D+01	0.1390050E+00
NO. 6	-0.3342787D-01	0.1260777D+01	0.2650439E-01
NO. 6	-0.3342787D-01	-0.1260777D+01	0.2650439E-01
NO. 7	-0.1144592D-01	0.6041955D+00	0.1894066E-01
NO. 7	-0.1144592D-01	-0.6041955D+00	0.1894066E-01
NO. 8	-0.1537569D-01	0.3459382D+00	0.4440252E-01
NO. 8	-0.1537569D-01	-0.3459382D+00	0.4440252E-01
NO. 9	-0.1094665D+00	0.2452122D+00	0.4076408E+00
NO. 9	-0.1094665D+00	-0.2452122D+00	0.4076408E+00
NO.10	-0.2820982D+00	0.4124979D-01	0.9894778E+00
NO.10	-0.2820982D+00	-0.4124979D-01	0.9894778E+00
NO.11	-0.3179021D+00	0.0	0.1000000E+01

EIGENVECTORS

-- CORRESPONDING TO NO. 1 EIGENVALUE -- (0.0 1+IMAG(0.0))

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.0	0.0	0.0
0.1000000E+01	0.1000000E+01	0.0

223

-- CORRESPONDING TO NO. 2 EIGENVALUE -- (-0.209D+00)+IMAG(0.407D+01)

** ABSOLUTE VALUE **

** REAL PART ** ** IMAGINARY PART **

0.1107064E+00	0.5960987E-01	-0.9328753E-01
0.4401162E-02	0.4983202E-03	-0.4372858E-02
0.3052047E-01	0.3021199E-01	-0.4328273E-02
0.1000000E+01	0.1000000E+01	0.0
0.2562390E-01	-0.2548093E-01	0.2702991E-02
0.1051418E-01	0.2121001E-02	0.1029802E-01
0.1073238E-03	0.3453433E-04	0.1016158E-03
0.1779419E-01	-0.1765273E-01	0.2239201E-02
0.5262852E-02	0.1084798E-02	0.5149834E-02
0.1381952E-01	0.1266621E-01	-0.5501822E-02

-- CORRESPONDING TO NO. 3 EIGENVALUE --

(-0.148D+00)+IMAG(0.242D+01)

** ABSOLUTE VALUE **

0.1813177E-01
0.4931911E+00
0.3320159E+00
0.3046985E-02
0.9230196E+00
0.1000000E+01
0.1226842E-01
0.3355967E-02
0.1654489E+00
0.9685631E-03

** REAL PART ** ** IMAGINARY PART **

0.5256832E-02 -0.1735301E-01
0.4925372E+00 -0.2539496E-01
-0.2398358E-01 -0.3311487E+00
0.5288171E-03 0.3000749E-02
0.5510997E-02 0.9230042E+00
0.1000000E+01 0.0
0.1224252E-01 -0.7968692E-03
-0.1360433E-03 0.3353212E-02
-0.1650685E+00 0.1121332E-01
-0.8815918E-03 -0.4011374E-03

224

-- CORRESPONDING TO NO. 4 EIGENVALUE --

(-0.202D+00)+IMAG(0.195D+01)

** ABSOLUTE VALUE **

0.2562918E-01
0.1000000E+01
0.9137043E+00
0.1247240E-02
0.3160684E+00
0.3624439E+00
0.4554648E-02
0.1546631E-02
0.1053016E+00
0.2736067E-02

** REAL PART ** ** IMAGINARY PART **

0.2539718E-01 0.4704274E-02
0.1000000E+01 0.0
-0.5365834E-01 -0.9121275E+00
-0.8799934E-03 0.8838666E-03
-0.2004018E+00 0.2444144E+00
0.2816455E+00 0.2281262E+00
0.4206777E-02 0.1745808E-02
-0.1443410E-02 0.5555502E-03
-0.9349859E-01 -0.4844000E-01
0.7346331E-03 -0.2635599E-02

-- CORRESPONDING TO NO. 5 EIGENVALUE -- (-0.263D+00)+IMAG(0.188D+01)

** ABSOLUTE VALUE **

0.1000000E+01
0.9817582E-01
0.5672661E-01
0.3115343E-01
0.1848055E-01
0.5520776E-01
0.6100570E-03
0.2630625E-01
0.4581391E-01
0.1181544E+00

** REAL PART ** ** IMAGINARY PART **

0.1000000E+01 0.0
-0.7606643E-01 -0.6206755E-01
0.2192894E-01 0.5231665E-01
-0.1489975E-01 0.2735936E-01
0.1686821E-01 0.7549502E-02
0.1644658E-02 -0.5519328E-01
0.7883347E-04 -0.6049422E-03
-0.2571483E-01 0.5546831E-02
0.2269105E-01 0.3979991E-01
-0.8819941E-03 -0.1181511E+00

225

-- CORRESPONDING TO NO. 6 EIGENVALUE -- (-0.334D-01)+IMAG(0.126D+01)

** ABSOLUTE VALUE **

0.5219237E-01
0.1000000E+01
0.3072107E+00
0.4124053E-02
0.5034070E+00
0.2649921E+00
0.1200790E-01
0.2355482E-01
0.7685637E+00
0.1921409E-01

** REAL PART ** ** IMAGINARY PART **

-0.4088937E-01 -0.3243618E-01
0.1000000E+01 0.0
0.1548536E+00 -0.2653276E+00
-0.1214229E-02 -0.3941245E-02
-0.2209883E+00 -0.4523084E+00
-0.9316647E-01 0.2480742E+00
-0.9718515E-02 0.7052649E-02
-0.9464018E-02 -0.2156994E-01
-0.7237886E+00 0.2584966E+00
-0.1733962E-01 0.8277591E-02

-- CORRESPONDING TO NO. 7 EIGENVALUE -- (-0.114D-01)+IMAG(0.604D+00)

** ABSOLUTE VALUE **	** REAL PART **	** IMAGINARY PART **
0.1899540E+00	-0.9512359E-01	0.1644202E+00
0.7186074E+00	-0.1414695E+00	0.7045444E+00
0.1000000E+01	0.1000000E+01	0.0
0.1727831E-01	-0.1256843E-01	0.1185641E-01
0.3531273E+00	0.1046424E+00	-0.3372667E+00
0.6229418E+00	-0.2424563E+00	-0.5738217E+00
0.5332350E-01	-0.2112583E-01	-0.4896023E-01
0.5013081E+00	-0.3956270E+00	0.3078783E+00
0.3995003E+00	-0.2640249E+00	-0.2998188E+00
0.4824777E+00	0.1262509E+00	0.4656667E+00

-- CORRESPONDING TO NO. 8 EIGENVALUE -- (-0.154D-01)+IMAG(0.346D+00)

** ABSOLUTE VALUE **	** REAL PART **	** IMAGINARY PART **
0.1800445E-02	0.6788953E-03	0.1667545E-02
0.2911242E+00	0.2866872E+00	0.5063349E-01
0.4352518E+00	0.4194663E+00	-0.1161560E+00
0.1424049E-03	0.4478541E-04	0.1351793E-03
0.0451266E+00	0.5476120E+00	-0.6437076E+00
0.6462139E+00	0.1607376E+00	0.6259041E+00
0.1000000E+01	0.1000000E+01	0.0
0.1269024E-01	0.1486531E-02	0.1260268E-01
0.2067884E-01	-0.9552781E-02	0.1834010E-01
0.1675373E-01	0.1418500E-01	0.8914784E-02

-- CORRESPONDING TO NO. 9 EIGENVALUE --

(-0.1090+00)+IMAGI 0.2450+00)

** ABSOLUTE VALUE **

0.2434947E-03
0.5692835E+00
0.5258981E+00
0.1357527E-04
0.9552389E+00
0.1000000E+01
0.8736736E-01
0.2355762E-02
0.8463684E-02
0.4402682E-02

** REAL PART ** ** IMAGINARY PART **

0.8291703E-04 0.2289419E-03
-0.5446492E+00 -0.1656526E+00
0.9681088E-01 -0.5169105E+00
0.4603972E-05 0.1277072E-04
-0.1093801E-01 -0.9551762E+00
0.1000000E+01 0.0
-0.8715111E-01 0.6141596E-02
0.1651092E-02 0.1680330E-02
0.7221349E-02 -0.4414298E-02
0.4384559E-02 -0.3990191E-03

-- CORRESPONDING TO NO.10 EIGENVALUE --

(-0.2820+00)+IMAGI 0.4120-01)

** ABSOLUTE VALUE **

0.2436394E-02
0.1000000E+01
0.9246252E+00
0.1798500E-04
0.6785136E+00
0.4797139E+00
0.4522312E-01
0.5225770E-02
0.3273904E-01
0.5858627E-01

** REAL PART ** ** IMAGINARY PART **

-0.2435637E-02 0.6074352E-04
0.1000000E+01 0.0
-0.2559280E+00 -0.8885002E+00
-0.9399982E-05 -0.1533299E-04
-0.5765943E+00 -0.3576586E+00
-0.2741120E+00 0.3936852E+00
0.4180256E-01 0.1725332E-01
0.2554759E-02 0.4558720E-02
-0.2485351E-01 0.2131075E-01
0.5792243E-01 0.8794524E-02

-- CORRESPONDING TO NO.11 EIGENVALUE --

(-0.318D+00)+IMAGI 0.0

** ABSOLUTE VALUE **

0.4641774E-01
0.1062824E+00
0.5789774E-01
0.2153117E-03
0.3157100E-01
0.7271057E-01
0.3048246E-02
0.6654162E-02
0.2990245E-02
0.1000000E+01

** REAL PART ** ** IMAGINARY PART **

-0.4641774E-01 0.0
0.1062824E+00 0.0
0.5789774E-01 0.0
0.2153117E-03 0.0
-0.3157100E-01 0.0
-0.7271057E-01 0.0
0.3048246E-02 0.0
-0.6654162E-02 0.0
-0.2990245E-02 0.0
0.1000000E+01 0.0